



Postbus 14607  
1001 LC Amsterdam  
+31[0]20-688 09 64  
E: info@ir-groep.nl  
www.deingenieursgroep.nl

Project **Interne verbouwing**  
Rustenburgerstraat 246 Amsterdam

Opdrachtgever Lycée français Vincent van Gogh

Onderdeel Statische berekening constructie

Projectnummer **240772**

Datum 18 december 2024

Aantal pagina's 125

Opgesteld door ir. T. Willeboordse

.....  
tw

Gecontroleerd door ir. L. Rob

.....  
Lz

| revisie | datum | omschrijving | door |
|---------|-------|--------------|------|
|         |       |              |      |
|         |       |              |      |
|         |       |              |      |
|         |       |              |      |

## INHOUDSOPGAVE

|       |                                                                |     |
|-------|----------------------------------------------------------------|-----|
| 1     | Algemene gegevens .....                                        | 3   |
| 1.1   | Projectbeschrijving .....                                      | 3   |
| 1.1.1 | Brandwerendheid .....                                          | 6   |
| 1.3   | Geldende voorschriften .....                                   | 7   |
| 1.4   | Gevolgklasse, betrouwbaarheidsklasse en belastingfactoren..... | 8   |
| 1.4.1 | Rekenwaarden van belastingen (STR/GEO) (Groep B).....          | 8   |
| 1.4.2 | Rekenwaarden van belastingen bruikbaarheidsgrenstoestand.....  | 9   |
| 1.5   | Materialen .....                                               | 10  |
| 1.5.1 | Beton .....                                                    | 10  |
| 1.5.2 | Staal.....                                                     | 10  |
| 1.5.3 | Hout .....                                                     | 10  |
| 1.5.4 | Metselwerk.....                                                | 10  |
| 1.6   | Bijbehorende documenten.....                                   | 11  |
| 1.6.1 | Tekeningen constructief .....                                  | 11  |
| 1.6.2 | Tekeningen bouwkundig .....                                    | 11  |
| 2     | Overzicht belastingen.....                                     | 12  |
| 3     | Houtconstructie .....                                          | 15  |
| 3.1   | Balklaag dakkapel .....                                        | 15  |
| 3.2   | Slaper dakkapel.....                                           | 17  |
| 3.4   | Controle balklaag zoldervloer .....                            | 45  |
| 3.5   | Controle balklaag zoldervloer met versterking.....             | 48  |
| 3.6   | Balklaag zoldervloer nieuw naast trapsparing .....             | 51  |
| 3.7   | Staartbalken trapraveling .....                                | 53  |
| 3.8   | Spant tpv trap .....                                           | 55  |
| 3.9   | Trapraveling.....                                              | 105 |
| 3.10  | Afdracht horizontale belasting spant naar vloer.....           | 117 |

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



## **1 ALGEMENE GEGEVENS**

### **1.1 Projectbeschrijving**

In dit document worden de volgende constructieve onderdelen behandeld:

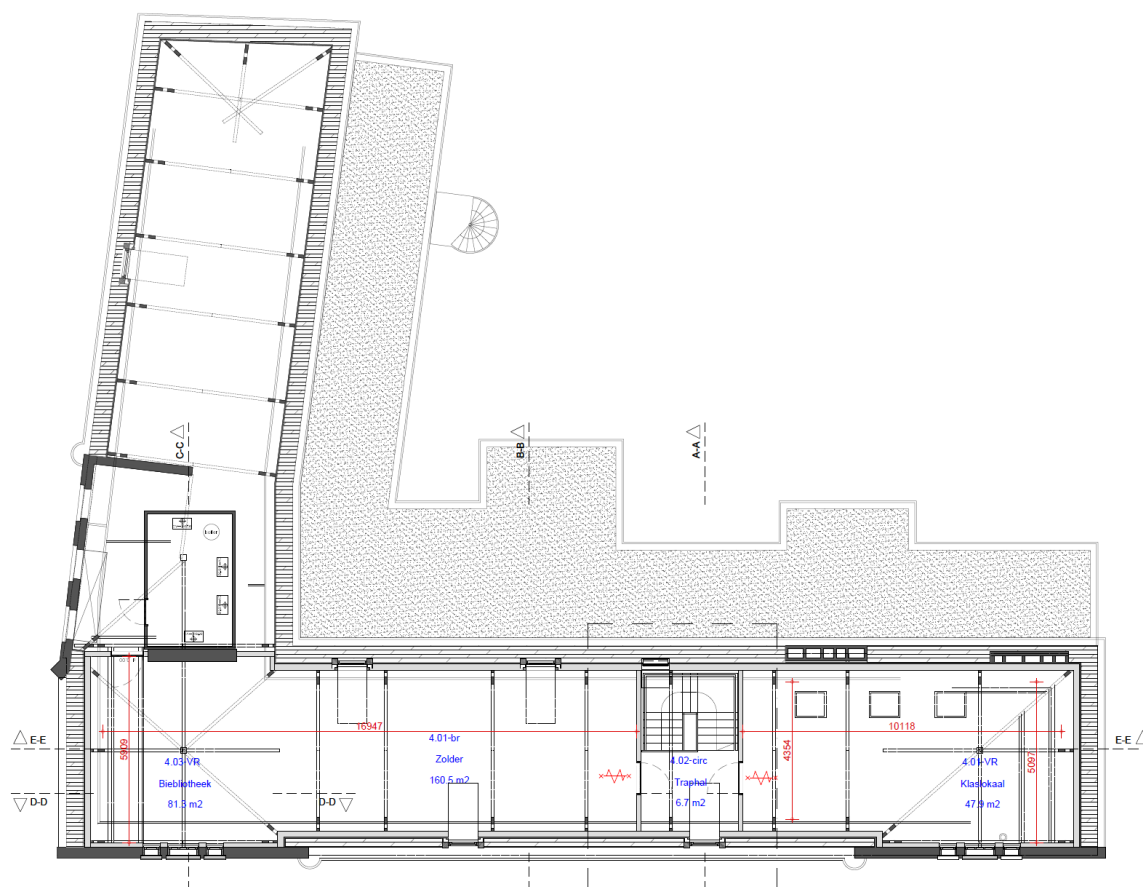
- Controle zoldervloer
- Traptraveling
- Controle dakspant tpv trapsparing
- dakkapel

Project Rustenburgerstraat 246 Franse School

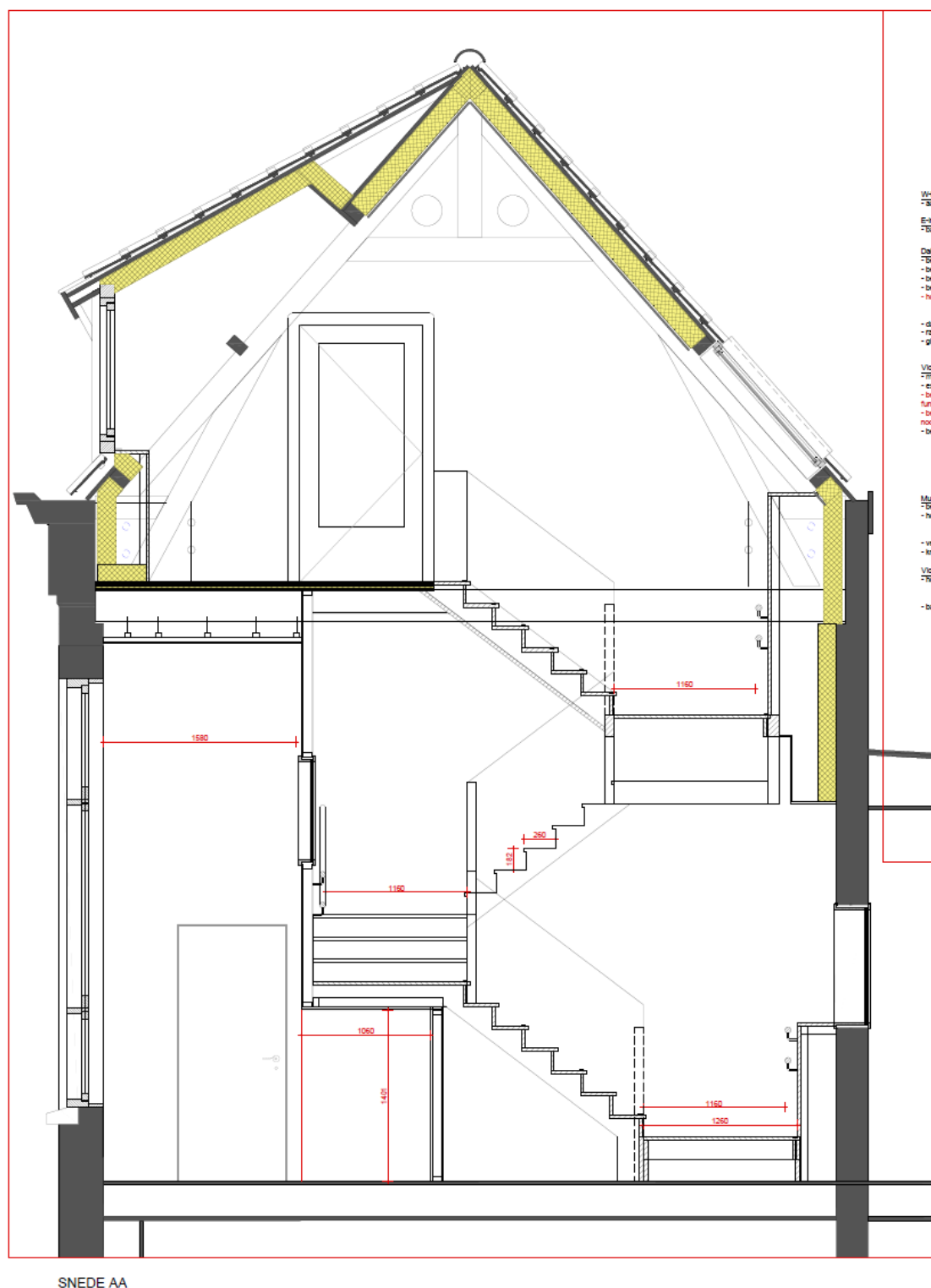
Projectnummer 240772

Revisie

IRg



Plattegrond 3<sup>e</sup> verdieping



doorsnede

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



#### 1.1.1 Brandwerendheid

Voor het in stand houden van de rookvrije vluchtroutes geldt een minimale eis aan de constructie van 30 min.

De door het bouwbesluit gestelde minimale eisen aan de hoofddraagconstructie zijn:

|                                       |                    |
|---------------------------------------|--------------------|
| hoogste vloer met een verblijfsgebied | : 15 m             |
| functie                               | : Onderwijsfunctie |
| reductie toegestaan?                  | : Nee              |

Brandwerendheid (hoofddraagconstructie) : 60 min ( bestaande bouw)

Deze brandwerendheid wordt bereikt door de constructie brandwerend te omkleden / schilderen / betongevulde profielen (met wapening) toe te passen.

In brandwerende scheidingen toegepaste constructie onderdelen dienen minimaal een brandwerendheid te hebben die overeenkomt met de eisen gesteld aan deze brandwerende scheiding.

### 1.3 Geldende voorschriften

#### Eurocode 0: Grondslagen

NEN-EN 1990 Grondslagen van het constructief ontwerp

#### Eurocode 1: Belastingen op constructies

NEN-EN 1991-1-1 Volumieke gewichten, eigen gewicht, opgelegde belastingen

NEN-EN 1991-1-2 Belastingen bij brand

NEN-EN 1991-1-3 Sneeuwbelastingen

NEN-EN 1991-1-4 Windbelastingen

NEN-EN 1991-1-5 Thermische belastingen

NEN-EN 1991-1-7 Buitengewone belastingen

#### Eurocode 2: Betonconstructies

NEN-EN 1992-1-1 Algemene regels en regels voor gebouwen

NEN-EN 1992-1-2 Ontwerp en berekening van betonconstructies bij brand

#### Eurocode 3: Staalconstructies

NEN-EN 1993-1-1 Algemene regels en regels voor gebouwen

NEN-EN 1993-1-2 Staalconstructies bij brand

#### Eurocode 4: Staal- betonconstructies

NEN-EN 1994-1-1 Algemene regels en regels voor gebouwen

NEN-EN 1994-1-2 Staal- betonconstructies bij brand

#### Eurocode 5: Houtconstructies

NEN-EN 1995-1-1 Algemene regels en regels voor gebouwen

NEN-EN 1995-1-2 Houtconstructies bij brand

#### Eurocode 6: Constructies van metselwerk

NEN-EN 1996-1-1 Algemene regels voor constructies van gewapend en ongewapend metselwerk

NEN-EN 1996-1-2 Ontwerp en berekening van metselwerkconstructies bij brand

#### Eurocode 7: Geotechnisch ontwerp

NEN-EN 1997-1 Algemene regels

Bij alle voorschriften worden de laatste versies van de Nationale Bijlage (NB) gehanteerd.

#### 1.4 Gevolgklasse, betrouwbaarheidsklasse en belastingfactoren

|                         |         |
|-------------------------|---------|
| Ontwerplevensduur       | 50 jaar |
| Ontwerplevensduurklasse | 3       |
| Gevolgklasse            | CC2     |
| Betrouwbaarheidsklasse  | RC2     |

##### Belastingcategorieën en $\Psi$ -factoren

| Belasting                                                                                 | $\Psi_0$       | $\Psi_1$   | $\Psi_2$   |
|-------------------------------------------------------------------------------------------|----------------|------------|------------|
| Voorgeschreven belastingen in gebouwen, categorie                                         |                |            |            |
| Categorie A: woon- en verblijfsruimtes                                                    | 0,4            | 0,5        | 0,3        |
| Categorie B: kantoorruimtes                                                               | 0,5            | 0,5        | 0,3        |
| <b>Categorie C: bijeenkomstruimtes</b>                                                    | <b>0,6/0,4</b> | <b>0,7</b> | <b>0,6</b> |
| Categorie D: winkelfuncties                                                               | 0,4            | 0,7        | 0,6        |
| Categorie E: opslagruimtes                                                                | 1,0            | 0,9        | 0,8        |
| Categorie F: verkeersruimte, voertuiggewicht $\leq 30$ kN                                 | 0,7            | 0,7        | 0,6        |
| Categorie G: verkeersruimte, $30 \text{ kN} < \text{voertuiggewicht} \leq 160 \text{ kN}$ | 0,7            | 0,5        | 0,3        |
| <b>Categorie H: Daken</b>                                                                 | <b>0</b>       | <b>0</b>   | <b>0</b>   |
| <b>Sneeuwbelasting</b>                                                                    | <b>0</b>       | <b>0,2</b> | <b>0</b>   |
| <b>Windbelasting</b>                                                                      | <b>0</b>       | <b>0,2</b> | <b>0</b>   |
| Temperatuur (geen brand)                                                                  | 0              | 0,5        | 0          |

##### 1.4.1 Rekenwaarden van belastingen (STR/GEO) (Groep B)

| Blijvende en tijdelijke ontwerp situaties | Blijvende belastingen     |                          | Overheersend veranderlijke belasting | Veranderlijke belastingen gelijktijdig |                          |
|-------------------------------------------|---------------------------|--------------------------|--------------------------------------|----------------------------------------|--------------------------|
|                                           | Ongunstig                 | Gunstig                  |                                      | Belangrijkste                          | Andere                   |
| (verg. 6.10a)                             | $1,35 G_{k,j,\text{sup}}$ | $0,9 G_{k,j,\text{inf}}$ |                                      |                                        | $1,5 \Psi_{0,i} Q_{k,i}$ |
| (verg. 6.10.b)                            | $1,2 G_{k,j,\text{sup}}$  | $0,9 G_{k,j,\text{inf}}$ | $1,5 Q_{k,1}$                        |                                        | $1,5 \Psi_{0,i} Q_{k,i}$ |

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



#### 1.4.2 Rekenwaarden van belastingen bruikbaarheidsgrenstoestand

| Combinatie | <i>Blijvende belastingen</i> |                          | <i>Veranderlijke belastingen</i> |                          |
|------------|------------------------------|--------------------------|----------------------------------|--------------------------|
|            | Ongunstig                    | Gunstig                  | Overheersende                    | Andere                   |
| kenmerkend | $1,0 G_{k,j,\text{sup}}$     | $1,0 G_{k,j,\text{inf}}$ | $1,0 Q_{k,1}$                    | $1,0 \Psi_{0,i} Q_{k,i}$ |

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



## 1.5 Materialen

### 1.5.1 Beton

|                     |                          |   |                    |
|---------------------|--------------------------|---|--------------------|
| Betonkwaliteit      | In het werk gestort      | : | C 28/35            |
|                     | Prefab                   | : | C 35/45            |
| Betonstaalkwaliteit |                          | : | B500 B/C           |
| Milieuklasse        | Funderingsbalken         | : | XC 2 / XF 1        |
|                     | Poeren                   | : | XC 1 / XS 1 / XC 2 |
|                     | Kolommen                 | : | XC 2 / XS 2        |
|                     | Prefab beton             | : | XC 3 / XS 3        |
|                     | Vloeren (binnen)         | : | XC 1               |
|                     | Vloeren (buiten)         | : | XD 1 / XF 1        |
|                     | Vloeren (vloeistofdicht) | : | XC 4 / XD 3 / XA 1 |
|                     | Wanden                   | : | XD 2 / XF 2        |

### 1.5.2 Staal

|                                      |             |                                                    |
|--------------------------------------|-------------|----------------------------------------------------|
| Staalkwaliteit IPE, HE-profielen     | :           | S235JRG2                                           |
| Staalkwaliteit buizen                | gelast      | : S355JRH                                          |
|                                      | warmgewalst | : S355J2H                                          |
| Staalkwaliteit kokers                | koudgevormd | : S275J0H                                          |
|                                      | warmgewalst | : S275J2H                                          |
| Staalkwaliteit geïntegreerde liggers | :           | S355J2G3                                           |
| Boutkwaliteit                        | :           | 8.8 Thermisch verzinkt                             |
| Ankerkwaliteit                       | :           | 4.6 Gerolde draad, met haak, tenzij anders vermeld |

### 1.5.3 Hout

|               |   |               |
|---------------|---|---------------|
| Houtkwaliteit | : | C 18 bestaand |
|               |   | C 24 nieuw    |

### 1.5.4 Metselwerk

|                              |   |                        |
|------------------------------|---|------------------------|
| Steenkwaliteit               | : | Rode baksteen          |
| Druksterkte<br>(rekenwaarde) | : | 2,00 N/mm <sup>2</sup> |

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



## 1.6 Bijbehorende documenten

### 1.6.1 Tekeningen constructief

|           |                    |            |
|-----------|--------------------|------------|
| 240772-01 | Interne verbouwing | 18-12-2024 |
|-----------|--------------------|------------|

### 1.6.2 Tekeningen bouwkundig

|                   |            |
|-------------------|------------|
| Bestaand en nieuw | 08-11-2024 |
|-------------------|------------|

## 2 OVERZICHT BELASTINGEN

|                |       |                          |                             | kN/m <sup>2</sup> |
|----------------|-------|--------------------------|-----------------------------|-------------------|
| plat dak       | $g_k$ | dakhout en dakbalken     |                             | 0,35              |
|                |       | plafond                  |                             | 0,15              |
|                |       | dakbedekking             |                             | 0,10              |
|                |       | isolatie                 |                             | 0,05              |
|                |       |                          |                             | <hr/> 0,65        |
|                | $q_k$ | $\psi_0 = 0,00$          | extreem                     | 1,00              |
| schuin dak     | $g_k$ | dakhout en gordingen     |                             | 0,25              |
|                |       | plafond                  |                             | 0,15              |
|                |       | pannen                   |                             | 0,40              |
|                |       | <u>projectie</u>         |                             | <hr/> 0,80        |
|                | $q_k$ | $\psi_0 = 0,00$          | extreem                     | 0,00              |
| 3e verdieping  | $g_k$ | vloerhout en vloerbalken |                             | 0,35              |
|                |       | plafond                  |                             | 0,15              |
|                |       | afwerking                |                             | 0,40              |
|                |       |                          |                             | <hr/> 0,90        |
|                | $q_k$ | $\psi_0 = 0,40$          | extreem<br>scheidingswanden | 2,50<br>0,50      |
| d=110 baksteen | $g_k$ |                          |                             | 2,00              |
| d=220 baksteen | $g_k$ |                          |                             | 4,00              |
| hsb wand       | $g_k$ |                          |                             | 0,80              |
| kozijnen       | $g_k$ |                          |                             | 0,50              |

**Tabel NB.1 – 6.2 — Opgelegde belastingen op vloeren, balkons en trappen in gebouwen**

| Klasse van belaste oppervlakte                                                                                                                                                                                                                                                     | $q_k$<br>kN/m <sup>2</sup> | $Q_k$<br>kN    |
|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------------|----------------|
| <b>Klasse A</b> (wonen en huishoudelijk gebruik)                                                                                                                                                                                                                                   |                            |                |
| A-vloeren                                                                                                                                                                                                                                                                          | 1,75                       | 3 <sup>a</sup> |
| A-trappen                                                                                                                                                                                                                                                                          | 2,0                        | 3              |
| A-balkons                                                                                                                                                                                                                                                                          | 2,5                        | 3              |
| <b>Klasse B</b> (kantoorruimten)                                                                                                                                                                                                                                                   |                            |                |
| B-kantoorruimten                                                                                                                                                                                                                                                                   | 2,5                        | 3              |
| <b>Klasse C</b> (bijeenkomstruimten)                                                                                                                                                                                                                                               |                            |                |
| C1-tafels                                                                                                                                                                                                                                                                          | 4,0 <sup>b</sup>           | 7              |
| C2-vaste zitplaatsen                                                                                                                                                                                                                                                               | 4,0 <sup>b</sup>           | 7              |
| C3-zonder obstakels voor rondlopende mensen                                                                                                                                                                                                                                        | 5,0                        | 7              |
| C4-fysieke activiteiten                                                                                                                                                                                                                                                            | 5,0                        | 7              |
| C5-grote mensenmassa's                                                                                                                                                                                                                                                             | 5,0                        | 7              |
| <b>Klasse D</b> (winkelruimten)                                                                                                                                                                                                                                                    |                            |                |
| D1-kleinhandel                                                                                                                                                                                                                                                                     | 4,0                        | 7              |
| D2-warenhuizen                                                                                                                                                                                                                                                                     | 4,0                        | 7              |
| <sup>a</sup> De puntlasten moeten zijn aangebracht op een oppervlakte van 100 mm × 100 mm; de gegeven waarden moeten ook zijn gebruikt voor constructies van ondergeschikte betekenis.<br><sup>b</sup> Voor schoolgebouwen volstaat een vloerbelasting van 2,5 kN/m <sup>2</sup> . |                            |                |

## Winddrukken en windkrachten

versie 2023-01

### invoergegevens

|                                |            |          |
|--------------------------------|------------|----------|
| gebouwhoogte                   | h          | 19 m     |
| loodrecht op windrichting      | b          | 20 m     |
| parallel aan windrichting      | d          | 10 m     |
|                                | h/d        | 1,90     |
| windgebied (I, II, III):       |            | 2        |
| Bebouwd, Onbebouwd, Kust:      |            | B        |
| ontwerplevensduur              | t          | 50 jaar  |
| waarschijnlijkheidsfactor      | $C_{prob}$ | 1,00 -   |
| fundamentele basiswindsnelheid | $V_{b,o}$  | 27,0 m/s |
| basiswindsnelheid              | $V_b$      | 27,0 m/s |
| ruwheidsfactor                 | $C_{rz}$   | 0,81 -   |
|                                | $Z_o$      | 0,5 m    |
|                                | $Z_{min}$  | 7 m      |
| factor ruwheidslengte          | $k_r$      | 0,22 -   |
| gemiddelde windsnelheid        | $V_{m(z)}$ | 21,9 m/s |
| turbulentie intensiteit        | $L_v$      | 0,27     |

### resultaten

|                             |            |                        |
|-----------------------------|------------|------------------------|
| extreme stuwdruk            | $q_p(z_e)$ | 0,88 kN/m <sup>2</sup> |
| Zone D                      |            | 0,80                   |
| Zone E                      |            | -0,55                  |
| drukcoefficient ( zone D+E) | $C_{pe}$   | 1,35                   |
| winddruk op buitenzijde     | $w_e$      | 1,18 kN/m <sup>2</sup> |
| bouwwerkfactor              | $C_s C_d$  | 1                      |
| reductiefactor (EN1991-1-4) |            | 0,85                   |
| windbelasting               | $q_{p,k}$  | 1,00 kN/m <sup>2</sup> |

### 3 HOUTCONSTRUCTIE

#### 3.1 Balklaag dakkapel

Technosoft Construct release 6.74  
2024

18 dec

Project : 240772  
Onderdeel : balklagen  
Datum : 11/12/2024  
Eenheden : kN/m/rad  
Bestand : G:\.shortcut-targets-by-id\  
0ByYUb81WrbDqYlpOSXRzaHdIV0E\Projecten\2024\240772\  
Houtconstructie\balklagen.cnw

#### Toegepaste normen volgens Eurocode met Nederlandse NB

|             |                      |                 |              |
|-------------|----------------------|-----------------|--------------|
| Belastingen | NEN-EN 1990:2002     | C2:2010,A1:2019 | NB:2019 (nl) |
|             | NEN-EN 1991-1-1:2002 | C1/C11:2019     | NB:2019 (nl) |
|             | NEN-EN 1991-1-3:2003 | C1:2009         | NB:2011 (nl) |
|             | NEN-EN 1991-1-4:2005 | C2:2011         | NB:2011 (nl) |
| Hout        | NEN-EN 1995-1-1:2005 | A1:2011,C1:2006 | NB:2013 (nl) |
|             | NEN-EN 14080:2013    |                 |              |

#### Gording berekening. (H)

plattendak

#### Algemene gegevens

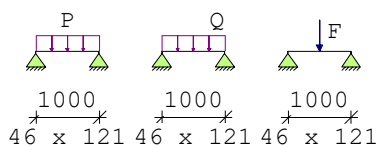
|                       |      |                         |                        |                      |          |
|-----------------------|------|-------------------------|------------------------|----------------------|----------|
| B x H                 | [mm] | : 46 x 121              | Sterkteklasse          | :                    | C24      |
| Overspanning          | [mm] | : 1000                  | Klimaatklasse          | :                    | I        |
| Aantal zijdl. steunen | :    | -                       | Referentie periode [j] | :                    | 50       |
| Opleglengte           | [mm] | : 100                   |                        |                      |          |
| Hoh in het dakvlak    | [mm] | : 600                   |                        |                      |          |
| Helling               | :    | 0.00                    |                        |                      |          |
| Beschot sterkteklasse | :    | C24                     |                        |                      |          |
| Dikte beschot         | [mm] | : 12                    | $E_{0,mean} \times I$  | [Nm <sup>2</sup> /m] | : 1584.0 |
| Windgebied            | :    | 2                       | Terrein                | :                    | Bebouwd  |
| Gebouw L x B x H      | [m]  | : 20.00 x 10.00 x 15.00 |                        |                      |          |

#### Permanente belastingen $G_{rep}$

|                             |   |       |
|-----------------------------|---|-------|
| EG balklaag                 | : | 0.35  |
| Isolatie                    | : | 0.10+ |
| Extra gewicht               | : | 0.30+ |
| Totaal [kN/m <sup>2</sup> ] | : | 0.75  |

#### Veranderlijke belastingen

|                           |                      |               |                                              |
|---------------------------|----------------------|---------------|----------------------------------------------|
| $Q_k$                     | [kN/m <sup>2</sup> ] | :             | 1.00                                         |
| $Q_k$                     | [kN/m]               | :             | 2.00                                         |
| $Q_k$                     | [kN]                 | :             | 1.50                                         |
| $Q_k$ oppervlak           | [m <sup>2</sup> ]    | : 0.10 x 0.10 |                                              |
| Reductiefactor            | :                    | 0.82          |                                              |
| Wind $Q_{p,prob}$         | [kN/m <sup>2</sup> ] | :             | 0.80 (= $C_{prob}^2 * Q_p = 1.00^2 * 0.80$ ) |
| Sneeuw vormfactor $\mu_1$ | :                    | 0.80          |                                              |



Belastingfactoren (NEN-EN 1990 - Bijlage A1.3)

Formule 6.10a:  $\gamma_G : 1.35$   $\gamma_Q : 1.50$

Formule 6.10b:  $\xi\gamma_G : 1.20$   $\gamma_Q : 1.50$

Perm.bel. gunstig : 0.90

Partiële factor (Tabel 2.3 NEN-EN 1995-1-1)

$\gamma_M [-] : 1.30$

### Stabiliteit

1.Toetsing kipstabiliteit m.b.t. montagefase volgens par.6.3.3. is n.v.t.:  
- u hebt het belastingsgeval 'Uitvoering' niet toegepast.

2.Factoren t.b.v. toetsing kipstabiliteit m.b.t. gebruiksfase volgens par.6.3.3:

Belastingcombinatie wind omhoog (opbuigend moment):

$\kappa_{crit,y} [-] : 1.00$  frm(6.34)

### Resultaten (maatgevende combinaties)

|                                                                                                                                                         |           |                                                                                                                               | eis                                  | u.c. |
|---------------------------------------------------------------------------------------------------------------------------------------------------------|-----------|-------------------------------------------------------------------------------------------------------------------------------|--------------------------------------|------|
| Geconc. belasting                                                                                                                                       | frm(6.13) | $\tau_{v,d} = 0.46$                                                                                                           | $< 2.46$ [N/mm <sup>2</sup> ]        | 0.19 |
| Geconc. belasting                                                                                                                                       | frm(6.3)  | $\sigma_{c,90,q,d} / (\kappa_{c,90,q} \cdot f_{c,90,d}) +$<br>$\sigma_{c,90,F,d} / (\kappa_{c,90,F} \cdot f_{c,90,d}) < 1.00$ | $= 0.06 / 1.54 + 0.49 / 2.31 = 0.25$ |      |
| Geconc. belasting                                                                                                                                       | frm(6.11) | $\sigma_{m,y,d} = 4.70$                                                                                                       | $< 15.42$ [N/mm <sup>2</sup> ]       | 0.30 |
| Let op: bij 1 of meerdere belastingcombinaties wind treedt een opwaartse oplegreactie op. Houdt hiermee rekening in het ontwerp van de oplegverbinding. |           |                                                                                                                               |                                      |      |

|          |               |          |          |      |      |
|----------|---------------|----------|----------|------|------|
| Lijnlast | $u_{bij}$     | $= 0.40$ | $< 4.00$ | [mm] | 0.10 |
| Lijnlast | $u_{net,fin}$ | $= 0.47$ | $< 4.00$ | [mm] | 0.12 |

**3.2 Slaper dakkapel****q1**

|          | $\psi_0$ | breedte | lengte | kN/m <sup>2</sup> | kN/m <sup>1</sup> |  | kN/m <sup>2</sup> | kN/m <sup>1</sup> |
|----------|----------|---------|--------|-------------------|-------------------|--|-------------------|-------------------|
| hsb wand |          | 1,00    | 2,20   | 0,80              | <u>1,76</u>       |  |                   |                   |
|          |          |         |        | $G_k =$           | 1,8               |  | $q_k =$           | 0,0               |

**q2**

|          | $\psi_0$ | breedte | lengte | kN/m <sup>2</sup> | kN/m <sup>1</sup> |       | kN/m <sup>2</sup> | kN/m <sup>1</sup> |
|----------|----------|---------|--------|-------------------|-------------------|-------|-------------------|-------------------|
| plat dak | 1        | 0,50    | 1,00   | 0,65              | <u>0,33</u>       | extr. | 1,00              | <u>0,50</u>       |
|          |          |         |        | $G_k =$           | 0,3               |       | $q_k =$           | 0,5               |

**q3**

|            | $\psi_0$ | breedte | lengte | kN/m <sup>2</sup> | kN/m <sup>1</sup> |      | kN/m <sup>2</sup> | kN/m <sup>1</sup> |
|------------|----------|---------|--------|-------------------|-------------------|------|-------------------|-------------------|
| schuin dak | 0        | 0,50    | 1,00   | 0,80              | <u>0,40</u>       | mom. | 0,00              | <u>0,00</u>       |
|            |          |         |        | $G_k =$           | 0,4               |      | $q_k =$           | 0,0               |

**q4**

|            | $\psi_0$ | breedte | lengte | kN/m <sup>2</sup> | kN/m <sup>1</sup> |      | kN/m <sup>2</sup> | kN/m <sup>1</sup> |
|------------|----------|---------|--------|-------------------|-------------------|------|-------------------|-------------------|
| schuin dak | 0        | 0,50    | 1,50   | 0,80              | <u>0,60</u>       | mom. | 0,00              | <u>0,00</u>       |
|            |          |         |        | $G_k =$           | 0,6               |      | $q_k =$           | 0,0               |

Technosoft Raamwerken release 6.82  
2024

18 dec

Project.....: 240772  
Onderdeel.....: slaper dakkapel  
Dimensies.....: kN;m;rad (tenzij anders aangegeven)  
Datum.....: 18/12/2024  
Bestand.....: G:\.shortcut-targets-by-id\0ByYUb81WrbDqYlpOSXRzaHdIV0E\  
Projecten\2024\240772\Houtconstructie\slaper dakkapel.rww

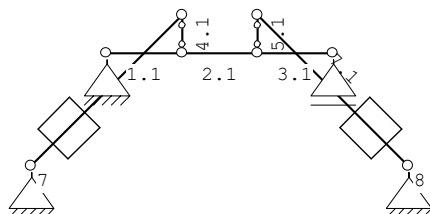
Belastingbreedte.: 1.500  
Rekenmodel.....: 2e-orde-elastisch.  
Theorieën voor de bepaling van de krachtsverdeling:  
1) Uiterste grenstoestand:  
Geometrisch niet lineair alle staven.  
Fysisch lineair alle staven.  
2) Gebruiksgrenstoestand:  
Lineaire-elasticiteitstheorie  
  
Maximum aantal iteraties.....: 50  
Max.deellengte kolommen/wanden: 0.500 Max.deellengte balken/vloeren: 0.500  
Max. X-verplaatsing in UGT.....: 0.500 Max. Z-verplaatsing in UGT....: 0.250

Gunstige werking van de permanente belasting wordt automatisch verwerkt.

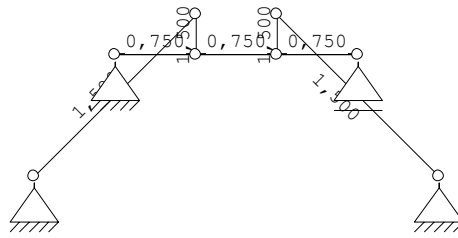
#### Toegepaste normen volgens Eurocode met Nederlandse NB

|             |                      |                 |             |
|-------------|----------------------|-----------------|-------------|
| Belastingen | NEN-EN 1990:2002     | C2:2010,A1:2019 | NB:2019(nl) |
|             | NEN-EN 1991-1-1:2002 | C1/C11:2019     | NB:2019(nl) |
|             | NEN-EN 1991-1-4:2005 | C2:2011         | NB:2011(nl) |
| Hout        | NEN-EN 1995-1-1:2005 | A1:2011,C1:2006 | NB:2013(nl) |

#### GEOMETRIE



#### BELASTINGBREEDTEN



Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



Project.....: 240772  
Onderdeel.....: slaper dakkapel

#### MATERIALEN

| Mt | Kwaliteit | E-modulus [N/mm <sup>2</sup> ] | S.G. | S.G.verhoogd | Pois. | Uitz. coëff |
|----|-----------|--------------------------------|------|--------------|-------|-------------|
| 1  | C24       | 11000                          | 3.5  | 4.2          | 1.00  | 5.0000e-06  |
| 2  | C20       | 9500                           | 3.3  | 4.0          | 1.00  | 5.0000e-06  |

Bij de bepaling v.h. e.g. van houten staven is de S.G.verhoogd toegepast.

#### PROFIELEN [mm]

| Prof. | Omschrijving | Materiaal | Oppervlak  | Traagheid  | Vormf. |
|-------|--------------|-----------|------------|------------|--------|
| 1     | B*H 157*150  | 2:C20     | 2.3550e+04 | 4.4156e+07 | 0.00   |
| 2     | B*H 160*200  | 2:C20     | 3.2000e+04 | 1.0667e+08 | 0.00   |

#### PROFIELEN vervolg [mm]

| Prof. | Staaftype | Breedte | Hoogte | e     | Type | b1 | h1 | b2 | h2 |
|-------|-----------|---------|--------|-------|------|----|----|----|----|
| 1     | 0:Normaal | 157     | 150    | 75.0  | 0:RH |    |    |    |    |
| 2     | 0:Normaal | 160     | 200    | 100.0 | 0:RH |    |    |    |    |

#### PROFIELVORMEN [mm]

1 B\*H 157\*150



2 B\*H 160\*200



#### KNOPEN

| Knoop | X     | Z      | Knoop | X      | Z      |
|-------|-------|--------|-------|--------|--------|
| 1     | 0.000 | 14.500 | 6     | 2.000  | 15.000 |
| 2     | 3.000 | 14.500 | 7     | -1.000 | 13.000 |
| 3     | 1.000 | 14.500 | 8     | 4.000  | 13.000 |
| 4     | 2.000 | 14.500 |       |        |        |
| 5     | 1.000 | 15.000 |       |        |        |

#### STAVEN

| St. | ki | kj | Profiel       | Aansl.i | Aansl.j | Lengte | Opm. |
|-----|----|----|---------------|---------|---------|--------|------|
| 1   | 1  | 3  | 1:B*H 157*150 | NDM     | NDM     | 1.000  |      |
| 2   | 3  | 4  | 1:B*H 157*150 | NDM     | NDM     | 1.000  |      |
| 3   | 4  | 2  | 1:B*H 157*150 | NDM     | NDM     | 1.000  |      |
| 4   | 3  | 5  | 1:B*H 157*150 | ND-     | ND-     | 0.500  |      |
| 5   | 4  | 6  | 1:B*H 157*150 | ND-     | ND-     | 0.500  |      |
| 6   | 7  | 5  | 1:B*H 157*150 | NDM     | NDM     | 2.828  |      |
| 7   | 8  | 6  | 1:B*H 157*150 | NDM     | NDM     | 2.828  |      |

#### VASTE STEUNPUNTEN

| Nr. | knoop | Kode | XZR | 1=vast | 0=vrij | Hoek |
|-----|-------|------|-----|--------|--------|------|
| 1   | 1     | 110  |     |        |        | 0.00 |
| 2   | 2     | 010  |     |        |        | 0.00 |
| 3   | 7     | 110  |     |        |        | 0.00 |
| 4   | 8     | 110  |     |        |        | 0.00 |

Project.....: 240772  
 Onderdeel....: slaper dakkapel

**BELASTINGBREEDTEN**

| Staaft | Breedte-i | Breedte-j | Staaft | Breedte-i | Breedte-j |
|--------|-----------|-----------|--------|-----------|-----------|
| 1      | 0.750     | 0.750     | 6      | 1.500     | 1.500     |
| 2      | 0.750     | 0.750     | 7      | 1.500     | 1.500     |
| 3      | 0.750     | 0.750     |        |           |           |
| 4      | 1.500     | 1.500     |        |           |           |
| 5      | 1.500     | 1.500     |        |           |           |

**BELASTINGGENERATIE ALGEMEEN.**

|                              |      |                         |       |
|------------------------------|------|-------------------------|-------|
| Betrouwbaarheidsklasse.....: | 2    | Referentieperiode.....: | 50    |
| Gebouwdiepte.....:           | 8.00 | Gebouwhoogte.....:      | 15.00 |
| Niveau aansl.terrein.....:   | 0.00 | E.g. scheid.w. [kN/m2]: | 0.00  |

**WIND**

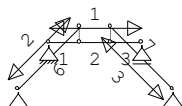
|                                   |         |                        |        |
|-----------------------------------|---------|------------------------|--------|
| Terrein categorie ...[4.3.2]....  | Bebouwd |                        |        |
| Windgebied .....                  | 2       | Vb,0 ..[4.2].....      | 27.000 |
| Positie spant in het gebouw....   | 0.000   | Kr ....[4.3.2].....    | 0.223  |
| z0 .....                          | 0.500   | Zmin ..[4.3.2].....    | 7.000  |
| Co wind van links ..[4.3.3]....   | 1.000   | Co wind van rechts.... | 1.000  |
| Co wind loodrecht ..[4.3.3]....   | 1.000   |                        |        |
| Cpi wind van links ..[7.2.9]....  | 0.200   | -0.300                 |        |
| Cpi windloodrecht ...[7.2.9]....  | 0.200   | -0.300                 |        |
| Cpi wind van rechts ..[7.2.9].... | 0.200   | -0.300                 |        |
| Cfr windwrijving ....[7.5].....   | 0.040   |                        |        |

**STAIFTYPEN**

| Type    | staven      |
|---------|-------------|
| 7:Dak.  | : 1-3, 6, 7 |
| 9:Open. | : 4, 5      |

**LASTVELDEN**

Veranderlijke belastingen door personen

**LASTVELDEN**

| Nr | Staaft | Tabel | Klasse-Gebruiksfunctie    | Verd. | q <sub>k</sub> | Q <sub>k</sub> | F <sub>t</sub> / F <sub>t,0</sub> |
|----|--------|-------|---------------------------|-------|----------------|----------------|-----------------------------------|
| 1  | 1-3    | 6.10  | H-Dak (onder dakbeschoot) | 1     | -1.00          | -2.00          | 1.00                              |
| 2  | 6-6    | 6.10  | H-Dak (onder dakbeschoot) | 0     | 0.00           | -2.00          | 1.00                              |
| 3  | 7-7    | 6.10  | H-Dak (onder dakbeschoot) | 0     | 0.00           | -2.00          | 1.00                              |

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

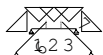
Revisie

IRg

Project.....: 240772  
Onderdeel....: slaper dakkapel

## LASTVELDEN

Wind staven Sneeuw staven

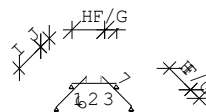
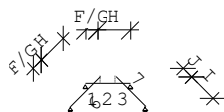


## WIND DAKTYPES

| Nr. | Staaft Type  | reductie bij<br>wind van links | reductie bij<br>wind van rechts | Cpe volgens art: |
|-----|--------------|--------------------------------|---------------------------------|------------------|
| 1   | 6 Zadel dak  | 1.000                          | 1.000                           | 7.2.5            |
| 2   | 1-3 Plat dak | 1.000                          | 1.000                           | 7.2.3            |
| 3   | 7 Zadel dak  | 1.000                          | 1.000                           | 7.2.5            |

## WIND ZONES

Wind van links Wind van rechts



## WIND VAN LINKS ZONES

| Nr. | Staaft | Positie | Lengte | Zone |
|-----|--------|---------|--------|------|
| 1   | 6      | 0.000   | 0.800  | F/G  |
| 2   | 6      | 0.800   | 2.028  | H    |
| 3   | 1-3    | 0.000   | 0.800  | F/G  |
| 4   | 1-3    | 0.800   | 2.200  | H    |
| 5   | 7      | 0.000   | 0.800  | J    |
| 6   | 7      | 0.800   | 2.028  | I    |

## WIND VAN RECHTS ZONES

| Nr. | Staaft | Positie | Lengte | Zone |
|-----|--------|---------|--------|------|
| 1   | 7      | 0.000   | 0.800  | F/G  |
| 2   | 7      | 0.800   | 2.028  | H    |
| 3   | 1-3    | 0.000   | 0.800  | F/G  |
| 4   | 1-3    | 0.800   | 2.200  | H    |
| 5   | 6      | 0.000   | 0.800  | J    |
| 6   | 6      | 0.800   | 2.028  | I    |

## Wind indexen

| Index | CsCd | Cpe/Cpi | qp    | breedte | reductie | Qw     | Zone | Hoek(en) |
|-------|------|---------|-------|---------|----------|--------|------|----------|
| Qw1   |      | 0.300   | 0.802 | 1.500   |          | -0.361 | -i   |          |
| Qw2   |      | 0.300   | 0.802 | 0.750   |          | -0.180 | -i   |          |
| Qw3   |      | -0.300  | 0.802 | 1.500   |          | 0.361  | -i   |          |
| Qw4   | 1.00 | 0.700   | 0.802 | 1.500   |          | -0.842 | F    | 45.0     |
| Qw5   | 1.00 | 0.600   | 0.802 | 1.500   |          | -0.721 | H    | 45.0     |
| Qw6   | 1.00 | -1.800  | 0.802 | 0.750   |          | 1.082  | F    | 0.0      |
| Qw7   | 1.00 | -0.700  | 0.802 | 0.750   |          | 0.421  | H    | 0.0      |
| Qw8   | 1.00 | 0.300   | 0.802 | 1.500   |          | -0.361 | J    | 45.0     |
| Qw9   | 1.00 | 0.200   | 0.802 | 1.500   |          | -0.240 | I    | 45.0     |
| Qw10  |      | -0.200  | 0.802 | 1.500   |          | 0.240  | +i   |          |

Project.....: 240772  
 Onderdeel.....: slaper dakkapel

**Wind indexen**

| Index | CsCd | Cpe/Cpi | qp    | breedte | reductie | Qw     | Zone | Hoek(en) |
|-------|------|---------|-------|---------|----------|--------|------|----------|
| Qw11  |      | -0.200  | 0.802 | 0.750   |          | 0.120  | +i   |          |
| Qw12  |      | 0.200   | 0.802 | 1.500   |          | -0.240 | +i   |          |
| Qw13  | 1.00 | -0.700  | 0.802 | 1.500   |          | 0.842  | F    | 45.0     |
| Qw14  | 1.00 | -0.600  | 0.802 | 1.500   |          | 0.721  | H    | 45.0     |
| Qw15  | 1.00 | -0.300  | 0.802 | 1.500   |          | 0.361  | J    | 45.0     |
| Qw16  | 1.00 | -0.200  | 0.802 | 1.500   |          | 0.240  | I    | 45.0     |

**BELASTINGGEVALLEN**

| B.G. | Omschrijving                    | Type |
|------|---------------------------------|------|
|      | 1 Permanente belasting EGZ=0.00 | 1    |
|      | 2 Ver. bel. pers. ed. ( $q_k$ ) | 2    |
| g    | 3 Ver. bel. pers. ed. ( $Q_k$ ) | 3    |
| g    | 4 Wind van links onderdruk A    | 7    |
| g    | 5 Wind van links overdruk A     | 8    |
| g    | 6 Wind van links onderdruk B    | 9    |
| g    | 7 Wind van links overdruk B     | 10   |
| g    | 8 Wind van links onderdruk C    | 37   |
| g    | 9 Wind van links overdruk C     | 38   |
| g    | 10 Wind van links onderdruk D   | 39   |
| g    | 11 Wind van links overdruk D    | 40   |
| g    | 12 Wind van rechts onderdruk A  | 11   |
| g    | 13 Wind van rechts overdruk A   | 12   |
| g    | 14 Wind van rechts onderdruk B  | 13   |
| g    | 15 Wind van rechts overdruk B   | 14   |
| g    | 16 Wind van rechts onderdruk C  | 41   |
| g    | 17 Wind van rechts overdruk C   | 42   |
| g    | 18 Wind van rechts onderdruk D  | 43   |
| g    | 19 Wind van rechts overdruk D   | 44   |

g = gegenereerd belastinggeval

**BELASTINGGEVALLEN vervolg**

| B.G. | Omschrijving                    | Belastingduurklasse |
|------|---------------------------------|---------------------|
|      | 1 Permanente belasting          | Blijvend            |
|      | 2 Ver. bel. pers. ed. ( $q_k$ ) | Middellang          |
|      | 3 Ver. bel. pers. ed. ( $Q_k$ ) | Middellang          |
|      | 4 Wind van links onderdruk A    | Kort                |
|      | 5 Wind van links overdruk A     | Kort                |
|      | 6 Wind van links onderdruk B    | Kort                |
|      | 7 Wind van links overdruk B     | Kort                |
|      | 8 Wind van links onderdruk C    | Kort                |
|      | 9 Wind van links overdruk C     | Kort                |
|      | 10 Wind van links onderdruk D   | Kort                |
|      | 11 Wind van links overdruk D    | Kort                |
|      | 12 Wind van rechts onderdruk A  | Kort                |
|      | 13 Wind van rechts overdruk A   | Kort                |
|      | 14 Wind van rechts onderdruk B  | Kort                |
|      | 15 Wind van rechts overdruk B   | Kort                |
|      | 16 Wind van rechts onderdruk C  | Kort                |
|      | 17 Wind van rechts overdruk C   | Kort                |
|      | 18 Wind van rechts onderdruk D  | Kort                |
|      | 19 Wind van rechts overdruk D   | Kort                |

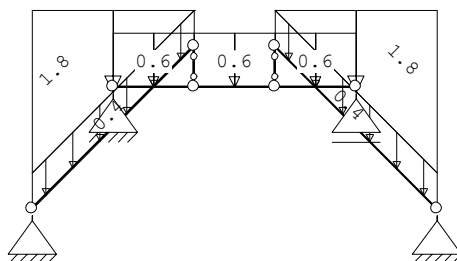
Project.....: 240772

Onderdeel.....: slaper dakkapel

**BELASTINGEN**

B.G:1 Permanente

belasting

**STAAFBELASTINGEN**

B.G:1 Permanente

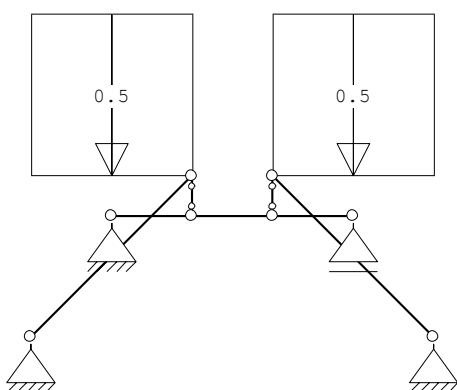
belasting

| Staat | Type        | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|-------|-------------|--------|-------|-------|-------|----------|----------|----------|
| 6     | 5:QZGloaal  | -1.80  | 0.00  | 0.000 | 0.000 |          |          |          |
| 7     | 5:QZGloaal  | -1.80  | 0.00  | 0.000 | 0.000 |          |          |          |
| 6     | 3:QZgeProj. | -0.30  | -0.30 | 0.000 | 0.000 |          |          |          |
| 7     | 3:QZgeProj. | -0.30  | -0.30 | 0.000 | 0.000 |          |          |          |
| 6     | 5:QZGloaal  | -0.40  | -0.40 | 0.000 | 0.000 |          |          |          |
| 7     | 5:QZGloaal  | -0.40  | -0.40 | 0.000 | 0.000 |          |          |          |
| 1     | 1:QZLokaal  | -0.60  | -0.60 | 0.000 | 0.000 |          |          |          |
| 2     | 1:QZLokaal  | -0.60  | -0.60 | 0.000 | 0.000 |          |          |          |
| 3     | 1:QZLokaal  | -0.60  | -0.60 | 0.000 | 0.000 |          |          |          |

**BELASTINGEN**

B.G:2 Ver. bel. pers. ed.

(q\_k)



Project.....: 240772

Onderdeel.....: slaper dakkapel

**STAAFBELASTINGEN**

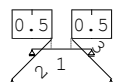
B.G:2 Ver. bel. pers. ed.

(q<sub>k</sub>)

| Staaftype | Type        | q1/p/m | q2    | A     | B     | ψ <sub>0</sub> | ψ <sub>1</sub> | ψ <sub>2</sub> |
|-----------|-------------|--------|-------|-------|-------|----------------|----------------|----------------|
| 6         | 3:QZgeProj. | -0.50  | -0.50 | 0.000 | 0.000 | 0.00           | 0.00           | 0.00           |
| 7         | 3:QZgeProj. | -0.50  | -0.50 | 0.000 | 0.000 | 0.00           | 0.00           | 0.00           |

**SITUATIES BELAST/ONBELAST**

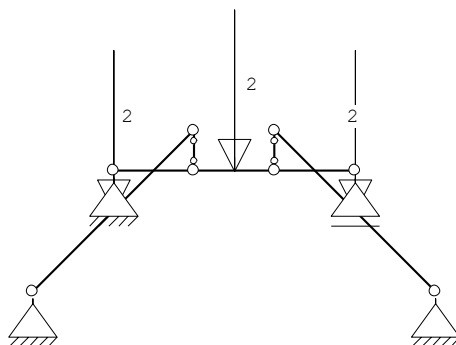
B.G:2 Ver. bel. pers. ed.

(q<sub>k</sub>)**SITUATIES BELAST/ONBELAST**Belastingtype: q<sub>k</sub>

| Nr | Lastvelden belast | Lastvelden onbelast |
|----|-------------------|---------------------|
| 1  | 1-3               |                     |

**BELASTINGEN**

B.G:3 Ver. bel. pers. ed.

(Q<sub>k</sub>)**STAAFBELASTINGEN**

B.G:3 Ver. bel. pers. ed.

(Q<sub>k</sub>)

| Staaftype | Type            | q1/p/m | q2 | A     | B | ψ <sub>0</sub> | ψ <sub>1</sub> | ψ <sub>2</sub> |
|-----------|-----------------|--------|----|-------|---|----------------|----------------|----------------|
| 2         | 10:PZGeproproj. | -2.00  |    | 0.500 |   | 0.00           | 0.00           | 0.00           |
| 6         | 10:PZGeproproj. | -2.00  |    | 1.414 |   | 0.00           | 0.00           | 0.00           |
| 7         | 10:PZGeproproj. | -2.00  |    | 1.414 |   | 0.00           | 0.00           | 0.00           |

Project

Rustenburgerstraat 246 Franse School

Projectnummer

240772

Revisie

IRg

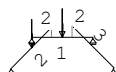
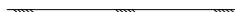
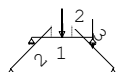
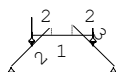
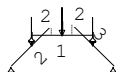
Project.....: 240772

Onderdeel.....: slaper dakkapel

### SITUATIES BELAST/ONBELAST

B.G:3 Ver. bel. pers. ed.

(Q<sub>k</sub>)



### SITUATIES BELAST/ONBELAST

Belastingtype: Q<sub>k</sub>

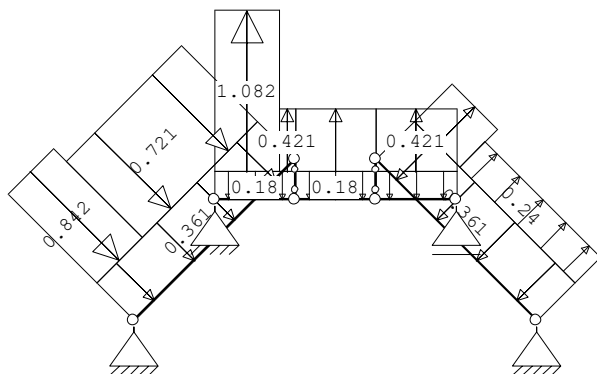
| Nr Lastvelden belast | Lastvelden onbelast |
|----------------------|---------------------|
| 1 1-3                |                     |
| 2 2,3                | 1                   |
| 3 1,3                | 2                   |
| 4 1,2                | 3                   |

Project.....: 240772  
 Onderdeel.....: slaper dakkapel

**BELASTINGEN**

B.G:4 Wind van links

onderdruk A

**STAAFBELASTINGEN**

B.G:4 Wind van links

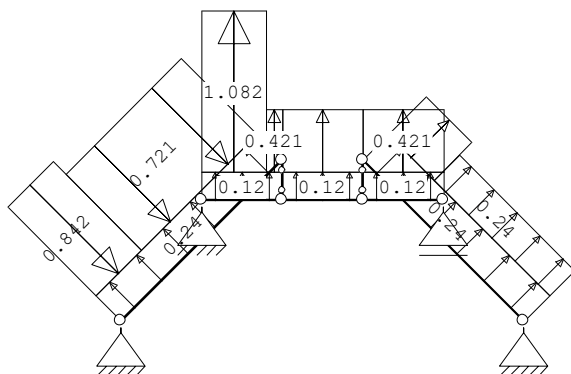
onderdruk A

| Staaftype | Type       | Index | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|-----------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 6         | 1:QZLokaal | Qw1   | -0.36  | -0.36 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1         | 1:QZLokaal | Qw2   | -0.18  | -0.18 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2         | 1:QZLokaal | Qw2   | -0.18  | -0.18 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3         | 1:QZLokaal | Qw2   | -0.18  | -0.18 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7         | 1:QZLokaal | Qw3   | 0.36   | 0.36  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 6         | 1:QZLokaal | Qw4   | -0.84  | -0.84 | 0.000 | 2.028 | 0.00     | 0.20     | 0.00     |
| 6         | 1:QZLokaal | Qw5   | -0.72  | -0.72 | 0.800 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1         | 1:QZLokaal | Qw6   | 1.08   | 1.08  | 0.000 | 0.200 | 0.00     | 0.20     | 0.00     |
| 1         | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.800 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2         | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3         | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7         | 1:QZLokaal | Qw8   | -0.36  | -0.36 | 2.028 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7         | 1:QZLokaal | Qw9   | -0.24  | -0.24 | 0.000 | 0.800 | 0.00     | 0.20     | 0.00     |

**BELASTINGEN**

B.G:5 Wind van links

overdruk A



Project.....: 240772

Onderdeel....: slaper dakkapel

**STAAFBELASTINGEN**

B.G:5 Wind van links

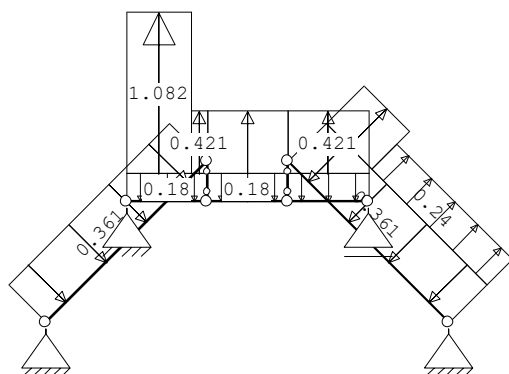
overdruk A

| Staaft | Type       | Index | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|--------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 6      | 1:QZLokaal | Qw10  | 0.24   | 0.24  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1      | 1:QZLokaal | Qw11  | 0.12   | 0.12  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2      | 1:QZLokaal | Qw11  | 0.12   | 0.12  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3      | 1:QZLokaal | Qw11  | 0.12   | 0.12  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7      | 1:QZLokaal | Qw12  | -0.24  | -0.24 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 6      | 1:QZLokaal | Qw4   | -0.84  | -0.84 | 0.000 | 2.028 | 0.00     | 0.20     | 0.00     |
| 6      | 1:QZLokaal | Qw5   | -0.72  | -0.72 | 0.800 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1      | 1:QZLokaal | Qw6   | 1.08   | 1.08  | 0.000 | 0.200 | 0.00     | 0.20     | 0.00     |
| 1      | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.800 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2      | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3      | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7      | 1:QZLokaal | Qw8   | -0.36  | -0.36 | 2.028 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7      | 1:QZLokaal | Qw9   | -0.24  | -0.24 | 0.000 | 0.800 | 0.00     | 0.20     | 0.00     |

**BELASTINGEN**

B.G:6 Wind van links

onderdruk B

**STAAFBELASTINGEN**

B.G:6 Wind van links

onderdruk B

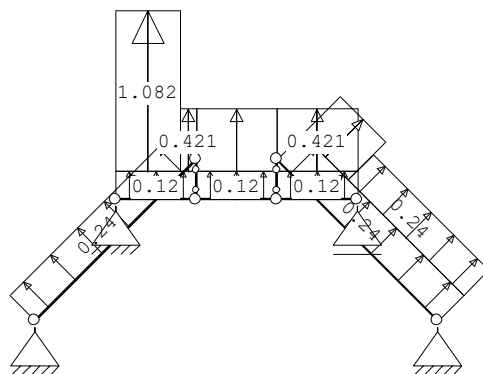
| Staaft | Type       | Index | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|--------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 6      | 1:QZLokaal | Qw1   | -0.36  | -0.36 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1      | 1:QZLokaal | Qw2   | -0.18  | -0.18 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2      | 1:QZLokaal | Qw2   | -0.18  | -0.18 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3      | 1:QZLokaal | Qw2   | -0.18  | -0.18 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7      | 1:QZLokaal | Qw3   | 0.36   | 0.36  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1      | 1:QZLokaal | Qw6   | 1.08   | 1.08  | 0.000 | 0.200 | 0.00     | 0.20     | 0.00     |
| 1      | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.800 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2      | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3      | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7      | 1:QZLokaal | Qw8   | -0.36  | -0.36 | 2.028 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7      | 1:QZLokaal | Qw9   | -0.24  | -0.24 | 0.000 | 0.800 | 0.00     | 0.20     | 0.00     |

Project.....: 240772  
 Onderdeel.....: slaper dakkapel

**BELASTINGEN**

B.G:7 Wind van links

overdruk B

**STAAFBELASTINGEN**

B.G:7 Wind van links

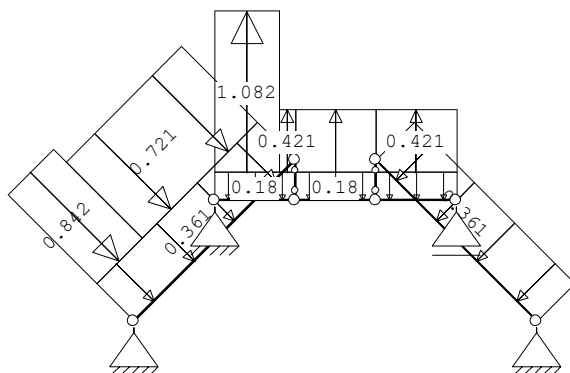
overdruk B

| Staaft | Type       | Index | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|--------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 6      | 1:QZLokaal | Qw10  | 0.24   | 0.24  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1      | 1:QZLokaal | Qw11  | 0.12   | 0.12  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2      | 1:QZLokaal | Qw11  | 0.12   | 0.12  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3      | 1:QZLokaal | Qw11  | 0.12   | 0.12  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7      | 1:QZLokaal | Qw12  | -0.24  | -0.24 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1      | 1:QZLokaal | Qw6   | 1.08   | 1.08  | 0.000 | 0.200 | 0.00     | 0.20     | 0.00     |
| 1      | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.800 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2      | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3      | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7      | 1:QZLokaal | Qw8   | -0.36  | -0.36 | 2.028 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7      | 1:QZLokaal | Qw9   | -0.24  | -0.24 | 0.000 | 0.800 | 0.00     | 0.20     | 0.00     |

**BELASTINGEN**

B.G:8 Wind van links

onderdruk C

**STAAFBELASTINGEN**

B.G:8 Wind van links

onderdruk C

| Staaft | Type       | Index | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|--------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 6      | 1:QZLokaal | Qw1   | -0.36  | -0.36 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1      | 1:QZLokaal | Qw2   | -0.18  | -0.18 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2      | 1:QZLokaal | Qw2   | -0.18  | -0.18 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3      | 1:QZLokaal | Qw2   | -0.18  | -0.18 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7      | 1:QZLokaal | Qw3   | 0.36   | 0.36  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 6      | 1:QZLokaal | Qw4   | -0.84  | -0.84 | 0.000 | 2.028 | 0.00     | 0.20     | 0.00     |
| 6      | 1:QZLokaal | Qw5   | -0.72  | -0.72 | 0.800 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1      | 1:QZLokaal | Qw6   | 1.08   | 1.08  | 0.000 | 0.200 | 0.00     | 0.20     | 0.00     |

Project.....: 240772

Onderdeel.....: slaper dakkapel

**STAAFBELASTINGEN**

B.G:8 Wind van links

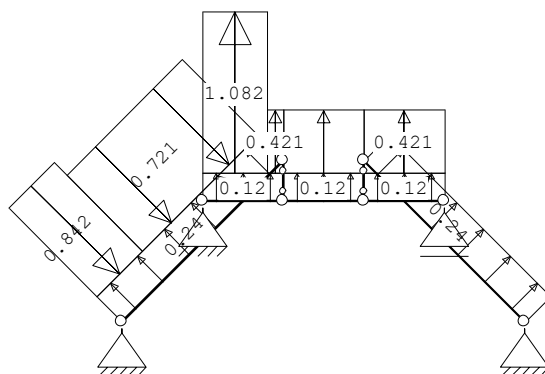
onderdruk C

| Staaft | Type       | Index | q1/p/m | q2   | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|--------|------------|-------|--------|------|-------|-------|----------|----------|----------|
| 1      | 1:QZLokaal | Qw7   | 0.42   | 0.42 | 0.800 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2      | 1:QZLokaal | Qw7   | 0.42   | 0.42 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3      | 1:QZLokaal | Qw7   | 0.42   | 0.42 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |

**BELASTINGEN**

B.G:9 Wind van links

overdruk C

**STAAFBELASTINGEN**

B.G:9 Wind van links

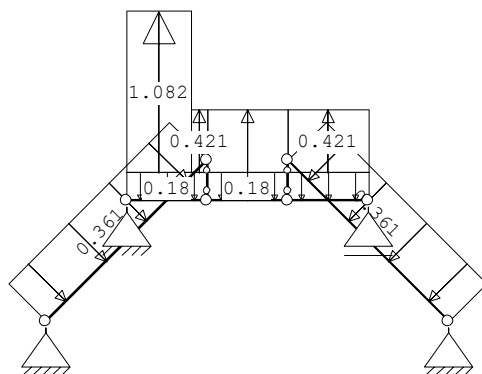
overdruk C

| Staaft | Type       | Index | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|--------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 6      | 1:QZLokaal | Qw10  | 0.24   | 0.24  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1      | 1:QZLokaal | Qw11  | 0.12   | 0.12  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2      | 1:QZLokaal | Qw11  | 0.12   | 0.12  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3      | 1:QZLokaal | Qw11  | 0.12   | 0.12  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7      | 1:QZLokaal | Qw12  | -0.24  | -0.24 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 6      | 1:QZLokaal | Qw4   | -0.84  | -0.84 | 0.000 | 2.028 | 0.00     | 0.20     | 0.00     |
| 6      | 1:QZLokaal | Qw5   | -0.72  | -0.72 | 0.800 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1      | 1:QZLokaal | Qw6   | 1.08   | 1.08  | 0.000 | 0.200 | 0.00     | 0.20     | 0.00     |
| 1      | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.800 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2      | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3      | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |

**BELASTINGEN**

B.G:10 Wind van links

onderdruk D



Project.....: 240772  
 Onderdeel.....: slaper dakkapel

**STAAFBELASTINGEN**

B.G:10 Wind van links

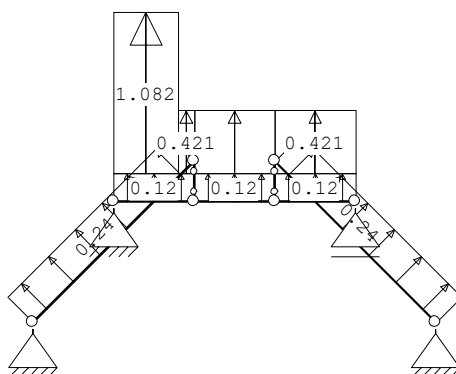
onderdruk D

| Staaf | Type       | Index | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|-------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 6     | 1:QZLokaal | Qw1   | -0.36  | -0.36 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw2   | -0.18  | -0.18 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2     | 1:QZLokaal | Qw2   | -0.18  | -0.18 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3     | 1:QZLokaal | Qw2   | -0.18  | -0.18 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7     | 1:QZLokaal | Qw3   | 0.36   | 0.36  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw6   | 1.08   | 1.08  | 0.000 | 0.200 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.800 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2     | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3     | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |

**BELASTINGEN**

B.G:11 Wind van links

overdruk D

**STAAFBELASTINGEN**

B.G:11 Wind van links

overdruk D

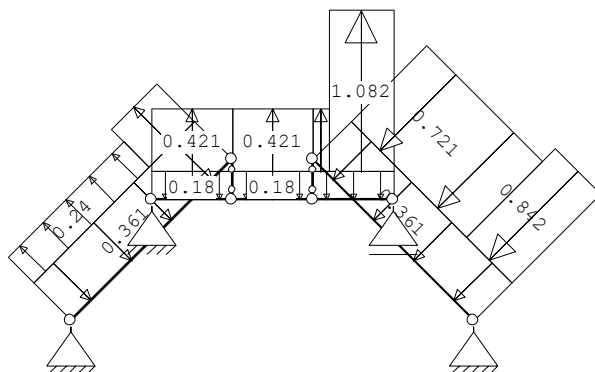
| Staaf | Type       | Index | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|-------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 6     | 1:QZLokaal | Qw10  | 0.24   | 0.24  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw11  | 0.12   | 0.12  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2     | 1:QZLokaal | Qw11  | 0.12   | 0.12  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3     | 1:QZLokaal | Qw11  | 0.12   | 0.12  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7     | 1:QZLokaal | Qw12  | -0.24  | -0.24 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw6   | 1.08   | 1.08  | 0.000 | 0.200 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.800 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2     | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3     | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |

Project.....: 240772  
 Onderdeel.....: slaper dakkapel

**BELASTINGEN**

B.G:12 Wind van rechts

onderdruk A

**STAAFBELASTINGEN**

B.G:12 Wind van rechts

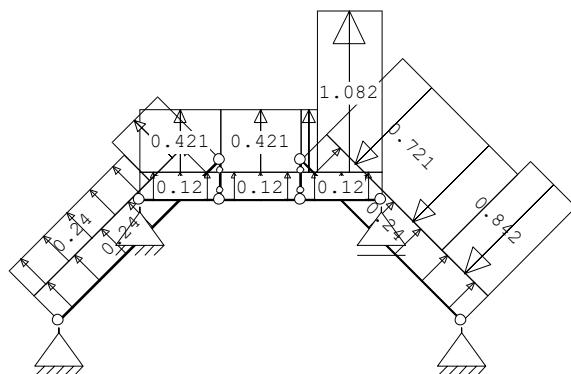
onderdruk A

| Staaftype | Type       | Index | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|-----------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 6         | 1:QZLokaal | Qw1   | -0.36  | -0.36 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1         | 1:QZLokaal | Qw2   | -0.18  | -0.18 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2         | 1:QZLokaal | Qw2   | -0.18  | -0.18 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3         | 1:QZLokaal | Qw2   | -0.18  | -0.18 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7         | 1:QZLokaal | Qw3   | 0.36   | 0.36  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7         | 1:QZLokaal | Qw13  | 0.84   | 0.84  | 0.000 | 2.028 | 0.00     | 0.20     | 0.00     |
| 7         | 1:QZLokaal | Qw14  | 0.72   | 0.72  | 0.800 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3         | 1:QZLokaal | Qw6   | 1.08   | 1.08  | 0.200 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3         | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.000 | 0.800 | 0.00     | 0.20     | 0.00     |
| 2         | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1         | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 6         | 1:QZLokaal | Qw15  | 0.36   | 0.36  | 2.028 | 0.000 | 0.00     | 0.20     | 0.00     |
| 6         | 1:QZLokaal | Qw16  | 0.24   | 0.24  | 0.000 | 0.800 | 0.00     | 0.20     | 0.00     |

**BELASTINGEN**

B.G:13 Wind van rechts

overdruk A



Project.....: 240772

Onderdeel.....: slaper dakkapel

**STAAFBELASTINGEN**

B.G:13 Wind van rechts

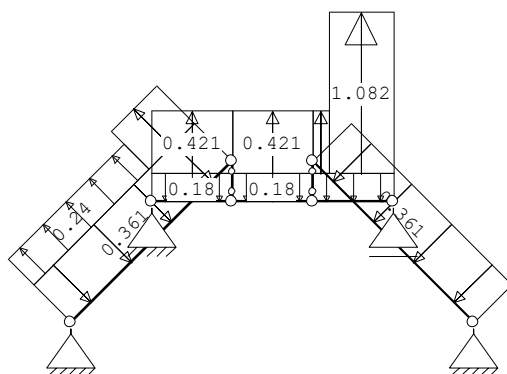
overdruk A

| Staaft | Type       | Index | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|--------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 6      | 1:QZLokaal | Qw10  | 0.24   | 0.24  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1      | 1:QZLokaal | Qw11  | 0.12   | 0.12  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2      | 1:QZLokaal | Qw11  | 0.12   | 0.12  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3      | 1:QZLokaal | Qw11  | 0.12   | 0.12  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7      | 1:QZLokaal | Qw12  | -0.24  | -0.24 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7      | 1:QZLokaal | Qw13  | 0.84   | 0.84  | 0.000 | 2.028 | 0.00     | 0.20     | 0.00     |
| 7      | 1:QZLokaal | Qw14  | 0.72   | 0.72  | 0.800 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3      | 1:QZLokaal | Qw6   | 1.08   | 1.08  | 0.200 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3      | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.000 | 0.800 | 0.00     | 0.20     | 0.00     |
| 2      | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1      | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 6      | 1:QZLokaal | Qw15  | 0.36   | 0.36  | 2.028 | 0.000 | 0.00     | 0.20     | 0.00     |
| 6      | 1:QZLokaal | Qw16  | 0.24   | 0.24  | 0.000 | 0.800 | 0.00     | 0.20     | 0.00     |

**BELASTINGEN**

B.G:14 Wind van rechts

onderdruk B

**STAAFBELASTINGEN**

B.G:14 Wind van rechts

onderdruk B

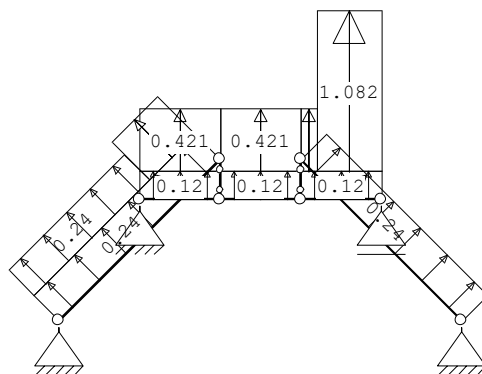
| Staaft | Type       | Index | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|--------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 6      | 1:QZLokaal | Qw1   | -0.36  | -0.36 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1      | 1:QZLokaal | Qw2   | -0.18  | -0.18 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2      | 1:QZLokaal | Qw2   | -0.18  | -0.18 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3      | 1:QZLokaal | Qw2   | -0.18  | -0.18 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7      | 1:QZLokaal | Qw3   | 0.36   | 0.36  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3      | 1:QZLokaal | Qw6   | 1.08   | 1.08  | 0.200 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3      | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.000 | 0.800 | 0.00     | 0.20     | 0.00     |
| 2      | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1      | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 6      | 1:QZLokaal | Qw15  | 0.36   | 0.36  | 2.028 | 0.000 | 0.00     | 0.20     | 0.00     |
| 6      | 1:QZLokaal | Qw16  | 0.24   | 0.24  | 0.000 | 0.800 | 0.00     | 0.20     | 0.00     |

Project.....: 240772  
 Onderdeel.....: slaper dakkapel

**BELASTINGEN**

B.G:15 Wind van rechts

overdruk B

**STAAFBELASTINGEN**

B.G:15 Wind van rechts

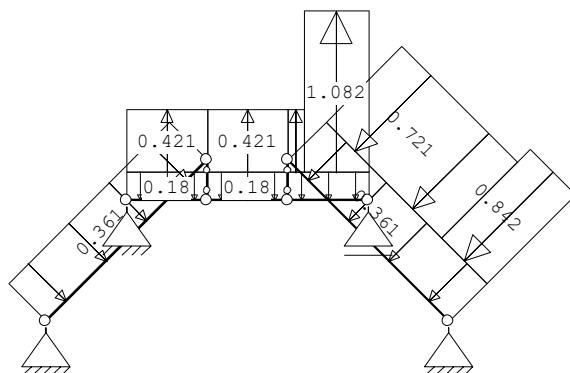
overdruk B

| Staaftype | Type       | Index | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|-----------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 6         | 1:QZLokaal | Qw10  | 0.24   | 0.24  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1         | 1:QZLokaal | Qw11  | 0.12   | 0.12  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2         | 1:QZLokaal | Qw11  | 0.12   | 0.12  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3         | 1:QZLokaal | Qw11  | 0.12   | 0.12  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7         | 1:QZLokaal | Qw12  | -0.24  | -0.24 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3         | 1:QZLokaal | Qw6   | 1.08   | 1.08  | 0.200 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3         | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.000 | 0.800 | 0.00     | 0.20     | 0.00     |
| 2         | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1         | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 6         | 1:QZLokaal | Qw15  | 0.36   | 0.36  | 2.028 | 0.000 | 0.00     | 0.20     | 0.00     |
| 6         | 1:QZLokaal | Qw16  | 0.24   | 0.24  | 0.000 | 0.800 | 0.00     | 0.20     | 0.00     |

**BELASTINGEN**

B.G:16 Wind van rechts

onderdruk C

**STAAFBELASTINGEN**

B.G:16 Wind van rechts

onderdruk C

| Staaftype | Type       | Index | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|-----------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 6         | 1:QZLokaal | Qw1   | -0.36  | -0.36 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1         | 1:QZLokaal | Qw2   | -0.18  | -0.18 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2         | 1:QZLokaal | Qw2   | -0.18  | -0.18 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3         | 1:QZLokaal | Qw2   | -0.18  | -0.18 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7         | 1:QZLokaal | Qw3   | 0.36   | 0.36  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7         | 1:QZLokaal | Qw13  | 0.84   | 0.84  | 0.000 | 2.028 | 0.00     | 0.20     | 0.00     |
| 7         | 1:QZLokaal | Qw14  | 0.72   | 0.72  | 0.800 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3         | 1:QZLokaal | Qw6   | 1.08   | 1.08  | 0.200 | 0.000 | 0.00     | 0.20     | 0.00     |

Project.....: 240772

Onderdeel.....: slaper dakkapel

**STAAFBELASTINGEN**

B.G:16 Wind van rechts

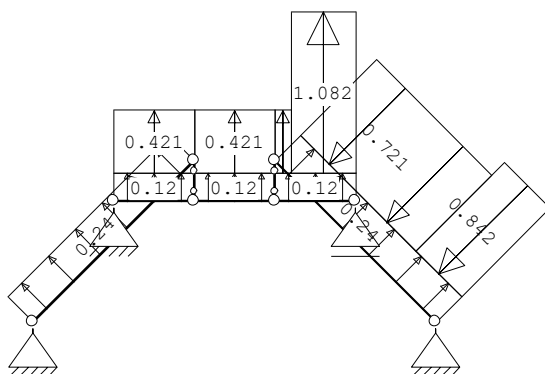
onderdruk C

| Staaft | Type       | Index | q1/p/m | q2   | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|--------|------------|-------|--------|------|-------|-------|----------|----------|----------|
| 3      | 1:QZLokaal | Qw7   | 0.42   | 0.42 | 0.000 | 0.800 | 0.00     | 0.20     | 0.00     |
| 2      | 1:QZLokaal | Qw7   | 0.42   | 0.42 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1      | 1:QZLokaal | Qw7   | 0.42   | 0.42 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |

**BELASTINGEN**

B.G:17 Wind van rechts

overdruk C

**STAAFBELASTINGEN**

B.G:17 Wind van rechts

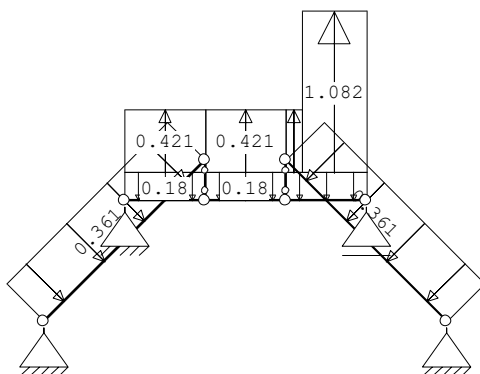
overdruk C

| Staaft | Type       | Index | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|--------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 6      | 1:QZLokaal | Qw10  | 0.24   | 0.24  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1      | 1:QZLokaal | Qw11  | 0.12   | 0.12  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2      | 1:QZLokaal | Qw11  | 0.12   | 0.12  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3      | 1:QZLokaal | Qw11  | 0.12   | 0.12  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7      | 1:QZLokaal | Qw12  | -0.24  | -0.24 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7      | 1:QZLokaal | Qw13  | 0.84   | 0.84  | 0.000 | 2.028 | 0.00     | 0.20     | 0.00     |
| 7      | 1:QZLokaal | Qw14  | 0.72   | 0.72  | 0.800 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3      | 1:QZLokaal | Qw6   | 1.08   | 1.08  | 0.200 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3      | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.000 | 0.800 | 0.00     | 0.20     | 0.00     |
| 2      | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1      | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |

**BELASTINGEN**

B.G:18 Wind van rechts

onderdruk D



Project.....: 240772  
 Onderdeel.....: slaper dakkapel

**STAAFBELASTINGEN**

B.G:18 Wind van rechts

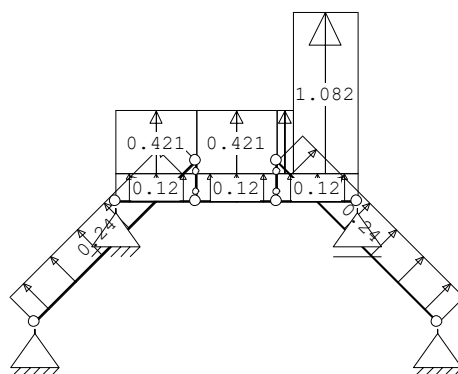
onderdruk D

| Staaf | Type       | Index | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|-------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 6     | 1:QZLokaal | Qw1   | -0.36  | -0.36 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw2   | -0.18  | -0.18 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2     | 1:QZLokaal | Qw2   | -0.18  | -0.18 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3     | 1:QZLokaal | Qw2   | -0.18  | -0.18 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7     | 1:QZLokaal | Qw3   | 0.36   | 0.36  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3     | 1:QZLokaal | Qw6   | 1.08   | 1.08  | 0.200 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3     | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.000 | 0.800 | 0.00     | 0.20     | 0.00     |
| 2     | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |

**BELASTINGEN**

B.G:19 Wind van rechts

overdruk D

**STAAFBELASTINGEN**

B.G:19 Wind van rechts

overdruk D

| Staaf | Type       | Index | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|-------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 6     | 1:QZLokaal | Qw10  | 0.24   | 0.24  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw11  | 0.12   | 0.12  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2     | 1:QZLokaal | Qw11  | 0.12   | 0.12  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3     | 1:QZLokaal | Qw11  | 0.12   | 0.12  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7     | 1:QZLokaal | Qw12  | -0.24  | -0.24 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3     | 1:QZLokaal | Qw6   | 1.08   | 1.08  | 0.200 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3     | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.000 | 0.800 | 0.00     | 0.20     | 0.00     |
| 2     | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw7   | 0.42   | 0.42  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |

**BEREKENINGSTATUS**

| B.C. | Iteratie | Status                 |
|------|----------|------------------------|
| 1    | 3        | Nauwkeurigheid bereikt |
| 2    | 3        | Nauwkeurigheid bereikt |
| 3    | 3        | Nauwkeurigheid bereikt |
| 4    | 3        | Nauwkeurigheid bereikt |
| 5    | 3        | Nauwkeurigheid bereikt |
| 6    | 3        | Nauwkeurigheid bereikt |
| 7    | 3        | Nauwkeurigheid bereikt |
| 8    | 3        | Nauwkeurigheid bereikt |
| 9    | 3        | Nauwkeurigheid bereikt |
| 10   | 3        | Nauwkeurigheid bereikt |
| 11   | 3        | Nauwkeurigheid bereikt |
| 12   | 3        | Nauwkeurigheid bereikt |
| 13   | 3        | Nauwkeurigheid bereikt |
| 14   | 3        | Nauwkeurigheid bereikt |

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



Project.....: 240772  
Onderdeel.....: slaper dakkapel

#### BEREKENINGSTATUS

| B.C. | Iteratie | Status                 |
|------|----------|------------------------|
| 15   | 3        | Nauwkeurigheid bereikt |
| 16   | 3        | Nauwkeurigheid bereikt |
| 17   | 3        | Nauwkeurigheid bereikt |
| 18   | 3        | Nauwkeurigheid bereikt |
| 19   | 3        | Nauwkeurigheid bereikt |
| 20   | 3        | Nauwkeurigheid bereikt |
| 21   | 3        | Nauwkeurigheid bereikt |
| 22   | 3        | Nauwkeurigheid bereikt |
| 23   | 3        | Nauwkeurigheid bereikt |
| 24   | 3        | Nauwkeurigheid bereikt |
| 25   | 3        | Nauwkeurigheid bereikt |
| 26   | 3        | Nauwkeurigheid bereikt |
| 27   | 3        | Nauwkeurigheid bereikt |
| 28   | 3        | Nauwkeurigheid bereikt |
| 29   | 3        | Nauwkeurigheid bereikt |
| 30   | 3        | Nauwkeurigheid bereikt |
| 31   | 3        | Nauwkeurigheid bereikt |
| 32   | 3        | Nauwkeurigheid bereikt |
| 33   | 3        | Nauwkeurigheid bereikt |
| 34   | 3        | Nauwkeurigheid bereikt |
| 35   | 3        | Nauwkeurigheid bereikt |
| 36   | 3        | Nauwkeurigheid bereikt |
| 37   | 3        | Nauwkeurigheid bereikt |
| 38   | 3        | Nauwkeurigheid bereikt |
| 39   | 1        | Lineaire berekening    |
| 40   | 1        | Lineaire berekening    |
| 41   | 1        | Lineaire berekening    |
| 42   | 1        | Lineaire berekening    |
| 43   | 1        | Lineaire berekening    |
| 44   | 1        | Lineaire berekening    |
| 45   | 1        | Lineaire berekening    |
| 46   | 1        | Lineaire berekening    |
| 47   | 1        | Lineaire berekening    |
| 48   | 1        | Lineaire berekening    |
| 49   | 1        | Lineaire berekening    |
| 50   | 1        | Lineaire berekening    |
| 51   | 1        | Lineaire berekening    |
| 52   | 1        | Lineaire berekening    |
| 53   | 1        | Lineaire berekening    |
| 54   | 1        | Lineaire berekening    |
| 55   | 1        | Lineaire berekening    |
| 56   | 1        | Lineaire berekening    |
| 57   | 1        | Lineaire berekening    |
| 58   | 1        | Lineaire berekening    |
| 59   | 1        | Lineaire berekening    |
| 60   | 1        | Lineaire berekening    |
| 61   | 1        | Lineaire berekening    |
| 62   | 1        | Lineaire berekening    |
| 63   | 1        | Lineaire berekening    |
| 64   | 1        | Lineaire berekening    |
| 65   | 1        | Lineaire berekening    |
| 66   | 1        | Lineaire berekening    |
| 67   | 1        | Lineaire berekening    |
| 68   | 1        | Lineaire berekening    |
| 69   | 1        | Lineaire berekening    |
| 70   | 1        | Lineaire berekening    |
| 71   | 1        | Lineaire berekening    |
| 72   | 1        | Lineaire berekening    |
| 73   | 1        | Lineaire berekening    |
| 74   | 1        | Lineaire berekening    |

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



Project.....: 240772  
Onderdeel....: slaper dakkapel

#### BEREKENINGSTATUS

| B.C. | Iteratie | Status              |
|------|----------|---------------------|
| 75   | 1        | Lineaire berekening |

#### BELASTINGCOMBINATIES

| BC | Type  |      |           |   |                 |
|----|-------|------|-----------|---|-----------------|
| 1  | Fund. | 1.35 | $G_{k,1}$ |   |                 |
| 2  | Fund. | 0.90 | $G_{k,1}$ |   |                 |
| 3  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 $Q_{k,2}$  |
| 4  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 $Q_{k,3}$  |
| 5  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 $Q_{k,4}$  |
| 6  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 $Q_{k,5}$  |
| 7  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 $Q_{k,6}$  |
| 8  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 $Q_{k,7}$  |
| 9  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 $Q_{k,8}$  |
| 10 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 $Q_{k,9}$  |
| 11 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 $Q_{k,10}$ |
| 12 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 $Q_{k,11}$ |
| 13 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 $Q_{k,12}$ |
| 14 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 $Q_{k,13}$ |
| 15 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 $Q_{k,14}$ |
| 16 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 $Q_{k,15}$ |
| 17 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 $Q_{k,16}$ |
| 18 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 $Q_{k,17}$ |
| 19 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 $Q_{k,18}$ |
| 20 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 $Q_{k,19}$ |
| 21 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 $Q_{k,2}$  |
| 22 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 $Q_{k,3}$  |
| 23 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 $Q_{k,4}$  |
| 24 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 $Q_{k,5}$  |
| 25 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 $Q_{k,6}$  |
| 26 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 $Q_{k,7}$  |
| 27 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 $Q_{k,8}$  |
| 28 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 $Q_{k,9}$  |
| 29 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 $Q_{k,10}$ |
| 30 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 $Q_{k,11}$ |
| 31 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 $Q_{k,12}$ |
| 32 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 $Q_{k,13}$ |
| 33 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 $Q_{k,14}$ |
| 34 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 $Q_{k,15}$ |
| 35 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 $Q_{k,16}$ |
| 36 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 $Q_{k,17}$ |
| 37 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 $Q_{k,18}$ |
| 38 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 $Q_{k,19}$ |
| 39 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 $Q_{k,2}$  |
| 40 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 $Q_{k,3}$  |
| 41 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 $Q_{k,4}$  |
| 42 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 $Q_{k,5}$  |
| 43 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 $Q_{k,6}$  |
| 44 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 $Q_{k,7}$  |
| 45 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 $Q_{k,8}$  |
| 46 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 $Q_{k,9}$  |
| 47 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 $Q_{k,10}$ |
| 48 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 $Q_{k,11}$ |
| 49 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 $Q_{k,12}$ |
| 50 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 $Q_{k,13}$ |

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



Project.....: 240772  
Onderdeel....: slaper dakkapel

#### BELASTINGCOMBINATIES

| BC Type |       |      |           |   |                        |
|---------|-------|------|-----------|---|------------------------|
| 51      | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 $Q_{k,14}$        |
| 52      | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 $Q_{k,15}$        |
| 53      | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 $Q_{k,16}$        |
| 54      | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 $Q_{k,17}$        |
| 55      | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 $Q_{k,18}$        |
| 56      | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 $Q_{k,19}$        |
| 57      | Quas. | 1.00 | $G_{k,1}$ |   |                        |
| 58      | Freq. | 1.00 | $G_{k,1}$ |   |                        |
| 59      | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 $\psi_1 Q_{k,4}$  |
| 60      | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 $\psi_1 Q_{k,5}$  |
| 61      | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 $\psi_1 Q_{k,6}$  |
| 62      | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 $\psi_1 Q_{k,7}$  |
| 63      | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 $\psi_1 Q_{k,8}$  |
| 64      | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 $\psi_1 Q_{k,9}$  |
| 65      | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 $\psi_1 Q_{k,10}$ |
| 66      | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 $\psi_1 Q_{k,11}$ |
| 67      | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 $\psi_1 Q_{k,12}$ |
| 68      | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 $\psi_1 Q_{k,13}$ |
| 69      | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 $\psi_1 Q_{k,14}$ |
| 70      | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 $\psi_1 Q_{k,15}$ |
| 71      | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 $\psi_1 Q_{k,16}$ |
| 72      | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 $\psi_1 Q_{k,17}$ |
| 73      | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 $\psi_1 Q_{k,18}$ |
| 74      | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 $\psi_1 Q_{k,19}$ |
| 75      | Blij. | 1.00 | $G_{k,1}$ |   |                        |

#### GUNSTIGE WERKING PERMANENTE BELASTINGEN

| BC Staven met gunstige werking |                            |
|--------------------------------|----------------------------|
| 1                              | Geen                       |
| 2                              | Alle staven de factor:0.90 |
| 3                              | Geen                       |
| 4                              | Geen                       |
| 5                              | Geen                       |
| 6                              | Geen                       |
| 7                              | Geen                       |
| 8                              | Geen                       |
| 9                              | Geen                       |
| 10                             | Geen                       |
| 11                             | Geen                       |
| 12                             | Geen                       |
| 13                             | Geen                       |
| 14                             | Geen                       |
| 15                             | Geen                       |
| 16                             | Geen                       |
| 17                             | Geen                       |
| 18                             | Geen                       |
| 19                             | Geen                       |
| 20                             | Geen                       |
| 21                             | Alle staven de factor:0.90 |
| 22                             | Alle staven de factor:0.90 |
| 23                             | Alle staven de factor:0.90 |
| 24                             | Alle staven de factor:0.90 |
| 25                             | Alle staven de factor:0.90 |
| 26                             | Alle staven de factor:0.90 |
| 27                             | Alle staven de factor:0.90 |

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie

IRg

Project.....: 240772  
Onderdeel.....: slaper dakkapel

#### GUNSTIGE WERKING PERMANENTE BELASTINGEN

BC Staven met gunstige werking

28 Alle staven de factor:0.90  
29 Alle staven de factor:0.90  
30 Alle staven de factor:0.90  
31 Alle staven de factor:0.90  
32 Alle staven de factor:0.90  
33 Alle staven de factor:0.90  
34 Alle staven de factor:0.90  
35 Alle staven de factor:0.90  
36 Alle staven de factor:0.90  
37 Alle staven de factor:0.90  
38 Alle staven de factor:0.90

#### BELASTINGCOMBINATIE

B.C:75

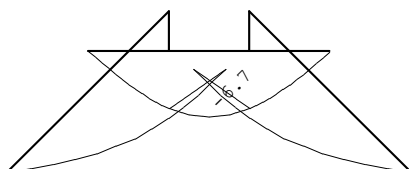
Blijvend

#### VERPLAATSINGEN

1e orde [mm]

B.C:75

Blijvend



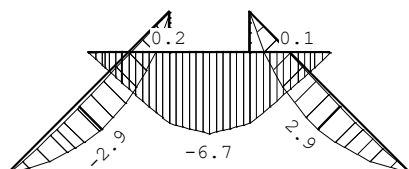
#### OMHULLENDE VAN DE FUNDAMENTELE COMBINATIES

#### MOMENTEN

2e orde

Fundamentele

combinatie



Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

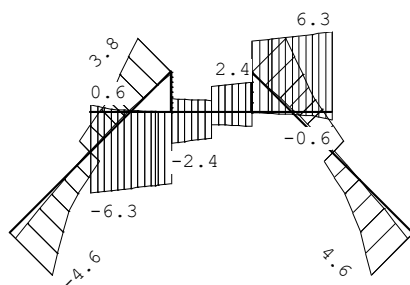
Revisie



Project.....: 240772  
Onderdeel.....: slaper dakkapel

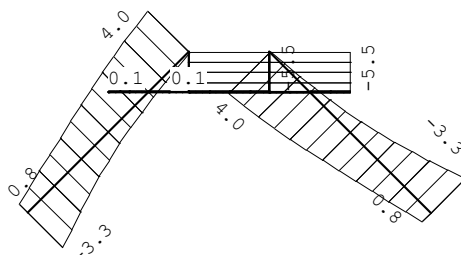
**DWARSKRACHTEN** 2e orde  
combinatie

Fundamentele



**NORMAALKRACHTEN** 2e orde  
combinatie

Fundamentele



**REACTIES** 2e orde  
combinatie

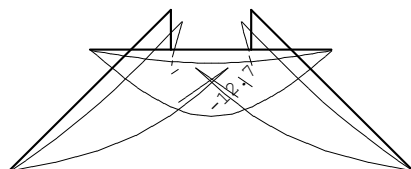
Fundamentele

| Kn. | X-min | X-max | Z-min | Z-max | M-min | M-max |
|-----|-------|-------|-------|-------|-------|-------|
| 1   | -0.06 | 0.06  | -0.57 | 6.27  |       |       |
| 2   |       |       | -0.57 | 6.27  |       |       |
| 7   | -3.46 | 1.55  | 2.26  | 4.48  |       |       |
| 8   | -1.55 | 3.46  | 2.26  | 4.48  |       |       |

Project.....: 240772  
 Onderdeel.....: slaper dakkapel

**OMHULLENDE VAN DE KARAKTERISTIEKE COMBINATIES**

**VERPLAATSINGEN** 1e orde [mm] Karakteristieke combinatie



**REACTIES** 1e orde Karakteristieke combinatie

| Kn. | X-min | X-max | Z-min | Z-max | M-min | M-max |
|-----|-------|-------|-------|-------|-------|-------|
| 1   | 0.00  | 0.00  | 0.66  | 4.61  |       |       |
| 2   |       |       | 0.66  | 4.61  |       |       |
| 7   | -2.23 | 1.03  | 2.56  | 3.56  |       |       |
| 8   | -1.03 | 2.23  | 2.56  | 3.56  |       |       |

**OMHULLENDE VAN DE BLIJVENDE COMBINATIES**

**REACTIES** 1e orde Blijvende combinatie

| Kn. | X    | Z    | M |
|-----|------|------|---|
| 1   | 0.00 | 2.61 |   |
| 2   |      | 2.61 |   |
| 7   | 0.00 | 2.56 |   |
| 8   | 0.00 | 2.56 |   |

**MATERIAALGEGEVENS**

| Mt | Kwaliteit | $f_{m,y,k}$<br>[N/mm <sup>2</sup> ] | $\rho_k$<br>[kg/m <sup>3</sup> ] | $\rho_{mean}$<br>[kg/m <sup>3</sup> ] | $f_{t,0,k}$<br>[N/mm <sup>2</sup> ] | $f_{t,90,k}$<br>[N/mm <sup>2</sup> ] | $f_{c,0,k}$<br>[N/mm <sup>2</sup> ] | $f_{c,90,k}$<br>[N/mm <sup>2</sup> ] | $f_{v,k}$<br>[N/mm <sup>2</sup> ] |
|----|-----------|-------------------------------------|----------------------------------|---------------------------------------|-------------------------------------|--------------------------------------|-------------------------------------|--------------------------------------|-----------------------------------|
| 1  | C24       | 24                                  | 350                              | 420                                   | 14.5                                | 0.4                                  | 21.0                                | 2.5                                  | 4.0                               |
| 2  | C20       | 20                                  | 330                              | 400                                   | 11.5                                | 0.4                                  | 19.0                                | 2.3                                  | 3.6                               |

**MATERIAALGEGEVENS (vervolg)**

| Mt | Kwaliteit | $G_{mean}$<br>[N/mm <sup>2</sup> ] | $E_{0,05}$<br>[N/mm <sup>2</sup> ] | $E_{0,mean}$<br>[N/mm <sup>2</sup> ] | $E_{0,mean}$<br>[N/mm <sup>2</sup> ] | Klimaatklasse | $k_{def}$ | $E_{0,mean,fin}$<br>[N/mm <sup>2</sup> ] |
|----|-----------|------------------------------------|------------------------------------|--------------------------------------|--------------------------------------|---------------|-----------|------------------------------------------|
| 1  | C24       | 690                                | 7400                               | 370                                  | 11000                                | I             | 0.60      | 6875                                     |
| 2  | C20       | 590                                | 6400                               | 320                                  | 9500                                 | I             | 0.60      | 5938                                     |

**KIPSTABILITEIT**

| Staaf | Plts.<br>aangr. | 1 sys.<br>[m]    | Kipsteunafstanden<br>[m]     |
|-------|-----------------|------------------|------------------------------|
| 1     | 1.0*h           | boven:<br>onder: | 1.00 0;1.000<br>1.00 0;1.000 |
| 2     | 1.0*h           | boven:<br>onder: | 1.00 1.000<br>1.00 1.000     |
| 3     | 1.0*h           | boven:<br>onder: | 1.00 1.000<br>1.00 1.000     |
| 4     | 0.0*h           | boven:<br>onder: | 0.50 0;0.500<br>0.50 0;0.500 |
| 5     | 1.0*h           | boven:<br>onder: | 0.50 0;0.500<br>0.50 0;0.500 |
| 6     | 1.0*h           | boven:<br>onder: | 2.83 0;2.828<br>2.83 0;2.828 |
| 7     | 0.0*h           | boven:<br>onder: | 2.83 0;2.828<br>2.83 0;2.828 |

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



Project.....: 240772  
Onderdeel.....: slaper dakkapel

### STABILITEIT

| Stf | b <sub>gem</sub><br>[mm] | h <sub>gem</sub><br>[mm] | l <sub>sys</sub><br>[mm] | l <sub>buc, y/z</sub><br>[mm] |     | $\lambda_y$ | $\lambda_z$ | $\lambda_{rel, y/z}$ | $\beta_c$ | k <sub>y</sub> | k <sub>z</sub> | k <sub>c, y</sub> | k <sub>c, z</sub> |       |
|-----|--------------------------|--------------------------|--------------------------|-------------------------------|-----|-------------|-------------|----------------------|-----------|----------------|----------------|-------------------|-------------------|-------|
| 1   | 157                      | 150                      | 1000                     | 1000                          | nvt | 23.1        | 22.1        | 0.401                | 0.383     | 0.2            | 0.590          | 0.581             | 0.977             | 0.981 |
| 2   | 157                      | 150                      | 1000                     | 1000                          | nvt | 23.1        | 22.1        | 0.401                | 0.383     | 0.2            | 0.590          | 0.581             | 0.977             | 0.981 |
| 3   | 157                      | 150                      | 1000                     | 1000                          | nvt | 23.1        | 22.1        | 0.401                | 0.383     | 0.2            | 0.590          | 0.581             | 0.977             | 0.981 |
| 4   | 157                      | 150                      | 500                      | 500                           | nvt | 11.5        | 11.0        | 0.200                | 0.191     | 0.2            | 0.510          | 0.507             | 1.021             | 1.023 |
| 5   | 157                      | 150                      | 500                      | 500                           | nvt | 11.5        | 11.0        | 0.200                | 0.191     | 0.2            | 0.510          | 0.507             | 1.021             | 1.023 |
| 6   | 157                      | 150                      | 2828                     | 2828                          | nvt | 65.3        | 62.4        | 1.133                | 1.082     | 0.2            | 1.225          | 1.164             | 0.591             | 0.628 |
| 7   | 157                      | 150                      | 2828                     | 2828                          | nvt | 65.3        | 62.4        | 1.133                | 1.082     | 0.2            | 1.225          | 1.164             | 0.591             | 0.628 |

### STABILITEIT (vervolg)

| Staaft | positie<br>[mm] | l <sub>ef, y</sub><br>[mm] | $\sigma_{my, crit}$<br>[N/mm <sup>2</sup> ] | $\lambda_{rel, my}$ | k <sub>crit, y</sub> |
|--------|-----------------|----------------------------|---------------------------------------------|---------------------|----------------------|
| 1      | 1000            | 1200                       | 683.60                                      | 0.17                | 1.00                 |
| 2      | 500             | 1300                       | 631.01                                      | 0.18                | 1.00                 |
| 3      | 0               | 1200                       | 683.60                                      | 0.17                | 1.00                 |
| 4      | 0               | 800                        | 1025.40                                     | 0.14                | 1.00                 |
| 5      | 0               | 425                        | 1930.16                                     | 0.10                | 1.00                 |
| 6      | 1414            | 3128                       | 262.25                                      | 0.28                | 1.00                 |
| 7      | 1414            | 3128                       | 262.25                                      | 0.28                | 1.00                 |

### TOETSING SPANNINGEN

| Staaft |   |  | BC / Sit. | 4 / 1  | UC frm(6.17) | 0.82 |
|--------|---|--|-----------|--------|--------------|------|
| Staaft | 2 |  | BC / Sit. | 4 / 1  | UC frm(6.17) | 0.93 |
| Staaft | 3 |  | BC / Sit. | 4 / 1  | UC frm(6.17) | 0.82 |
| Staaft | 4 |  | BC / Sit. | 9 / 1  | UC frm(6.2 ) | 0.02 |
| Staaft | 5 |  | BC / Sit. | 17 / 1 | UC frm(6.2 ) | 0.02 |
| Staaft | 6 |  | BC / Sit. | 4 / 1  | UC frm(6.17) | 0.40 |
| Staaft | 7 |  | BC / Sit. | 4 / 1  | UC frm(6.17) | 0.40 |

### TOETSING DOORBUIGING

| Stf | Soort | Mtg | l <sub>sys</sub><br>[mm] | Overstek<br>i j | BC Sit | u <sub>bi j</sub><br>[mm] | Toelaatbaar<br>[mm] | *1      | u <sub>rin, net</sub><br>[mm] | Toelaatbaar<br>[mm] | *1      |
|-----|-------|-----|--------------------------|-----------------|--------|---------------------------|---------------------|---------|-------------------------------|---------------------|---------|
| 1   | Dak   | ss  | 1000                     | Nee Nee         | 57 1   | -7.1                      | -8.0                | 2*0.004 | -11.8                         | -8.0                | 2*0.004 |
| 2   | Dak   | db  | 1000                     | Nee Nee         | 57 1   | -1.1                      | -4.0                | 0.004   | -1.8                          | -4.0                | 0.004   |
| 3   | Dak   | ss  | 1000                     | Nee Nee         | 57 1   | -7.1                      | -8.0                | 2*0.004 | -11.8                         | -8.0                | 2*0.004 |

### TOETSING DOORBUIGING (vervolg)

| Stf | Soort | Mtg | l <sub>sys</sub><br>[mm] | Overstek<br>i j | Zeeg | BC Sit | u <sub>inst</sub><br>[mm] | Toelaatbaar<br>[mm] | *1      |
|-----|-------|-----|--------------------------|-----------------|------|--------|---------------------------|---------------------|---------|
| 1   | Dak   | ss  | 1000                     | Nee Nee         | 0.0  | 40 1   | -9.0                      | -8.0                | 2*0.004 |
| 2   | Dak   | db  | 1000                     | Nee Nee         | 0.0  | 40 1   | -1.4                      | -4.0                | 0.004   |
| 3   | Dak   | ss  | 1000                     | Nee Nee         | 0.0  | 40 1   | -9.0                      | -8.0                | 2*0.004 |

### TOETSING HORIZONTALE VERPLAATSING

| Staaft | Mtg | l <sub>sys</sub><br>[mm] | BC Sit | w <sub>tot</sub><br>[mm] | Toelaatbaar<br>[mm] | [h/ ] |
|--------|-----|--------------------------|--------|--------------------------|---------------------|-------|
| 4      | ss  | 500                      | 40 3   | -9.0                     | -1.7                | 300   |
| 5      | ss  | 500                      | 40 3   | -9.0                     | -1.7                | 300   |

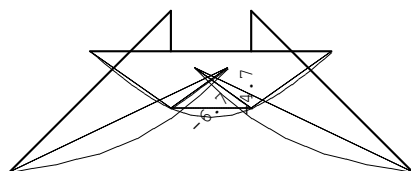
Project.....: 240772  
Onderdeel.....: slaper dakkapel

**VERVORMINGEN w1**

Blijvende

combinatie

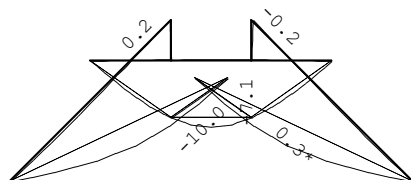
\* - relatief aan de rechte lijn die de uiteinden verbindt

**VERVORMINGEN w<sub>bij</sub>**

Karakteristieke

combinatie

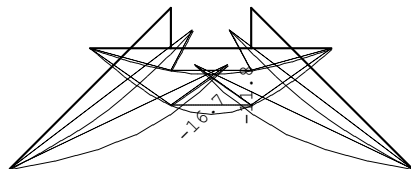
\* - relatief aan de rechte lijn die de uiteinden verbindt

**VERVORMINGEN w<sub>max</sub>**

Karakteristieke

combinatie

\* - relatief aan de rechte lijn die de uiteinden verbindt

**DOORBUIGINGEN**

Karakteristieke

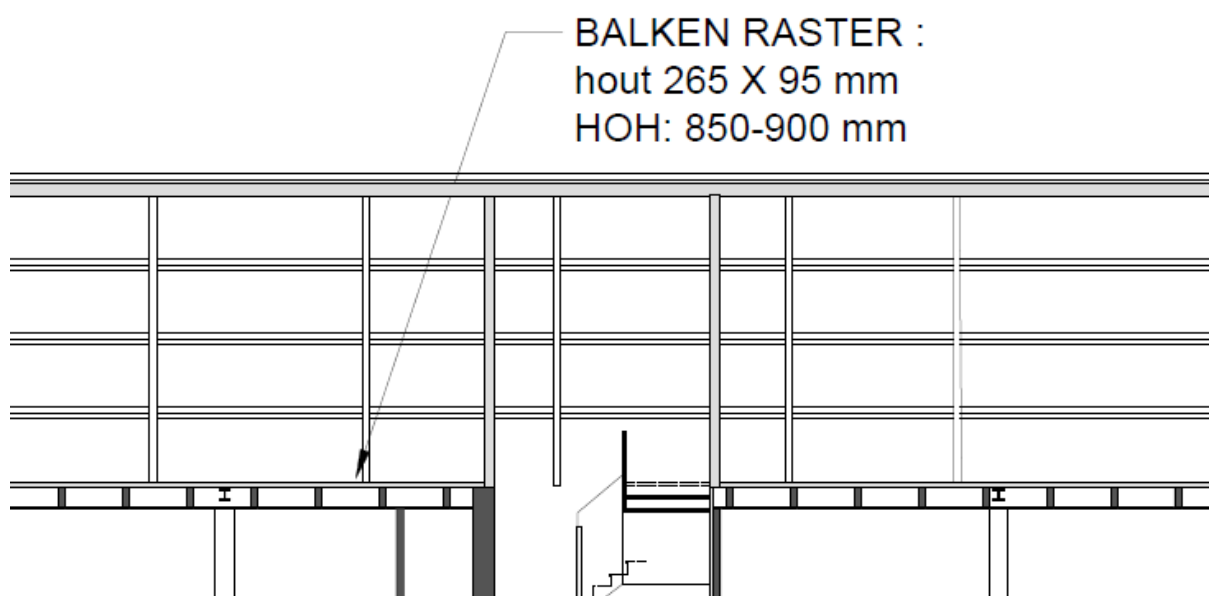
combinatie

| Nr. | staven | Zijde | positie | $l_{rep}$ | $w_1$ | $w_2$ | $w_{bij}$    | $w_{tot}$ | $w_c$ | $w_{max}$    |
|-----|--------|-------|---------|-----------|-------|-------|--------------|-----------|-------|--------------|
|     |        |       | [m]     | [mm]      | [mm]  | [mm]  | [mm] [lrep/] | [mm]      | [mm]  | [mm] [lrep/] |
| 1   | 1      | Neg.  | /       | 2000      | -4.7  | -2.8  | -7.1         | 282       | -11.8 | -11.8        |
| 2   | 2      | Neg.  | 0.500   | 1000      | -0.7  | -0.4  | -1.1         | 893       | -1.8  | -1.8         |
| 3   | 3      | Neg.  | 0.500   | 1000      | -0.4  | -0.2  | -0.5         | 1938      | -0.9  | -0.9         |
| 3   | 3      | Pos.  | /       | 2000      | 4.7   | 2.8   | 7.1          | 282       | 11.8  | 11.8         |
| 6   | 6      | Neg.  | /       | 5657      | -6.7  | -4.0  | -10.0        | 563       | -16.7 | -16.7        |
| 7   | 7      | Pos.  | /       | 5657      | 6.7   | 4.0   | 10.0         | 563       | 16.7  | 16.7         |

### 3.4 Controle balklaag zoldervloer

De bestaande balklaag heeft een afmeting van 95x265 hoh 875 mm

Balklaag voldoet ruim niet.



Technosoft Construct release 6.74  
2024

11 dec

Project : 240772  
 Onderdeel : balklagen  
 Datum : 11/12/2024  
 Eenheden : kN/m/rad  
 Bestand : G:\shortcut-targets-by-id\0ByYUb81WrbDqYlpOSXRzaHdIV0E\Projecten\2024\240772\Houtconstructie\balklagen.cnw

**Toegepaste normen volgens Eurocode met Nederlandse NB**

|             |                      |                 |             |
|-------------|----------------------|-----------------|-------------|
| Belastingen | NEN-EN 1990:2002     | C2:2010,A1:2019 | NB:2019(nl) |
|             | NEN-EN 1991-1-1:2002 | C1/C11:2019     | NB:2019(nl) |
| Hout        | NEN-EN 1995-1-1:2005 | A1:2011,C1:2006 | NB:2013(nl) |
|             | NEN-EN 14080:2013    |                 |             |

**Balklaag berekening. (H)****Algemene gegevens**

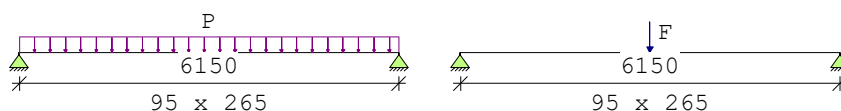
|                        |                 |                                            |        |
|------------------------|-----------------|--------------------------------------------|--------|
| B x H                  | [mm] : 95 x 265 | Sterkteklasse                              | : C18  |
| Overspanning           | [mm] : 6150     | Klimaatklasse                              | : I    |
| Opleglengte            | [mm] : 100      | Referentie periode [j]                     | : 50   |
| H.o.h. afstand         | [mm] : 875      | Min. eigenfreq. [Hz]                       | : 3    |
| Beschot sterkteklasse: | C24             |                                            |        |
| Dikte beschot          | [mm] : 12       | $E_{0,mean} \times I$ [Nm <sup>2</sup> /m] | : 1584 |

**Permanente belastingen** $G_{rep}$ 

|                             |         |
|-----------------------------|---------|
| EG balklaag                 | : 0.35  |
| Extra belasting             | : 0.55+ |
| Totaal [kN/m <sup>2</sup> ] | : 0.90  |

**Veranderlijke belastingen**

|                                         |                      |
|-----------------------------------------|----------------------|
| $Q_k + P_{wanden}$ [kN/m <sup>2</sup> ] | : 3.00 = 2.50 + 0.50 |
| $\Psi_0$ [ - ]                          | : 0.40               |
| $\Psi_2$ [ - ]                          | : 0.30               |
| $Q_k$ [kN]                              | : 3.00               |
| $Q_k$ oppervlak [m <sup>2</sup> ]       | : 0.50 x 0.50        |
| Reductiefactor                          | : 1.00               |



Belastingfactoren (NEN-EN 1990)

Formule 6.10a:  $\gamma_G$  : 1.35  $\gamma_Q$  : 1.50Formule 6.10b:  $\xi\gamma_G$  : 1.20  $\gamma_Q$  : 1.50

Partiële factor (Tabel 2.3 NEN-EN 1995-1-1)

 $\gamma_M$  [-]: 1.30Meegenomen combinaties in de berekening :  $k_{mod}$  [-]  $b_{ef}$  [mm]  $k_{c,90,q}$  $k_{c,90,F}$ \* Permanent (G<sub>rep</sub>) 0.60 95

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



|                            |                                      |      |    |      |
|----------------------------|--------------------------------------|------|----|------|
| * Perm. + q-last (6.10a)   | (G <sub>rep</sub> + q <sub>k</sub> ) | 0.80 | 95 | 1.00 |
| * Perm. + q-last (6.10b)   | (G <sub>rep</sub> + q <sub>k</sub> ) | 0.80 | 95 | 1.00 |
| * Perm. + puntlast (6.10a) | (G <sub>rep</sub> + Q <sub>k</sub> ) | 0.80 | 95 | 1.00 |
| 1.00                       |                                      |      |    |      |
| * Perm. + puntlast (6.10b) | (G <sub>rep</sub> + Q <sub>k</sub> ) | 0.80 | 95 | 1.00 |
| 1.00                       |                                      |      |    |      |

#### Resultaten (maatgevende combinaties)

eis

u.c.

|                               |                                                   |   |                           |   |             |                      |             |
|-------------------------------|---------------------------------------------------|---|---------------------------|---|-------------|----------------------|-------------|
| Perm + qlast(6.10b) frm(6.11) | $\sigma_{m,y,d}$                                  | = | 20.76                     | < | 11.08       | [N/mm <sup>2</sup> ] | <u>1.87</u> |
| Perm + qlast(6.10b) frm(6.13) | $\tau_{v,d}$                                      | = | 0.88                      | < | 2.09        | [N/mm <sup>2</sup> ] | 0.42        |
| Perm + qlast(6.10b) frm(6.3)  | $\sigma_{c,90,q,d} / (k_{c,90,q} * f_{c,90,d}) +$ |   |                           |   |             |                      |             |
|                               | $\sigma_{c,90,F,d} / (k_{c,90,F} * f_{c,90,d})$   | < | 1.00                      |   |             |                      |             |
|                               |                                                   | = | 1.57 / 1.35 + 0.00 / 1.35 | = | <u>1.16</u> |                      |             |

|                     |                      |   |       |   |       |      |             |
|---------------------|----------------------|---|-------|---|-------|------|-------------|
| Verdeelde belasting | U <sub>bij</sub>     | = | 50.15 | < | 18.45 | [mm] | <u>2.72</u> |
| Verdeelde belasting | U <sub>net,fin</sub> | = | 61.21 | < | 24.60 | [mm] | <u>2.49</u> |

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



### **3.5 Controle balklaag zoldervloer met versterking**

De balklaag wordt versterkt met 2x71x265 mm C24 kwaliteit

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



Technosoft Construct release 6.74  
2024

11 dec

Project : 240772  
Onderdeel : balklagen  
Datum : 11/12/2024  
Eenheden : kN/m/rad  
Bestand : G:\shortcut-targets-by-id\  
0ByYUb81WrbDqYlpOSXRzaHdIV0E\Projecten\2024\240772\  
Houtconstructie\balklagen.cnw

### Toegepaste normen volgens Eurocode met Nederlandse NB

|             |                      |                 |             |
|-------------|----------------------|-----------------|-------------|
| Belastingen | NEN-EN 1990:2002     | C2:2010,A1:2019 | NB:2019(nl) |
|             | NEN-EN 1991-1-1:2002 | C1/C11:2019     | NB:2019(nl) |
| Hout        | NEN-EN 1995-1-1:2005 | A1:2011,C1:2006 | NB:2013(nl) |
|             | NEN-EN 14080:2013    |                 |             |

### Balklaag berekening. (H)

#### Algemene gegevens

|                        |                  |                                            |   |      |
|------------------------|------------------|--------------------------------------------|---|------|
| B x H                  | [mm] : 237 x 265 | Sterkteklasse                              | : | C20  |
| Overspanning           | [mm] : 6150      | Klimaatklasse                              | : | I    |
| Opleglengte            | [mm] : 100       | Referentie periode [j]                     | : | 50   |
| H.o.h. afstand         | [mm] : 875       | Min. eigenfreq. [Hz]                       | : | 3    |
| Beschot sterkteklasse: | C24              |                                            |   |      |
| Dikte beschot          | [mm] : 12        | $E_{0,mean} \times I$ [Nm <sup>2</sup> /m] | : | 1584 |

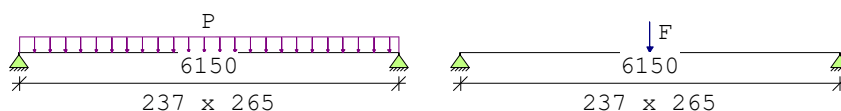
#### Permanente belastingen

$G_{rep}$

|                             |   |       |
|-----------------------------|---|-------|
| EG balklaag                 | : | 0.35  |
| Extra belasting             | : | 0.55+ |
| Totaal [kN/m <sup>2</sup> ] | : | 0.90  |

#### Veranderlijke belastingen

|                                         |   |                    |
|-----------------------------------------|---|--------------------|
| $Q_k + P_{wanden}$ [kN/m <sup>2</sup> ] | : | 3.00 = 2.50 + 0.50 |
| $\Psi_0$ [ - ]                          | : | 0.40               |
| $\Psi_2$ [ - ]                          | : | 0.30               |
| $Q_k$ [kN]                              | : | 3.00               |
| $Q_k$ oppervlak [m <sup>2</sup> ]       | : | 0.50 x 0.50        |
| Reductiefactor                          | : | 1.00               |



Belastingfactoren (NEN-EN 1990)

Formule 6.10a:  $\gamma_G$  : 1.35  $\gamma_Q$  : 1.50

Formule 6.10b:  $\xi\gamma_G$  : 1.20  $\gamma_Q$  : 1.50

Partiële factor (Tabel 2.3 NEN-EN 1995-1-1)

$\gamma_M$  [-]: 1.30

Meegenomen combinaties in de berekening :  $k_{mod}$  [-]  $b_{ef}$  [mm]  $k_{c,90,q}$

$k_{c,90,F}$

\* Permanent (  $G_{rep}$  ) 0.60 237

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



|                            |                                      |      |     |      |
|----------------------------|--------------------------------------|------|-----|------|
| * Perm. + q-last (6.10a)   | (G <sub>rep</sub> + q <sub>k</sub> ) | 0.80 | 237 | 1.00 |
| * Perm. + q-last (6.10b)   | (G <sub>rep</sub> + q <sub>k</sub> ) | 0.80 | 237 | 1.00 |
| * Perm. + puntlast (6.10a) | (G <sub>rep</sub> + Q <sub>k</sub> ) | 0.80 | 237 | 1.00 |
| 1.00                       |                                      |      |     |      |
| * Perm. + puntlast (6.10b) | (G <sub>rep</sub> + Q <sub>k</sub> ) | 0.80 | 237 | 1.00 |
| 1.00                       |                                      |      |     |      |

#### Resultaten (maatgevende combinaties)

eis

u.c.

|                               |                                                   |   |                           |   |       |                      |      |
|-------------------------------|---------------------------------------------------|---|---------------------------|---|-------|----------------------|------|
| Perm + qlast(6.10b) frm(6.11) | $\sigma_{m,y,d}$                                  | = | 8.32                      | < | 12.31 | [N/mm <sup>2</sup> ] | 0.68 |
| Perm + qlast(6.10b) frm(6.13) | $\tau_{v,d}$                                      | = | 0.35                      | < | 2.22  | [N/mm <sup>2</sup> ] | 0.16 |
| Perm + qlast(6.10b) frm(6.3)  | $\sigma_{c,90,q,d} / (k_{c,90,q} * f_{c,90,d}) +$ |   |                           |   |       |                      |      |
|                               | $\sigma_{c,90,F,d} / (k_{c,90,F} * f_{c,90,d})$   | < | 1.00                      |   |       |                      |      |
|                               |                                                   | = | 0.63 / 1.42 + 0.00 / 1.42 | = | 0.44  |                      |      |

|                     |                      |   |       |   |       |      |             |
|---------------------|----------------------|---|-------|---|-------|------|-------------|
| Verdeelde belasting | U <sub>bij</sub>     | = | 19.04 | < | 18.45 | [mm] | <u>1.03</u> |
| Verdeelde belasting | U <sub>net,fin</sub> | = | 23.24 | < | 24.60 | [mm] | 0.94        |

### 3.6 Balklaag zoldervloer nieuw naast trapparing

Technosoft Construct release 6.74  
 2024

11 dec

Project : 240772  
 Onderdeel : balklagen  
 Datum : 11/12/2024  
 Eenheden : kN/m/rad  
 Bestand : G:\.shortcut-targets-by-id\  
 0ByYUb81WrbDqYlpOSXRzaHdIV0E\Projecten\2024\240772\  
 Houtconstructie\balklagen.cnw

#### Toegepaste normen volgens Eurocode met Nederlandse NB

|             |                      |                 |             |
|-------------|----------------------|-----------------|-------------|
| Belastingen | NEN-EN 1990:2002     | C2:2010,A1:2019 | NB:2019(nl) |
|             | NEN-EN 1991-1-1:2002 | C1/C11:2019     | NB:2019(nl) |
| Hout        | NEN-EN 1995-1-1:2005 | A1:2011,C1:2006 | NB:2013(nl) |
|             | NEN-EN 14080:2013    |                 |             |

#### Balklaag berekening. (H)

##### Algemene gegevens

|                        |        |          |                                            |   |      |
|------------------------|--------|----------|--------------------------------------------|---|------|
| B x H                  | [mm] : | 96 x 271 | Sterkteklasse                              | : | C24  |
| Overspanning           | [mm] : | 6150     | Klimaatklasse                              | : | I    |
| Opleglengte            | [mm] : | 100      | Referentie periode [j]                     | : | 50   |
| H.o.h. afstand         | [mm] : | 400      | Min. eigenfreq. [Hz]                       | : | 3    |
| Beschot sterkteklasse: |        | C24      |                                            |   |      |
| Dikte beschot          | [mm] : | 12       | $E_{0,mean} \times I$ [Nm <sup>2</sup> /m] | : | 1584 |

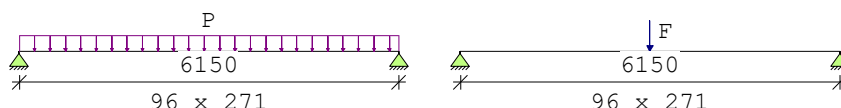
##### Permanente belastingen

$G_{rep}$

|                             |   |       |
|-----------------------------|---|-------|
| EG balklaag                 | : | 0.35  |
| Extra belasting             | : | 0.55+ |
| Totaal [kN/m <sup>2</sup> ] | : | 0.90  |

##### Veranderlijke belastingen

|                                         |   |                    |
|-----------------------------------------|---|--------------------|
| $q_k + P_{wanden}$ [kN/m <sup>2</sup> ] | : | 3.00 = 2.50 + 0.50 |
| $\Psi_0$ [ - ]                          | : | 0.40               |
| $\Psi_2$ [ - ]                          | : | 0.30               |
| $Q_k$ [kN]                              | : | 3.00               |
| $Q_k$ oppervlak [m <sup>2</sup> ]       | : | 0.50 x 0.50        |
| Reductiefactor                          | : | 0.66               |



Belastingfactoren (NEN-EN 1990)

|                |                  |      |              |      |
|----------------|------------------|------|--------------|------|
| Formule 6.10a: | $\gamma_G$ :     | 1.35 | $\gamma_Q$ : | 1.50 |
| Formule 6.10b: | $\xi \gamma_G$ : | 1.20 | $\gamma_Q$ : | 1.50 |

Partiële factor (Tabel 2.3 NEN-EN 1995-1-1)

$\gamma_M [-]$ : 1.30

| Meegenomen combinaties in de berekening : |                   |               |               |              |
|-------------------------------------------|-------------------|---------------|---------------|--------------|
|                                           |                   | $k_{mod} [-]$ | $b_{ef} [mm]$ | $k_{c,90,q}$ |
| $k_{c,90,F}$                              |                   |               |               |              |
| * Permanent                               | $(G_{rep})$       | 0.60          | 96            |              |
| * Perm. + q-last (6.10a)                  | $(G_{rep} + q_k)$ | 0.80          | 96            | 1.00         |
| * Perm. + q-last (6.10b)                  | $(G_{rep} + q_k)$ | 0.80          | 96            | 1.00         |
| * Perm. + puntlast (6.10a)                | $(G_{rep} + Q_k)$ | 0.80          | 96            | 1.00         |
| 1.00                                      |                   |               |               |              |
| * Perm. + puntlast (6.10b)                | $(G_{rep} + Q_k)$ | 0.80          | 96            | 1.00         |
| 1.00                                      |                   |               |               |              |

**Resultaten (maatgevende combinaties)****eis****u.c.**

|                               |                                                        |   |                           |   |                            |      |
|-------------------------------|--------------------------------------------------------|---|---------------------------|---|----------------------------|------|
| Perm + qlast(6.10b) frm(6.11) | $\sigma_{m,y,d}$                                       | = | 8.98                      | < | 14.77 [N/mm <sup>2</sup> ] | 0.61 |
| Perm + qlast(6.10b) frm(6.13) | $\tau_{v,d}$                                           | = | 0.39                      | < | 2.46 [N/mm <sup>2</sup> ]  | 0.16 |
| Perm + qlast(6.10b) frm(6.3)  | $\sigma_{c,90,q,d} / (k_{c,90,q} * f_{c,90,d}) +$      |   |                           |   |                            |      |
|                               | $\sigma_{c,90,F,d} / (k_{c,90,F} * f_{c,90,d}) < 1.00$ |   |                           |   |                            |      |
|                               |                                                        | = | 0.71 / 1.54 + 0.00 / 1.54 | = | 0.46                       |      |

|                     |               |   |       |   |            |      |
|---------------------|---------------|---|-------|---|------------|------|
| Verdeelde belasting | $u_{bij}$     | = | 17.35 | < | 18.45 [mm] | 0.94 |
| Verdeelde belasting | $u_{net,fin}$ | = | 21.18 | < | 24.60 [mm] | 0.86 |

### 3.7 Staartbalken trapaveling

Bestaande balklaag voldoet

Technosoft Construct release 6.74  
 2024

11 dec

Project : 240772  
 Onderdeel : balklagen  
 Datum : 11/12/2024  
 Eenheden : kN/m/rad  
 Bestand : G:\.shortcut-targets-by-id\0ByYUb81WrbDqYlpOSXRzaHdIV0E\Projecten\2024\240772\Houtconstructie\balklagen.cnw

#### Toegepaste normen volgens Eurocode met Nederlandse NB

|             |                      |                 |              |
|-------------|----------------------|-----------------|--------------|
| Belastingen | NEN-EN 1990:2002     | C2:2010,A1:2019 | NB:2019 (nl) |
|             | NEN-EN 1991-1-1:2002 | C1/C11:2019     | NB:2019 (nl) |
| Hout        | NEN-EN 1995-1-1:2005 | A1:2011,C1:2006 | NB:2013 (nl) |
|             | NEN-EN 14080:2013    |                 |              |

#### Balklaag berekening. (H)

##### Algemene gegevens

|                        |        |          |                                              |      |
|------------------------|--------|----------|----------------------------------------------|------|
| B x H                  | [mm] : | 95 x 265 | Sterkteklasse :                              | C18  |
| Overspanning           | [mm] : | 3000     | Klimaatklasse :                              | I    |
| Opleglengte            | [mm] : | 100      | Referentie periode [j] :                     | 50   |
| H.o.h. afstand         | [mm] : | 875      | Min. eigenfreq. [Hz] :                       | 3    |
| Beschot sterkteklasse: |        | C24      |                                              |      |
| Dikte beschot          | [mm] : | 12       | $E_{0,mean} \times I$ [Nm <sup>2</sup> /m] : | 1584 |

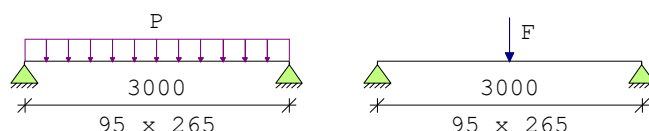
##### Permanente belastingen

$G_{rep}$

|                             |   |       |
|-----------------------------|---|-------|
| EG balklaag                 | : | 0.35  |
| Extra belasting             | : | 0.55+ |
| Totaal [kN/m <sup>2</sup> ] | : | 0.90  |

##### Veranderlijke belastingen

|                                         |   |             |        |      |
|-----------------------------------------|---|-------------|--------|------|
| $q_k + P_{wanden}$ [kN/m <sup>2</sup> ] | : | 3.00 =      | 2.50 + | 0.50 |
| $\Psi_0$ [ - ]                          | : | 0.40        |        |      |
| $\Psi_2$ [ - ]                          | : | 0.30        |        |      |
| $Q_k$ [kN]                              | : | 3.00        |        |      |
| $Q_k$ oppervlak [m <sup>2</sup> ]       | : | 0.50 x 0.50 |        |      |
| Reductiefactor                          | : | 1.00        |        |      |



Belastingfactoren (NEN-EN 1990)

|                |                  |      |              |      |
|----------------|------------------|------|--------------|------|
| Formule 6.10a: | $\gamma_G$ :     | 1.35 | $\gamma_Q$ : | 1.50 |
| Formule 6.10b: | $\xi \gamma_G$ : | 1.20 | $\gamma_Q$ : | 1.50 |

Partiële factor (Tabel 2.3 NEN-EN 1995-1-1)

$\gamma_M [-]: 1.30$ 

Meegenomen combinaties in de berekening :

|                                                | $k_{mod} [-]$ | $b_{ef} [mm]$ | $k_{c,90,q}$ |
|------------------------------------------------|---------------|---------------|--------------|
| $k_{c,90,F}$                                   |               |               |              |
| * Permanent ( $G_{rep}$ )                      | 0.60          | 95            |              |
| * Perm. + q-last (6.10a) ( $G_{rep} + q_k$ )   | 0.80          | 95            | 1.00         |
| * Perm. + q-last (6.10b) ( $G_{rep} + q_k$ )   | 0.80          | 95            | 1.00         |
| * Perm. + puntlast (6.10a) ( $G_{rep} + Q_k$ ) | 0.80          | 95            | 1.00         |
| 1.00                                           |               |               |              |
| * Perm. + puntlast (6.10b) ( $G_{rep} + Q_k$ ) | 0.80          | 95            | 1.00         |
| 1.00                                           |               |               |              |

**Resultaten (maatgevende combinaties)****eis****u.c.**

Perm + qlast(6.10b) frm(6.11)  $\sigma_{m,y,d} = 4.94 < 11.08 [N/mm^2]$  0.45  
 Perm + qlast(6.10b) frm(6.13)  $\tau_{v,d} = 0.43 < 2.09 [N/mm^2]$  0.20  
 Perm + qlast(6.10b) frm(6.3)  $\sigma_{c,90,q,d} / (k_{c,90,q} * f_{c,90,d}) +$   
 $\sigma_{c,90,F,d} / (k_{c,90,F} * f_{c,90,d}) < 1.00$   
 $= 0.76 / 1.35 + 0.00 / 1.35 = 0.56$

Verdeelde belasting  $u_{bij} = 2.84 < 9.00 [mm]$  0.32  
 Verdeelde belasting  $u_{net,fin} = 3.46 < 12.00 [mm]$  0.29

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



### 3.8 Spant tpv trap

#### q1

|            | $\psi_0$ | breedte | lengte | kN/m <sup>2</sup> | kN/m <sup>1</sup> |       | kN/m <sup>2</sup> | kN/m <sup>1</sup> |
|------------|----------|---------|--------|-------------------|-------------------|-------|-------------------|-------------------|
| schuin dak | 1        | 1,00    | 3,00   | 0,80              | <u>2,40</u>       | extr. | 0,00              | <u>0,00</u>       |
|            |          |         |        | $G_k =$           | 2,4               |       | $q_k =$           | 0,0               |

#### q2

|               | $\psi_0$ | breedte | lengte | kN/m <sup>2</sup> | kN/m <sup>1</sup> |       | kN/m <sup>2</sup> | kN/m <sup>1</sup> |
|---------------|----------|---------|--------|-------------------|-------------------|-------|-------------------|-------------------|
| 3e verdieping | 1        | 1,00    | 0,90   | 0,90              | <u>0,81</u>       | extr. | 3,00              | <u>2,70</u>       |
|               |          |         |        | $G_k =$           | 0,8               |       | $q_k =$           | 2,7               |

Technosoft Raamwerken release 6.82  
2024

11 dec

```
Project.....: 240772
Onderdeel....: spant
Dimensies....: kN;m;rad   (tenzij anders aangegeven)
Datum.....: 11/12/2024
Bestand.....: G:\.shortcut-targets-by-id\0ByYUub81WrbDqYlpOSXRzaHdIV0E\
               Projecten\2024\240772\Houtconstructie\spant bestand.rww
```

```
Belastingbreedte.: 3.000
Rekenmodel.....: 2e-orde-elastisch.
Theorieën voor de bepaling van de krachtsverdeling:
1) Uiterste grenstoestand:
   Geometrisch niet lineair alle staven.
   Fysisch lineair alle staven.
2) Gebruiksgrenstoestand:
   Lineaire-elasticiteitstheorie
```

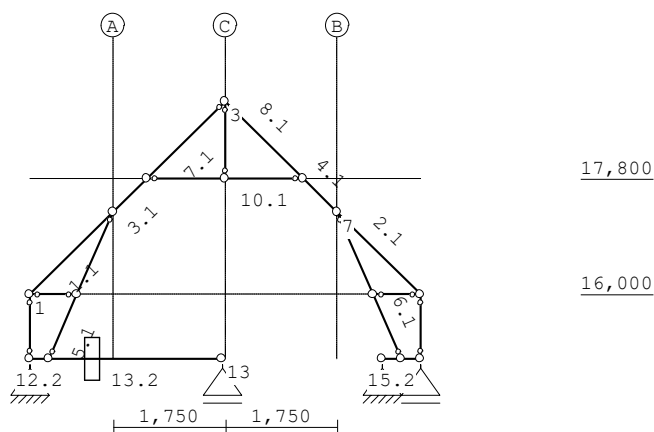
```
Maximum aantal iteraties.....: 50
Max.deellengte kolommen/wanden: 0.500 Max.deellengte balken/vloeren: 0.500
Max. X-verplaatsing in UGT....: 0.500 Max. Z-verplaatsing in UGT...: 0.250
```

Gunstige werking van de permanente belasting wordt automatisch verwerkt.

Toegepaste normen volgens Eurocode met Nederlandse NB

|             |                      |                 |             |
|-------------|----------------------|-----------------|-------------|
| Belastingen | NEN-EN 1990:2002     | C2:2010,A1:2019 | NB:2019(nl) |
|             | NEN-EN 1991-1-1:2002 | C1/C11:2019     | NB:2019(nl) |
|             | NEN-EN 1991-1-3:2003 | C1:2009         | NB:2011(nl) |
|             | NEN-EN 1991-1-4:2005 | C2:2011         | NB:2011(nl) |
| Hout        | NEN-EN 1995-1-1:2005 | A1:2011,C1:2006 | NB:2013(nl) |

# GEOMETRIE



## STRAMIENLIJNEN

| Nr. | Naam | X     | Z-min  | Z-max  |
|-----|------|-------|--------|--------|
| 1   | A    | 1.300 | 15.000 | 19.000 |
| 2   | B    | 4.800 | 15.000 | 19.000 |
| 3   | C    | 3.050 | 15.000 | 19.000 |

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



Project.....: 240772  
Onderdeel.....: spant

#### NIVEAUS

| Nr. | Z      | X-min | X-max |
|-----|--------|-------|-------|
| 1   | 16.000 | 0.000 | 6.100 |
| 2   | 17.800 | 0.000 | 6.100 |

#### MATERIALEN

| Mt | Kwaliteit | E-modulus [N/mm <sup>2</sup> ] | S.G. | S.G.verhoogd | Pois. | Uitz. coëff |
|----|-----------|--------------------------------|------|--------------|-------|-------------|
| 1  | C18       | 9000                           | 3.2  | 3.8          | 1.00  | 5.0000e-06  |

Bij de bepaling v.h. e.g. van houten staven is de S.G.verhoogd toegepast.

#### PROFIELEN [mm]

| Prof. | Omschrijving | Materiaal | Oppervlak  | Traagheid  | Vormf. |
|-------|--------------|-----------|------------|------------|--------|
| 1     | B*H 100*220  | 1:C18     | 2.2000e+04 | 8.8733e+07 | 0.00   |
| 2     | B*H 95*265   | 1:C18     | 2.5175e+04 | 1.4733e+08 | 0.00   |

#### PROFIELEN vervolg [mm]

| Prof. | Staaftype | Breedte | Hoogte | e     | Type | b1 | h1 | b2 | h2 |
|-------|-----------|---------|--------|-------|------|----|----|----|----|
| 1     | 0:Normaal | 100     | 220    | 110.0 | 0:RH |    |    |    |    |
| 2     | 0:Normaal | 95      | 265    | 132.5 | 0:RH |    |    |    |    |

#### PROFIELVORMEN [mm]

|   |             |                                                                                     |
|---|-------------|-------------------------------------------------------------------------------------|
| 1 | B*H 100*220 |   |
| 2 | B*H 95*265  |  |

#### KNOPEN

| Knoop | X     | Z      | Knoop | X     | Z      |
|-------|-------|--------|-------|-------|--------|
| 1     | 0.000 | 16.000 | 6     | 1.300 | 17.279 |
| 2     | 6.100 | 16.000 | 7     | 4.800 | 17.279 |
| 3     | 3.050 | 19.000 | 8     | 1.830 | 17.800 |
| 4     | 0.300 | 15.000 | 9     | 4.270 | 17.800 |
| 5     | 5.800 | 15.000 | 10    | 3.050 | 17.800 |
| 11    | 0.000 | 15.000 | 16    | 5.361 | 16.000 |
| 12    | 6.100 | 15.000 |       |       |        |
| 13    | 3.000 | 15.000 |       |       |        |
| 14    | 5.500 | 15.000 |       |       |        |
| 15    | 0.739 | 16.000 |       |       |        |

#### STAVEN

| St. | ki | kj | Profiel       | Aansl.i | Aansl.j | Lengte | Opm. |
|-----|----|----|---------------|---------|---------|--------|------|
| 1   | 1  | 6  | 1:B*H 100*220 | NDM     | NDM     | 1.823  |      |
| 2   | 2  | 7  | 1:B*H 100*220 | NDM     | NDM     | 1.823  |      |
| 3   | 6  | 8  | 1:B*H 100*220 | NDM     | NDM     | 0.743  |      |
| 4   | 7  | 9  | 1:B*H 100*220 | NDM     | NDM     | 0.743  |      |
| 5   | 4  | 15 | 1:B*H 100*220 | ND-     | NDM     | 1.092  |      |
| 6   | 5  | 16 | 1:B*H 100*220 | ND-     | NDM     | 1.092  |      |
| 7   | 8  | 3  | 1:B*H 100*220 | NDM     | ND-     | 1.711  |      |
| 8   | 9  | 3  | 1:B*H 100*220 | NDM     | NDM     | 1.711  |      |
| 9   | 8  | 10 | 1:B*H 100*220 | ND-     | NDM     | 1.220  |      |
| 10  | 10 | 9  | 1:B*H 100*220 | NDM     | ND-     | 1.220  |      |
| 11  | 10 | 3  | 1:B*H 100*220 | ND-     | ND-     | 1.200  |      |
| 12  | 11 | 4  | 2:B*H 95*265  | NDM     | NDM     | 0.300  |      |

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



Project.....: 240772  
Onderdeel.....: spant

#### STAVEN

| St. | ki | kj | Profiel       | Aansl.i | Aansl.j | Lengte | Opm. |
|-----|----|----|---------------|---------|---------|--------|------|
| 13  | 4  | 13 | 2:B*H 95*265  | NDM     | NDM     | 2.700  |      |
| 14  | 11 | 1  | 1:B*H 100*220 | ND-     | ND-     | 1.000  |      |
| 15  | 14 | 5  | 2:B*H 95*265  | NDM     | NDM     | 0.300  |      |
| 16  | 5  | 12 | 2:B*H 95*265  | NDM     | NDM     | 0.300  |      |
| 17  | 12 | 2  | 1:B*H 100*220 | ND-     | ND-     | 1.000  |      |
| 18  | 15 | 6  | 1:B*H 100*220 | NDM     | ND-     | 1.396  |      |
| 19  | 16 | 7  | 1:B*H 100*220 | NDM     | ND-     | 1.396  |      |
| 20  | 1  | 15 | 1:B*H 100*220 | ND      | ND-     | 0.739  |      |
| 21  | 16 | 2  | 1:B*H 100*220 | ND      | ND-     | 0.739  |      |

#### VASTE STEUNPUNTEN

| Nr. | knoop | Kode | XZR | 1=vast | 0=vrij | Hoek |
|-----|-------|------|-----|--------|--------|------|
| 1   | 11    | 110  |     |        |        | 0.00 |
| 2   | 12    | 010  |     |        |        | 0.00 |
| 3   | 13    | 010  |     |        |        | 0.00 |
| 4   | 14    | 110  |     |        |        | 0.00 |

#### BELASTINGGENERATIE ALGEMEEN.

Betrouwbaarheidsklasse.....: 2 Referentieperiode.....: 50  
Gebouwdiepte.....: 10.00 Gebouwhoogte.....: 19.00  
Niveau aansl.terrein.....: 0.00 E.g. scheid.w. [kN/m2]: 0.00

#### WIND

Terrein categorie ...[4.3.2]...: Bebouwd  
Windgebied .....: 2 Vb,0 ..[4.2].....: 27.000  
Positie spant in het gebouw....: 0.000 Kr ....[4.3.2].....: 0.223  
z0 .....[4.3.2]...: 0.500 Zmin ..[4.3.2].....: 7.000  
Co wind van links ..[4.3.3]...: 1.000 Co wind van rechts....: 1.000  
Co wind loodrecht ..[4.3.3]...: 1.000  
Cpi wind van links ..[7.2.9]...: 0.200 -0.300  
Cpi windloodrecht ...[7.2.9]...: 0.200 -0.300  
Cpi wind van rechts ..[7.2.9]...: 0.200 -0.300  
Cfr windwrijving ....[7.5].....: 0.040

#### SNEEUW

Sneeuwbelasting (sk) 50 jaar : 0.70  
Sneeuwbelasting (sn) n jaar : 0.70

#### STAFTYPEN

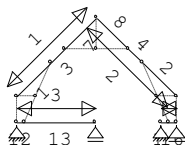
| Type             | staven           |
|------------------|------------------|
| 1:Vloer.         | : 12,13,15,16    |
| 4:Wand / kolom.  | : 11             |
| 5:Linker gevel.  | : 14             |
| 6:Rechter gevel. | : 17             |
| 7:Dak.           | : 1-4,7,8        |
| 9:Open.          | : 5,6,9,10,18-21 |

Project.....: 240772

Onderdeel.....: spant

**LASTVELDEN**

Veranderlijke belastingen door personen

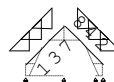
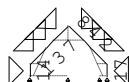
**LASTVELDEN**

| Nr | Staaf | Tabel | Klasse-Gebruiksfunctie   | Verd. | $q_k$ | $Q_k$ | $F_t / F_{t,0}$ |
|----|-------|-------|--------------------------|-------|-------|-------|-----------------|
| 1  | 1-7   | 6.10  | H-Dak (onder dakbeschot) | 0     | 0.00  | -2.00 | 1.00            |
| 2  | 2-8   | 6.10  | H-Dak (onder dakbeschot) | 0     | 0.00  | -2.00 | 1.00            |
| 3  | 12-13 | 6.2   | A-Vloeren                | 0     | -1.75 | -3.00 | 1.00            |
| 4  | 15-16 | 6.2   | A-Vloeren                | 0     | -1.75 | -3.00 | 1.00            |

**LASTVELDEN**

Wind staven

Sneeuw staven

**WIND DAKTYPES**

| Nr. | Staaf | Type     | reductie bij<br>wind van links | reductie bij<br>wind van rechts | Cpe volgens art: |
|-----|-------|----------|--------------------------------|---------------------------------|------------------|
| 1   | 14    | Gevel    | 1.000                          | 1.000                           | 7.2.2            |
| 2   | 1-7   | Zadeldak | 1.000                          | 1.000                           | 7.2.5            |
| 3   | 8-2   | Zadeldak | 1.000                          | 1.000                           | 7.2.5            |
| 4   | 17    | Gevel    | 1.000                          | 1.000                           | 7.2.2            |

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie

IRg

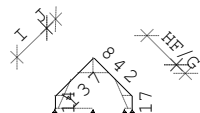
Project.....: 240772  
Onderdeel.....: spant

## WIND ZONES

Wind van links



Wind van rechts



### WIND VAN LINKS ZONES

| Nr. | Staaft | Positie | Lengte | Zone |
|-----|--------|---------|--------|------|
| 1   | 14     | 0.000   | 1.000  | D    |
| 2   | 1-7    | 0.000   | 1.000  | F/G  |
| 3   | 1-7    | 1.000   | 3.278  | H    |
| 4   | 8-2    | 0.000   | 1.000  | J    |
| 5   | 8-2    | 1.000   | 3.278  | I    |
| 6   | 17     | 0.000   | 1.000  | E    |

### WIND VAN RECHTS ZONES

| Nr. | Staaft | Positie | Lengte | Zone |
|-----|--------|---------|--------|------|
| 1   | 17     | 0.000   | 1.000  | D    |
| 2   | 8-2    | 0.000   | 1.000  | F/G  |
| 3   | 8-2    | 1.000   | 3.278  | H    |
| 4   | 1-7    | 0.000   | 1.000  | J    |
| 5   | 1-7    | 1.000   | 3.278  | I    |
| 6   | 14     | 0.000   | 1.000  | E    |

### Wind indexen

| Index | CsCd | Cpe/Cpi | qp    | breedte | reductie | Qw     | Zone | Hoek(en) |
|-------|------|---------|-------|---------|----------|--------|------|----------|
| Qw1   |      | 0.300   | 0.877 | 3.000   |          | -0.789 | -i   |          |
| Qw2   |      | -0.300  | 0.877 | 3.000   |          | 0.789  | -i   |          |
| Qw3   | 1.00 | 0.800   | 0.877 | 3.000   |          | -2.104 | D    |          |
| Qw4   | 1.00 | 0.700   | 0.877 | 2.500   |          | -1.534 | F    | 44.5     |
| Qw5   | 1.00 | 0.700   | 0.877 | 0.500   |          | -0.307 | G    | 44.5     |
| Qw6   | 1.00 | 0.593   | 0.877 | 3.000   |          | -1.561 | H    | 44.5     |
| Qw7   | 1.00 | 0.307   | 0.877 | 3.000   |          | -0.807 | J    | 44.5     |
| Qw8   | 1.00 | 0.207   | 0.877 | 3.000   |          | -0.544 | I    | 44.5     |
| Qw9   | 1.00 | 0.606   | 0.877 | 3.000   |          | -1.593 | E    |          |
| Qw10  |      | -0.200  | 0.877 | 3.000   |          | 0.526  | +i   |          |
| Qw11  |      | 0.200   | 0.877 | 3.000   |          | -0.526 | +i   |          |
| Qw12  | 1.00 | -0.017  | 0.877 | 2.500   |          | 0.037  | F    | 44.5     |
| Qw13  | 1.00 | -0.017  | 0.877 | 0.500   |          | 0.007  | G    | 44.5     |
| Qw14  | 1.00 | -0.007  | 0.877 | 3.000   |          | 0.018  | H    | 44.5     |
| Qw15  | 1.00 | -0.800  | 0.877 | 3.000   |          | 2.104  | D    |          |
| Qw16  | 1.00 | -0.700  | 0.877 | 2.500   |          | 1.534  | F    | 44.5     |
| Qw17  | 1.00 | -0.700  | 0.877 | 0.500   |          | 0.307  | G    | 44.5     |
| Qw18  | 1.00 | -0.593  | 0.877 | 3.000   |          | 1.561  | H    | 44.5     |
| Qw19  | 1.00 | -0.307  | 0.877 | 3.000   |          | 0.807  | J    | 44.5     |
| Qw20  | 1.00 | -0.207  | 0.877 | 3.000   |          | 0.544  | I    | 44.5     |
| Qw21  | 1.00 | -0.606  | 0.877 | 3.000   |          | 1.593  | E    |          |
| Qw22  | 1.00 | 0.017   | 0.877 | 2.500   |          | -0.037 | F    | 44.5     |
| Qw23  | 1.00 | 0.017   | 0.877 | 0.500   |          | -0.007 | G    | 44.5     |
| Qw24  | 1.00 | 0.007   | 0.877 | 3.000   |          | -0.018 | H    | 44.5     |

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



Project.....: 240772  
Onderdeel.....: spant

#### SNEEUW DAKTYPEN

Staaf artikel

1-7 5.3.3 Zadel dak  
8-2 5.3.3 Zadel dak

#### Sneeuw indexen

| Index | art   | $\mu$ | $s_k$ | red. posfac | breedte | $Q_s$ | hoek |
|-------|-------|-------|-------|-------------|---------|-------|------|
| Qs1   | 5.3.3 | 0.413 | 0.70  | 1.00        | 3.000   | 0.867 | 44.5 |
| Qs2   | 5.3.3 | 0.206 | 0.70  | 1.00        | 3.000   | 0.433 | 44.5 |

#### BELASTINGGEVALLEN

| B.G. | Omschrijving                    | Type |
|------|---------------------------------|------|
|      | 1 Permanente belasting EGZ=0.00 | 1    |
| g*   | 2 Ver. bel. pers. ed. ( $q_k$ ) | 2    |
| g    | 3 Ver. bel. pers. ed. ( $Q_k$ ) | 3    |
| g    | 4 Wind van links onderdruk A    | 7    |
| g    | 5 Wind van links overdruk A     | 8    |
| g    | 6 Wind van links onderdruk B    | 9    |
| g    | 7 Wind van links overdruk B     | 10   |
| g    | 8 Wind van links onderdruk C    | 37   |
| g    | 9 Wind van links overdruk C     | 38   |
| g    | 10 Wind van links onderdruk D   | 39   |
| g    | 11 Wind van links overdruk D    | 40   |
| g    | 12 Wind van rechts onderdruk A  | 11   |
| g    | 13 Wind van rechts overdruk A   | 12   |
| g    | 14 Wind van rechts onderdruk B  | 13   |
| g    | 15 Wind van rechts overdruk B   | 14   |
| g    | 16 Wind van rechts onderdruk C  | 41   |
| g    | 17 Wind van rechts overdruk C   | 42   |
| g    | 18 Wind van rechts onderdruk D  | 43   |
| g    | 19 Wind van rechts overdruk D   | 44   |
| g    | 20 Sneeuw A                     | 22   |
| g    | 21 Sneeuw B                     | 23   |
| g    | 22 Sneeuw C                     | 33   |

g = gegenereerd belastinggeval

\* = belastinggeval bevat 1 of meer handmatig toegevoegde en/of gewijzigde lasten

#### BELASTINGGEVALLEN vervolg

| B.G. | Omschrijving                    | Belastingduurklasse |
|------|---------------------------------|---------------------|
|      | 1 Permanente belasting          | Blijvend            |
|      | 2 Ver. bel. pers. ed. ( $q_k$ ) | Middellang          |
|      | 3 Ver. bel. pers. ed. ( $Q_k$ ) | Middellang          |
|      | 4 Wind van links onderdruk A    | Kort                |
|      | 5 Wind van links overdruk A     | Kort                |
|      | 6 Wind van links onderdruk B    | Kort                |
|      | 7 Wind van links overdruk B     | Kort                |
|      | 8 Wind van links onderdruk C    | Kort                |
|      | 9 Wind van links overdruk C     | Kort                |
|      | 10 Wind van links onderdruk D   | Kort                |
|      | 11 Wind van links overdruk D    | Kort                |
|      | 12 Wind van rechts onderdruk A  | Kort                |
|      | 13 Wind van rechts overdruk A   | Kort                |
|      | 14 Wind van rechts onderdruk B  | Kort                |
|      | 15 Wind van rechts overdruk B   | Kort                |

Project.....: 240772

Onderdeel.....: spant

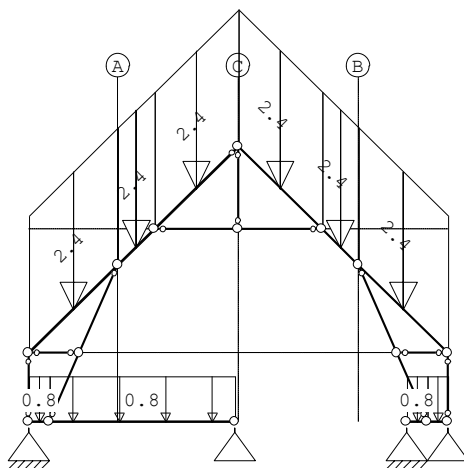
**BELASTINGGEVALLEN vervolg**

| B.G. | Omschrijving                | Belastingduurklasse |
|------|-----------------------------|---------------------|
| 16   | Wind van rechts onderdruk C | Kort                |
| 17   | Wind van rechts overdruk C  | Kort                |
| 18   | Wind van rechts onderdruk D | Kort                |
| 19   | Wind van rechts overdruk D  | Kort                |
| 20   | Sneeuw A                    | Kort                |
| 21   | Sneeuw B                    | Kort                |
| 22   | Sneeuw C                    | Kort                |

**BELASTINGEN**

B.G:1 Permanente

belasting

**STAAFBELASTINGEN**

B.G:1 Permanente

belasting

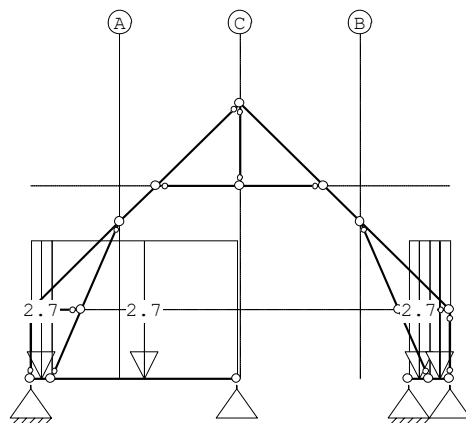
| Staat | Type       | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|-------|------------|--------|-------|-------|-------|----------|----------|----------|
| 1     | 5:QZGloaal | -2.40  | -2.40 | 0.000 | 0.000 |          |          |          |
| 3     | 5:QZGloaal | -2.40  | -2.40 | 0.000 | 0.000 |          |          |          |
| 7     | 5:QZGloaal | -2.40  | -2.40 | 0.000 | 0.000 |          |          |          |
| 8     | 5:QZGloaal | -2.40  | -2.40 | 0.000 | 0.000 |          |          |          |
| 4     | 5:QZGloaal | -2.40  | -2.40 | 0.000 | 0.000 |          |          |          |
| 2     | 5:QZGloaal | -2.40  | -2.40 | 0.000 | 0.000 |          |          |          |
| 12    | 1:QZLokaal | -0.80  | -0.80 | 0.000 | 0.000 |          |          |          |
| 13    | 1:QZLokaal | -0.80  | -0.80 | 0.000 | 0.000 |          |          |          |
| 15    | 1:QZLokaal | -0.80  | -0.80 | 0.000 | 0.000 |          |          |          |
| 16    | 1:QZLokaal | -0.80  | -0.80 | 0.000 | 0.000 |          |          |          |

Project.....: 240772

Onderdeel.....: spant

**BELASTINGEN**

B.G:2 Ver. bel. pers. ed.

(q<sub>k</sub>)**STAAFBELASTINGEN**

B.G:2 Ver. bel. pers. ed.

(q<sub>k</sub>)

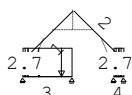
| Staaftype      | Index | q1/p/m | q2    | A     | B     | ψ <sub>0</sub> | ψ <sub>1</sub> | ψ <sub>2</sub> |
|----------------|-------|--------|-------|-------|-------|----------------|----------------|----------------|
| 12 3:QZgeProj. | *     | -2.70  | -2.70 | 0.000 | 0.000 | 0.40           | 0.50           | 0.30           |
| 13 3:QZgeProj. | *     | -2.70  | -2.70 | 0.000 | 0.000 | 0.40           | 0.50           | 0.30           |
| 15 3:QZgeProj. | *     | -2.70  | -2.70 | 0.000 | 0.000 | 0.40           | 0.50           | 0.30           |
| 16 3:QZgeProj. | *     | -2.70  | -2.70 | 0.000 | 0.000 | 0.40           | 0.50           | 0.30           |

Opmerkingen

[\*] Deze belasting is handmatig toegevoegd of gewijzigd.

**SITUATIES BELAST/ONBELAST**

B.G:2 Ver. bel. pers. ed.

(q<sub>k</sub>)**SITUATIES BELAST/ONBELAST**Belastingtype: q<sub>k</sub>

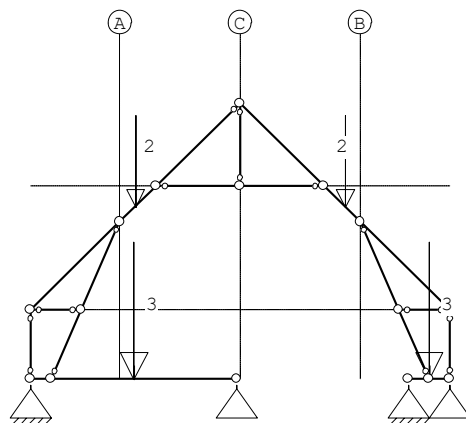
| Nr Lastvelden belast | Lastvelden onbelast |
|----------------------|---------------------|
| 1 1-4                |                     |

Project.....: 240772

Onderdeel.....: spant

**BELASTINGEN**

B.G:3 Ver. bel. pers. ed.

(Q<sub>k</sub>)**STAAFBELASTINGEN**

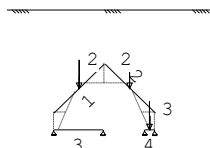
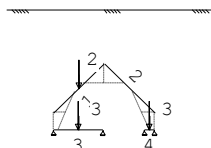
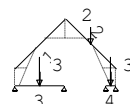
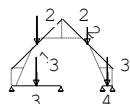
B.G:3 Ver. bel. pers. ed.

(Q<sub>k</sub>)

| Staaft | Type          | q1/p/m | q2 | A     | B | ψ <sub>0</sub> | ψ <sub>1</sub> | ψ <sub>2</sub> |
|--------|---------------|--------|----|-------|---|----------------|----------------|----------------|
| 3      | 10:PZGeprojl. | -2.00  |    | 0.316 |   | 0.00           | 0.00           | 0.00           |
| 4      | 10:PZGeprojl. | -2.00  |    | 0.316 |   | 0.00           | 0.00           | 0.00           |
| 13     | 10:PZGeprojl. | -3.00  |    | 1.200 |   | 0.40           | 0.50           | 0.30           |
| 15     | 10:PZGeprojl. | -3.00  |    | 0.300 |   | 0.40           | 0.50           | 0.30           |

**SITUATIES BELAST/ONBELAST**

B.G:3 Ver. bel. pers. ed.

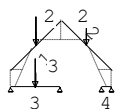
(Q<sub>k</sub>)

Project.....: 240772

Onderdeel....: spant

## SITUATIES BELAST/ONBELAST

B.G:3 Ver. bel. pers. ed.

 $(Q, k)$ 

## SITUATIES BELAST/ONBELAST

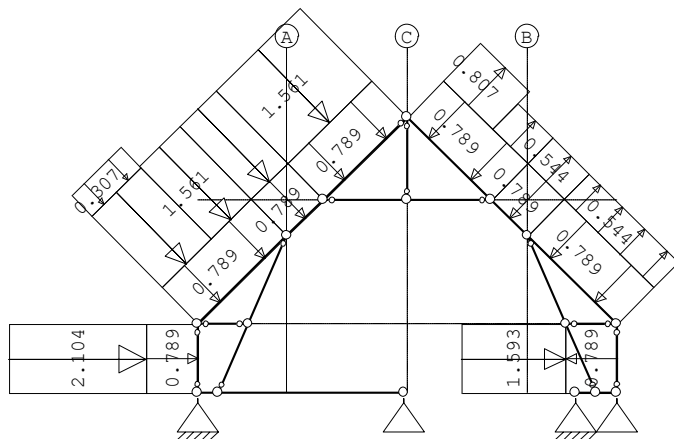
Belastingtype: Q k

| Nr Lastvelden belast | Lastvelden onbelast |
|----------------------|---------------------|
| 1 1-4                |                     |
| 2 2-4                | 1                   |
| 3 1, 3, 4            | 2                   |
| 4 1, 2, 4            | 3                   |
| 5 1-3                | 4                   |

## BELASTINGEN

B.G:4 Wind van links

onderdruk A



## STAAFBELASTINGEN

B.G:4 Wind van links

onderdruk A

| Staaf | Type       | Index | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|-------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 14    | 1:QZLokaal | Qw1   | -0.79  | -0.79 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw1   | -0.79  | -0.79 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3     | 1:QZLokaal | Qw1   | -0.79  | -0.79 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7     | 1:QZLokaal | Qw1   | -0.79  | -0.79 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 8     | 1:QZLokaal | Qw2   | 0.79   | 0.79  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 4     | 1:QZLokaal | Qw2   | 0.79   | 0.79  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2     | 1:QZLokaal | Qw2   | 0.79   | 0.79  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 17    | 1:QZLokaal | Qw2   | 0.79   | 0.79  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 14    | 1:QZLokaal | Qw3   | -2.10  | -2.10 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw4   | -1.53  | -1.53 | 0.000 | 0.823 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw5   | -0.31  | -0.31 | 0.000 | 0.823 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw6   | -1.56  | -1.56 | 1.000 | 0.000 | 0.00     | 0.20     | 0.00     |

Project.....: 240772

Onderdeel.....: spant

**STAAFBELASTINGEN**

B.G:4 Wind van links

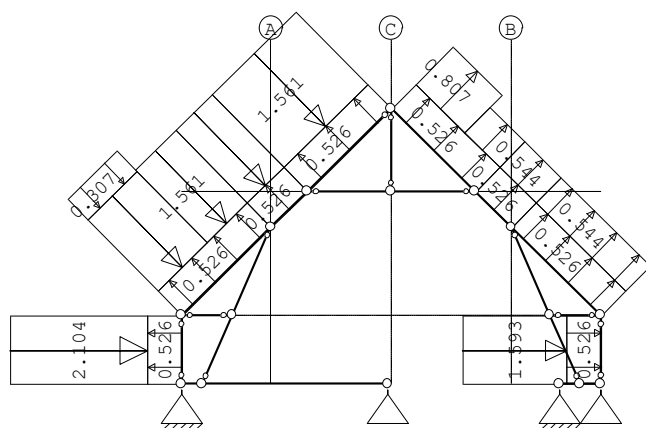
onderdruk A

| Staal | Type       | Index | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|-------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 3     | 1:QZLokaal | Qw6   | -1.56  | -1.56 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7     | 1:QZLokaal | Qw6   | -1.56  | -1.56 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 8     | 1:QZLokaal | Qw7   | -0.81  | -0.81 | 0.711 | 0.000 | 0.00     | 0.20     | 0.00     |
| 8     | 1:QZLokaal | Qw8   | -0.54  | -0.54 | 0.000 | 1.000 | 0.00     | 0.20     | 0.00     |
| 4     | 1:QZLokaal | Qw8   | -0.54  | -0.54 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2     | 1:QZLokaal | Qw8   | -0.54  | -0.54 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 17    | 1:QZLokaal | Qw9   | -1.59  | -1.59 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |

**BELASTINGEN**

B.G:5 Wind van links

overdruk A

**STAAFBELASTINGEN**

B.G:5 Wind van links

overdruk A

| Staal | Type       | Index | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|-------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 14    | 1:QZLokaal | Qw10  | 0.53   | 0.53  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw10  | 0.53   | 0.53  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3     | 1:QZLokaal | Qw10  | 0.53   | 0.53  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7     | 1:QZLokaal | Qw10  | 0.53   | 0.53  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 8     | 1:QZLokaal | Qw11  | -0.53  | -0.53 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 4     | 1:QZLokaal | Qw11  | -0.53  | -0.53 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2     | 1:QZLokaal | Qw11  | -0.53  | -0.53 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 17    | 1:QZLokaal | Qw11  | -0.53  | -0.53 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 14    | 1:QZLokaal | Qw3   | -2.10  | -2.10 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw4   | -1.53  | -1.53 | 0.000 | 0.823 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw5   | -0.31  | -0.31 | 0.000 | 0.823 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw6   | -1.56  | -1.56 | 1.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3     | 1:QZLokaal | Qw6   | -1.56  | -1.56 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7     | 1:QZLokaal | Qw6   | -1.56  | -1.56 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 8     | 1:QZLokaal | Qw7   | -0.81  | -0.81 | 0.711 | 0.000 | 0.00     | 0.20     | 0.00     |
| 8     | 1:QZLokaal | Qw8   | -0.54  | -0.54 | 0.000 | 1.000 | 0.00     | 0.20     | 0.00     |
| 4     | 1:QZLokaal | Qw8   | -0.54  | -0.54 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2     | 1:QZLokaal | Qw8   | -0.54  | -0.54 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 17    | 1:QZLokaal | Qw9   | -1.59  | -1.59 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |

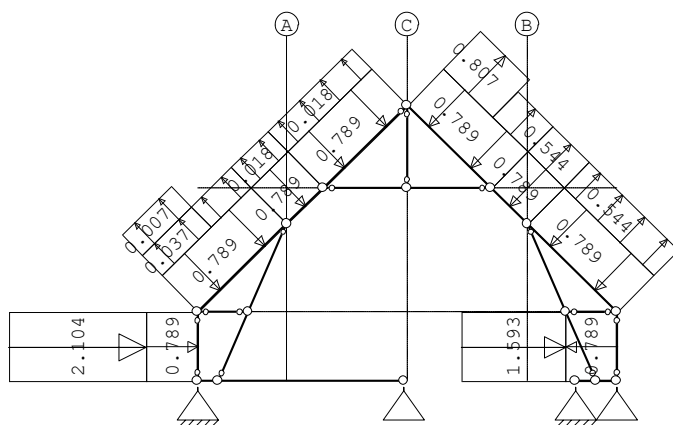
Project.....: 240772

Onderdeel.....: spant

**BELASTINGEN**

B.G:6 Wind van links

onderdruk B

**STAAFBELASTINGEN**

B.G:6 Wind van links

onderdruk B

| Staat | Type       | Index | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|-------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 14    | 1:QZLokaal | Qw1   | -0.79  | -0.79 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw1   | -0.79  | -0.79 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3     | 1:QZLokaal | Qw1   | -0.79  | -0.79 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7     | 1:QZLokaal | Qw1   | -0.79  | -0.79 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 8     | 1:QZLokaal | Qw2   | 0.79   | 0.79  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 4     | 1:QZLokaal | Qw2   | 0.79   | 0.79  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2     | 1:QZLokaal | Qw2   | 0.79   | 0.79  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 17    | 1:QZLokaal | Qw2   | 0.79   | 0.79  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 14    | 1:QZLokaal | Qw3   | -2.10  | -2.10 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw12  | 0.04   | 0.04  | 0.000 | 0.823 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw13  | 0.01   | 0.01  | 0.000 | 0.823 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw14  | 0.02   | 0.02  | 1.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3     | 1:QZLokaal | Qw14  | 0.02   | 0.02  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7     | 1:QZLokaal | Qw14  | 0.02   | 0.02  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 8     | 1:QZLokaal | Qw7   | -0.81  | -0.81 | 0.711 | 0.000 | 0.00     | 0.20     | 0.00     |
| 8     | 1:QZLokaal | Qw8   | -0.54  | -0.54 | 0.000 | 1.000 | 0.00     | 0.20     | 0.00     |
| 4     | 1:QZLokaal | Qw8   | -0.54  | -0.54 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2     | 1:QZLokaal | Qw8   | -0.54  | -0.54 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 17    | 1:QZLokaal | Qw9   | -1.59  | -1.59 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |

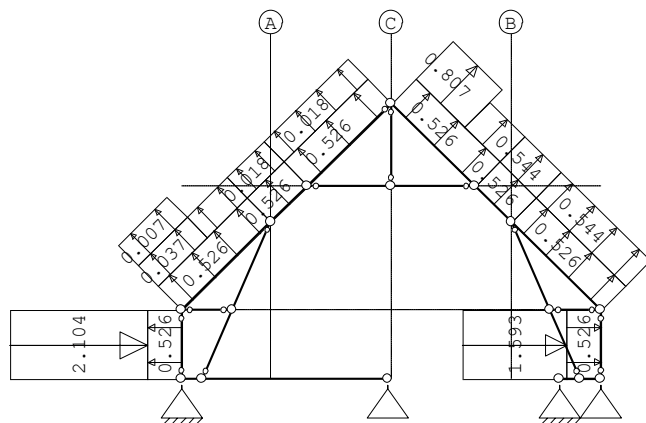
Project.....: 240772

Onderdeel....: spant

## BELASTINGEN

B.G:7 Wind van links

overdruk B



## STAAFBELASTINGEN

B.G:7 Wind van links

overdruk B

| Staaf | Type       | Index | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|-------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 14    | 1:QZLokaal | Qw10  | 0.53   | 0.53  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw10  | 0.53   | 0.53  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3     | 1:QZLokaal | Qw10  | 0.53   | 0.53  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7     | 1:QZLokaal | Qw10  | 0.53   | 0.53  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 8     | 1:QZLokaal | Qw11  | -0.53  | -0.53 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 4     | 1:QZLokaal | Qw11  | -0.53  | -0.53 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2     | 1:QZLokaal | Qw11  | -0.53  | -0.53 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 17    | 1:QZLokaal | Qw11  | -0.53  | -0.53 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 14    | 1:QZLokaal | Qw3   | -2.10  | -2.10 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw12  | 0.04   | 0.04  | 0.000 | 0.823 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw13  | 0.01   | 0.01  | 0.000 | 0.823 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw14  | 0.02   | 0.02  | 1.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3     | 1:QZLokaal | Qw14  | 0.02   | 0.02  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7     | 1:QZLokaal | Qw14  | 0.02   | 0.02  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 8     | 1:QZLokaal | Qw7   | -0.81  | -0.81 | 0.711 | 0.000 | 0.00     | 0.20     | 0.00     |
| 8     | 1:QZLokaal | Qw8   | -0.54  | -0.54 | 0.000 | 1.000 | 0.00     | 0.20     | 0.00     |
| 4     | 1:QZLokaal | Qw8   | -0.54  | -0.54 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2     | 1:QZLokaal | Qw8   | -0.54  | -0.54 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 17    | 1:QZLokaal | Qw9   | -1.59  | -1.59 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |

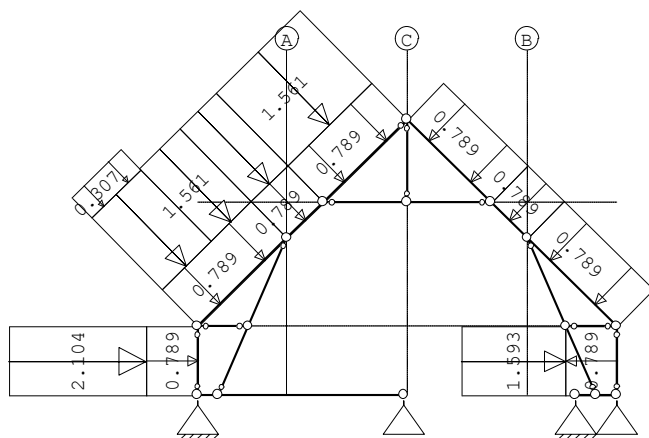
Project.....: 240772

Onderdeel.....: spant

**BELASTINGEN**

B.G:8 Wind van links

onderdruk C

**STAAFBELASTINGEN**

B.G:8 Wind van links

onderdruk C

| Staaftype | Type       | Index | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|-----------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 14        | 1:QZLokaal | Qw1   | -0.79  | -0.79 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1         | 1:QZLokaal | Qw1   | -0.79  | -0.79 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3         | 1:QZLokaal | Qw1   | -0.79  | -0.79 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7         | 1:QZLokaal | Qw1   | -0.79  | -0.79 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 8         | 1:QZLokaal | Qw2   | 0.79   | 0.79  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 4         | 1:QZLokaal | Qw2   | 0.79   | 0.79  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2         | 1:QZLokaal | Qw2   | 0.79   | 0.79  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 17        | 1:QZLokaal | Qw2   | 0.79   | 0.79  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 14        | 1:QZLokaal | Qw3   | -2.10  | -2.10 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1         | 1:QZLokaal | Qw4   | -1.53  | -1.53 | 0.000 | 0.823 | 0.00     | 0.20     | 0.00     |
| 1         | 1:QZLokaal | Qw5   | -0.31  | -0.31 | 0.000 | 0.823 | 0.00     | 0.20     | 0.00     |
| 1         | 1:QZLokaal | Qw6   | -1.56  | -1.56 | 1.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3         | 1:QZLokaal | Qw6   | -1.56  | -1.56 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7         | 1:QZLokaal | Qw6   | -1.56  | -1.56 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 17        | 1:QZLokaal | Qw9   | -1.59  | -1.59 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |

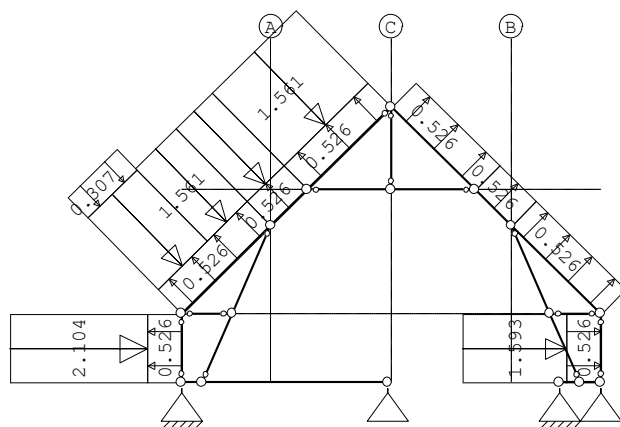
Project.....: 240772

Onderdeel.....: spant

**BELASTINGEN**

B.G:9 Wind van links

overdruk C

**STAAFBELASTINGEN**

B.G:9 Wind van links

overdruk C

| Staaft | Type       | Index | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|--------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 14     | 1:QZLokaal | Qw10  | 0.53   | 0.53  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1      | 1:QZLokaal | Qw10  | 0.53   | 0.53  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3      | 1:QZLokaal | Qw10  | 0.53   | 0.53  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7      | 1:QZLokaal | Qw10  | 0.53   | 0.53  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 8      | 1:QZLokaal | Qw11  | -0.53  | -0.53 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 4      | 1:QZLokaal | Qw11  | -0.53  | -0.53 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2      | 1:QZLokaal | Qw11  | -0.53  | -0.53 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 17     | 1:QZLokaal | Qw11  | -0.53  | -0.53 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 14     | 1:QZLokaal | Qw3   | -2.10  | -2.10 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1      | 1:QZLokaal | Qw4   | -1.53  | -1.53 | 0.000 | 0.823 | 0.00     | 0.20     | 0.00     |
| 1      | 1:QZLokaal | Qw5   | -0.31  | -0.31 | 0.000 | 0.823 | 0.00     | 0.20     | 0.00     |
| 1      | 1:QZLokaal | Qw6   | -1.56  | -1.56 | 1.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3      | 1:QZLokaal | Qw6   | -1.56  | -1.56 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7      | 1:QZLokaal | Qw6   | -1.56  | -1.56 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 17     | 1:QZLokaal | Qw9   | -1.59  | -1.59 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |

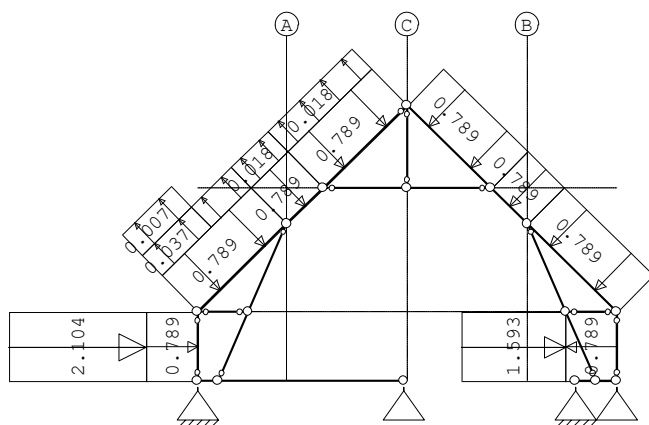
Project.....: 240772

Onderdeel....: spant

## BELASTINGEN

B.G:10 Wind van links

onderdruk D



## STAAFBELASTINGEN

B.G:10 Wind van links

onderdruk D

| Staaf | Type       | Index | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|-------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 14    | 1:QZLokaal | Qw1   | -0.79  | -0.79 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw1   | -0.79  | -0.79 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3     | 1:QZLokaal | Qw1   | -0.79  | -0.79 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7     | 1:QZLokaal | Qw1   | -0.79  | -0.79 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 8     | 1:QZLokaal | Qw2   | 0.79   | 0.79  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 4     | 1:QZLokaal | Qw2   | 0.79   | 0.79  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2     | 1:QZLokaal | Qw2   | 0.79   | 0.79  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 17    | 1:QZLokaal | Qw2   | 0.79   | 0.79  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 14    | 1:QZLokaal | Qw3   | -2.10  | -2.10 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw12  | 0.04   | 0.04  | 0.000 | 0.823 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw13  | 0.01   | 0.01  | 0.000 | 0.823 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw14  | 0.02   | 0.02  | 1.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3     | 1:QZLokaal | Qw14  | 0.02   | 0.02  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7     | 1:QZLokaal | Qw14  | 0.02   | 0.02  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 17    | 1:QZLokaal | Qw9   | -1.59  | -1.59 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |

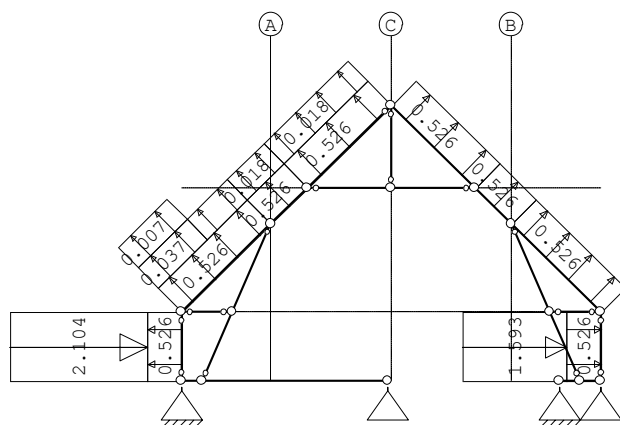
Project.....: 240772

Onderdeel.....: spant

**BELASTINGEN**

B.G:11 Wind van links

overdruk D

**STAAFBELASTINGEN**

B.G:11 Wind van links

overdruk D

| Staal | Type       | Index | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|-------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 14    | 1:QZLokaal | Qw10  | 0.53   | 0.53  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw10  | 0.53   | 0.53  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3     | 1:QZLokaal | Qw10  | 0.53   | 0.53  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7     | 1:QZLokaal | Qw10  | 0.53   | 0.53  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 8     | 1:QZLokaal | Qw11  | -0.53  | -0.53 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 4     | 1:QZLokaal | Qw11  | -0.53  | -0.53 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2     | 1:QZLokaal | Qw11  | -0.53  | -0.53 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 17    | 1:QZLokaal | Qw11  | -0.53  | -0.53 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 14    | 1:QZLokaal | Qw3   | -2.10  | -2.10 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw12  | 0.04   | 0.04  | 0.000 | 0.823 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw13  | 0.01   | 0.01  | 0.000 | 0.823 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw14  | 0.02   | 0.02  | 1.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3     | 1:QZLokaal | Qw14  | 0.02   | 0.02  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7     | 1:QZLokaal | Qw14  | 0.02   | 0.02  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 17    | 1:QZLokaal | Qw9   | -1.59  | -1.59 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |

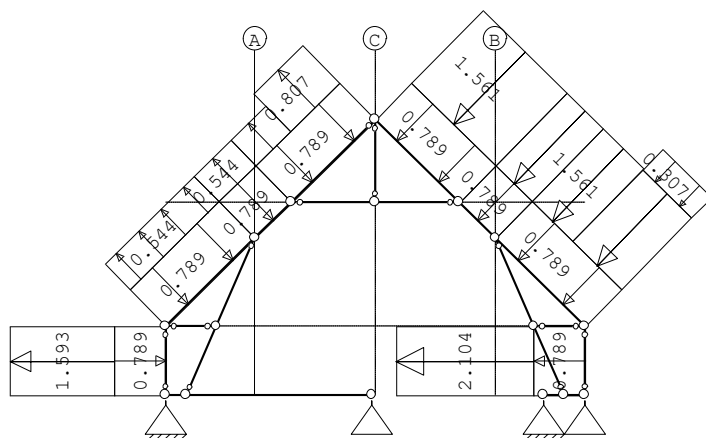
Project.....: 240772

Onderdeel.....: spant

**BELASTINGEN**

B.G:12 Wind van rechts

onderdruk A

**STAAFBELASTINGEN**

B.G:12 Wind van rechts

onderdruk A

| Staaftype | Type       | Index | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|-----------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 14        | 1:QZLokaal | Qw1   | -0.79  | -0.79 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1         | 1:QZLokaal | Qw1   | -0.79  | -0.79 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3         | 1:QZLokaal | Qw1   | -0.79  | -0.79 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7         | 1:QZLokaal | Qw1   | -0.79  | -0.79 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 8         | 1:QZLokaal | Qw2   | 0.79   | 0.79  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 4         | 1:QZLokaal | Qw2   | 0.79   | 0.79  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2         | 1:QZLokaal | Qw2   | 0.79   | 0.79  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 17        | 1:QZLokaal | Qw2   | 0.79   | 0.79  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 17        | 1:QZLokaal | Qw15  | 2.10   | 2.10  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2         | 1:QZLokaal | Qw16  | 1.53   | 1.53  | 0.000 | 0.823 | 0.00     | 0.20     | 0.00     |
| 2         | 1:QZLokaal | Qw17  | 0.31   | 0.31  | 0.000 | 0.823 | 0.00     | 0.20     | 0.00     |
| 2         | 1:QZLokaal | Qw18  | 1.56   | 1.56  | 1.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 4         | 1:QZLokaal | Qw18  | 1.56   | 1.56  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 8         | 1:QZLokaal | Qw18  | 1.56   | 1.56  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7         | 1:QZLokaal | Qw19  | 0.81   | 0.81  | 0.711 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7         | 1:QZLokaal | Qw20  | 0.54   | 0.54  | 0.000 | 1.000 | 0.00     | 0.20     | 0.00     |
| 3         | 1:QZLokaal | Qw20  | 0.54   | 0.54  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1         | 1:QZLokaal | Qw20  | 0.54   | 0.54  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 14        | 1:QZLokaal | Qw21  | 1.59   | 1.59  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |

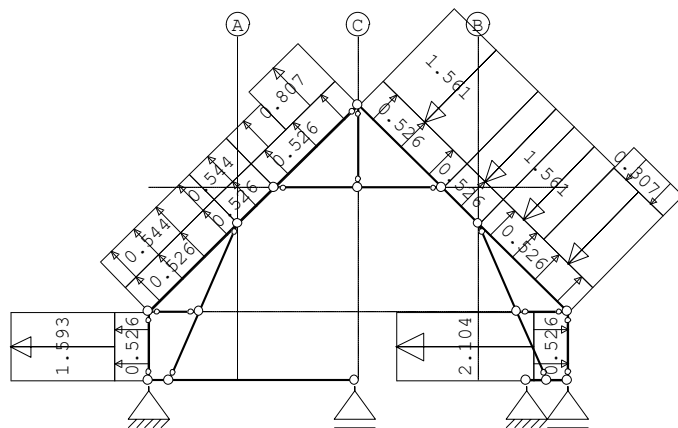
Project.....: 240772

Onderdeel.....: spant

**BELASTINGEN**

B.G:13 Wind van rechts

overdruk A

**STAAFBELASTINGEN**

B.G:13 Wind van rechts

overdruk A

| Staaft | Type       | Index | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|--------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 14     | 1:QZLokaal | Qw10  | 0.53   | 0.53  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1      | 1:QZLokaal | Qw10  | 0.53   | 0.53  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3      | 1:QZLokaal | Qw10  | 0.53   | 0.53  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7      | 1:QZLokaal | Qw10  | 0.53   | 0.53  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 8      | 1:QZLokaal | Qw11  | -0.53  | -0.53 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 4      | 1:QZLokaal | Qw11  | -0.53  | -0.53 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2      | 1:QZLokaal | Qw11  | -0.53  | -0.53 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 17     | 1:QZLokaal | Qw11  | -0.53  | -0.53 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 17     | 1:QZLokaal | Qw15  | 2.10   | 2.10  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2      | 1:QZLokaal | Qw16  | 1.53   | 1.53  | 0.000 | 0.823 | 0.00     | 0.20     | 0.00     |
| 2      | 1:QZLokaal | Qw17  | 0.31   | 0.31  | 0.000 | 0.823 | 0.00     | 0.20     | 0.00     |
| 2      | 1:QZLokaal | Qw18  | 1.56   | 1.56  | 1.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 4      | 1:QZLokaal | Qw18  | 1.56   | 1.56  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 8      | 1:QZLokaal | Qw18  | 1.56   | 1.56  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7      | 1:QZLokaal | Qw19  | 0.81   | 0.81  | 0.711 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7      | 1:QZLokaal | Qw20  | 0.54   | 0.54  | 0.000 | 1.000 | 0.00     | 0.20     | 0.00     |
| 3      | 1:QZLokaal | Qw20  | 0.54   | 0.54  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1      | 1:QZLokaal | Qw20  | 0.54   | 0.54  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 14     | 1:QZLokaal | Qw21  | 1.59   | 1.59  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |

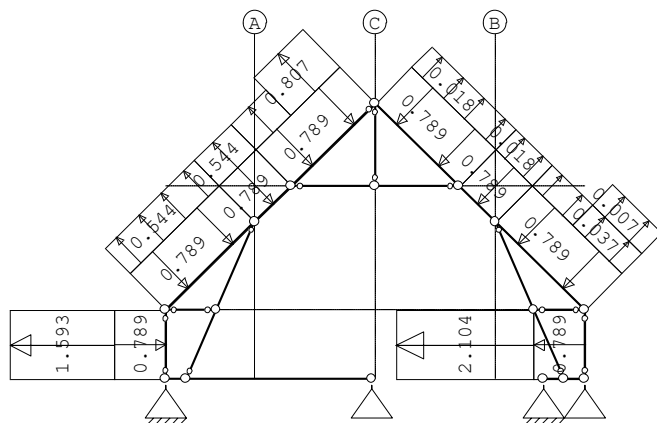
Project.....: 240772

Onderdeel....: spant

## BELASTINGEN

B.G:14 Wind van rechts

onderdruk B



## STAAFBELASTINGEN

B.G:14 Wind van rechts

onderdruk B

| Staaf | Type       | Index | q1/p/m | q2    | A     | B     | $\Psi_0$ | $\Psi_1$ | $\Psi_2$ |
|-------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 14    | 1:QZLokaal | Qw1   | -0.79  | -0.79 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw1   | -0.79  | -0.79 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3     | 1:QZLokaal | Qw1   | -0.79  | -0.79 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7     | 1:QZLokaal | Qw1   | -0.79  | -0.79 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 8     | 1:QZLokaal | Qw2   | 0.79   | 0.79  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 4     | 1:QZLokaal | Qw2   | 0.79   | 0.79  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2     | 1:QZLokaal | Qw2   | 0.79   | 0.79  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 17    | 1:QZLokaal | Qw2   | 0.79   | 0.79  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 17    | 1:QZLokaal | Qw15  | 2.10   | 2.10  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2     | 1:QZLokaal | Qw22  | -0.04  | -0.04 | 0.000 | 0.823 | 0.00     | 0.20     | 0.00     |
| 2     | 1:QZLokaal | Qw23  | -0.01  | -0.01 | 0.000 | 0.823 | 0.00     | 0.20     | 0.00     |
| 2     | 1:QZLokaal | Qw24  | -0.02  | -0.02 | 1.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 4     | 1:QZLokaal | Qw24  | -0.02  | -0.02 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 8     | 1:QZLokaal | Qw24  | -0.02  | -0.02 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7     | 1:QZLokaal | Qw19  | 0.81   | 0.81  | 0.711 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7     | 1:QZLokaal | Qw20  | 0.54   | 0.54  | 0.000 | 1.000 | 0.00     | 0.20     | 0.00     |
| 3     | 1:QZLokaal | Qw20  | 0.54   | 0.54  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw20  | 0.54   | 0.54  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 14    | 1:QZLokaal | Qw21  | 1.59   | 1.59  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |

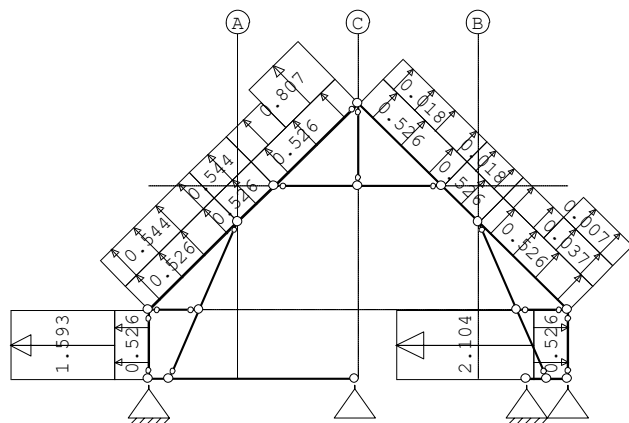
Project.....: 240772

Onderdeel....: spant

## BELASTINGEN

B.G:15 Wind van rechts

overdruk B



## STAAFBELASTINGEN

B.G:15 Wind van rechts

overdruk B

| Staaf | Type       | Index | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|-------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 14    | 1:QZLokaal | Qw10  | 0.53   | 0.53  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw10  | 0.53   | 0.53  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3     | 1:QZLokaal | Qw10  | 0.53   | 0.53  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7     | 1:QZLokaal | Qw10  | 0.53   | 0.53  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 8     | 1:QZLokaal | Qw11  | -0.53  | -0.53 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 4     | 1:QZLokaal | Qw11  | -0.53  | -0.53 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2     | 1:QZLokaal | Qw11  | -0.53  | -0.53 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 17    | 1:QZLokaal | Qw11  | -0.53  | -0.53 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 17    | 1:QZLokaal | Qw15  | 2.10   | 2.10  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2     | 1:QZLokaal | Qw22  | -0.04  | -0.04 | 0.000 | 0.823 | 0.00     | 0.20     | 0.00     |
| 2     | 1:QZLokaal | Qw23  | -0.01  | -0.01 | 0.000 | 0.823 | 0.00     | 0.20     | 0.00     |
| 2     | 1:QZLokaal | Qw24  | -0.02  | -0.02 | 1.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 4     | 1:QZLokaal | Qw24  | -0.02  | -0.02 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 8     | 1:QZLokaal | Qw24  | -0.02  | -0.02 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7     | 1:QZLokaal | Qw19  | 0.81   | 0.81  | 0.711 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7     | 1:QZLokaal | Qw20  | 0.54   | 0.54  | 0.000 | 1.000 | 0.00     | 0.20     | 0.00     |
| 3     | 1:QZLokaal | Qw20  | 0.54   | 0.54  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw20  | 0.54   | 0.54  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 14    | 1:QZLokaal | Qw21  | 1.59   | 1.59  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |

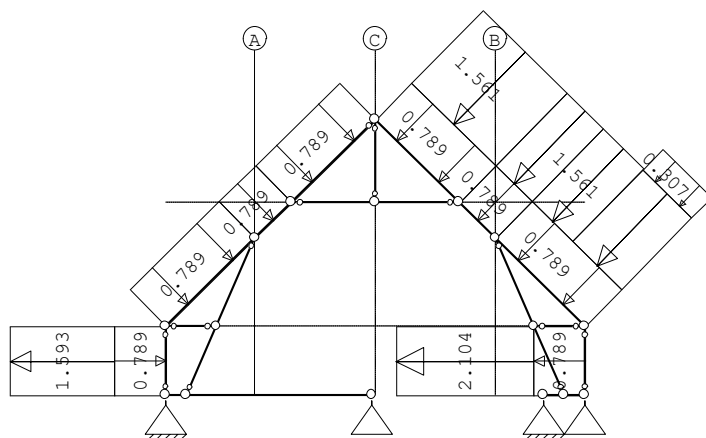
Project.....: 240772

Onderdeel.....: spant

**BELASTINGEN**

B.G:16 Wind van rechts

onderdruk C

**STAAFBELASTINGEN**

B.G:16 Wind van rechts

onderdruk C

| Staaftype | Type       | Index | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|-----------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 14        | 1:QZLokaal | Qw1   | -0.79  | -0.79 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1         | 1:QZLokaal | Qw1   | -0.79  | -0.79 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3         | 1:QZLokaal | Qw1   | -0.79  | -0.79 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7         | 1:QZLokaal | Qw1   | -0.79  | -0.79 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 8         | 1:QZLokaal | Qw2   | 0.79   | 0.79  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 4         | 1:QZLokaal | Qw2   | 0.79   | 0.79  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2         | 1:QZLokaal | Qw2   | 0.79   | 0.79  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 17        | 1:QZLokaal | Qw2   | 0.79   | 0.79  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 17        | 1:QZLokaal | Qw15  | 2.10   | 2.10  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2         | 1:QZLokaal | Qw16  | 1.53   | 1.53  | 0.000 | 0.823 | 0.00     | 0.20     | 0.00     |
| 2         | 1:QZLokaal | Qw17  | 0.31   | 0.31  | 0.000 | 0.823 | 0.00     | 0.20     | 0.00     |
| 2         | 1:QZLokaal | Qw18  | 1.56   | 1.56  | 1.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 4         | 1:QZLokaal | Qw18  | 1.56   | 1.56  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 8         | 1:QZLokaal | Qw18  | 1.56   | 1.56  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 14        | 1:QZLokaal | Qw21  | 1.59   | 1.59  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |

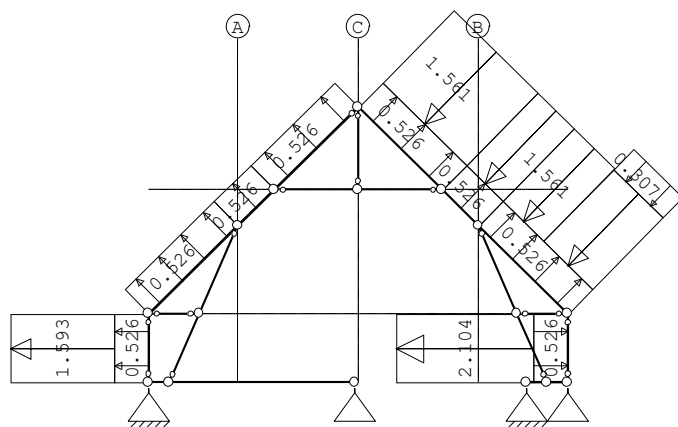
Project.....: 240772

Onderdeel.....: spant

**BELASTINGEN**

B.G:17 Wind van rechts

overdruk C

**STAAFBELASTINGEN**

B.G:17 Wind van rechts

overdruk C

| Staaft | Type       | Index | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|--------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 14     | 1:QZLokaal | Qw10  | 0.53   | 0.53  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1      | 1:QZLokaal | Qw10  | 0.53   | 0.53  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3      | 1:QZLokaal | Qw10  | 0.53   | 0.53  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7      | 1:QZLokaal | Qw10  | 0.53   | 0.53  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 8      | 1:QZLokaal | Qw11  | -0.53  | -0.53 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 4      | 1:QZLokaal | Qw11  | -0.53  | -0.53 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2      | 1:QZLokaal | Qw11  | -0.53  | -0.53 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 17     | 1:QZLokaal | Qw11  | -0.53  | -0.53 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 17     | 1:QZLokaal | Qw15  | 2.10   | 2.10  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2      | 1:QZLokaal | Qw16  | 1.53   | 1.53  | 0.000 | 0.823 | 0.00     | 0.20     | 0.00     |
| 2      | 1:QZLokaal | Qw17  | 0.31   | 0.31  | 0.000 | 0.823 | 0.00     | 0.20     | 0.00     |
| 2      | 1:QZLokaal | Qw18  | 1.56   | 1.56  | 1.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 4      | 1:QZLokaal | Qw18  | 1.56   | 1.56  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 8      | 1:QZLokaal | Qw18  | 1.56   | 1.56  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 14     | 1:QZLokaal | Qw21  | 1.59   | 1.59  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |

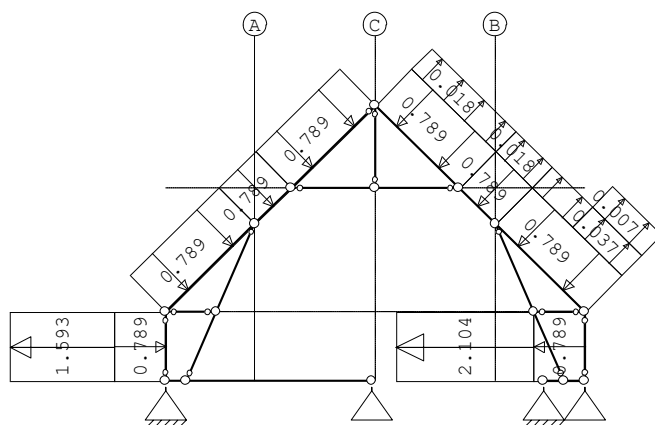
Project.....: 240772

Onderdeel.....: spant

**BELASTINGEN**

B.G:18 Wind van rechts

onderdruk D

**STAAFBELASTINGEN**

B.G:18 Wind van rechts

onderdruk D

| Staal | Type       | Index | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|-------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 14    | 1:QZLokaal | Qw1   | -0.79  | -0.79 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw1   | -0.79  | -0.79 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3     | 1:QZLokaal | Qw1   | -0.79  | -0.79 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7     | 1:QZLokaal | Qw1   | -0.79  | -0.79 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 8     | 1:QZLokaal | Qw2   | 0.79   | 0.79  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 4     | 1:QZLokaal | Qw2   | 0.79   | 0.79  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2     | 1:QZLokaal | Qw2   | 0.79   | 0.79  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 17    | 1:QZLokaal | Qw2   | 0.79   | 0.79  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 17    | 1:QZLokaal | Qw15  | 2.10   | 2.10  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2     | 1:QZLokaal | Qw22  | -0.04  | -0.04 | 0.000 | 0.823 | 0.00     | 0.20     | 0.00     |
| 2     | 1:QZLokaal | Qw23  | -0.01  | -0.01 | 0.000 | 0.823 | 0.00     | 0.20     | 0.00     |
| 2     | 1:QZLokaal | Qw24  | -0.02  | -0.02 | 1.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 4     | 1:QZLokaal | Qw24  | -0.02  | -0.02 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 8     | 1:QZLokaal | Qw24  | -0.02  | -0.02 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 14    | 1:QZLokaal | Qw21  | 1.59   | 1.59  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |

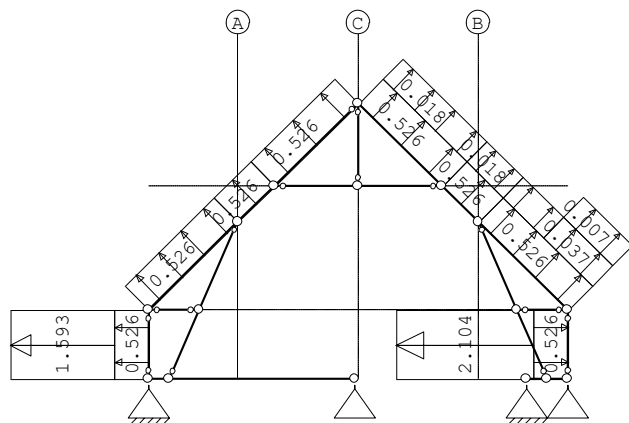
Project.....: 240772

Onderdeel....: spant

## BELASTINGEN

B.G:19 Wind van rechts

overdruk D



## STAAFBELASTINGEN

B.G:19 Wind van rechts

overdruk D

| Staal | Type       | Index | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|-------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 14    | 1:QZLokaal | Qw10  | 0.53   | 0.53  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 1     | 1:QZLokaal | Qw10  | 0.53   | 0.53  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3     | 1:QZLokaal | Qw10  | 0.53   | 0.53  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7     | 1:QZLokaal | Qw10  | 0.53   | 0.53  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 8     | 1:QZLokaal | Qw11  | -0.53  | -0.53 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 4     | 1:QZLokaal | Qw11  | -0.53  | -0.53 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2     | 1:QZLokaal | Qw11  | -0.53  | -0.53 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 17    | 1:QZLokaal | Qw11  | -0.53  | -0.53 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 17    | 1:QZLokaal | Qw15  | 2.10   | 2.10  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2     | 1:QZLokaal | Qw22  | -0.04  | -0.04 | 0.000 | 0.823 | 0.00     | 0.20     | 0.00     |
| 2     | 1:QZLokaal | Qw23  | -0.01  | -0.01 | 0.000 | 0.823 | 0.00     | 0.20     | 0.00     |
| 2     | 1:QZLokaal | Qw24  | -0.02  | -0.02 | 1.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 4     | 1:QZLokaal | Qw24  | -0.02  | -0.02 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 8     | 1:QZLokaal | Qw24  | -0.02  | -0.02 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 14    | 1:QZLokaal | Qw21  | 1.59   | 1.59  | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |

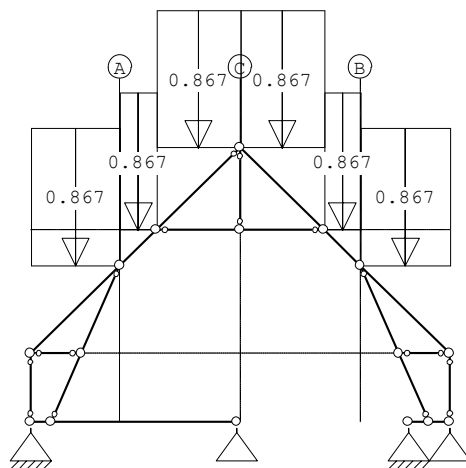
Project.....: 240772

Onderdeel.....: spant

**BELASTINGEN**

B.G:20

Sneeuw A

**STAAFBELASTINGEN**

B.G:20

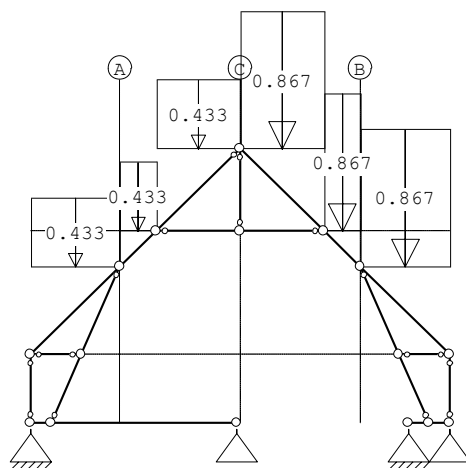
Sneeuw A

| Staat | Type        | Index | q1 / p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|-------|-------------|-------|----------|-------|-------|-------|----------|----------|----------|
| 1     | 3:QZgeProj. | Qs1   | -0.87    | -0.87 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2     | 3:QZgeProj. | Qs1   | -0.87    | -0.87 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3     | 3:QZgeProj. | Qs1   | -0.87    | -0.87 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 4     | 3:QZgeProj. | Qs1   | -0.87    | -0.87 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7     | 3:QZgeProj. | Qs1   | -0.87    | -0.87 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 8     | 3:QZgeProj. | Qs1   | -0.87    | -0.87 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |

**BELASTINGEN**

B.G:21

Sneeuw B



Project.....: 240772

Onderdeel.....: spant

**STAAFBELASTINGEN**

B.G:21

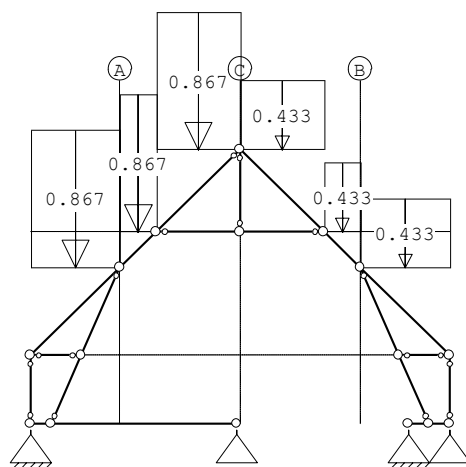
Sneeuw B

| Staat | Type        | Index | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|-------|-------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 1     | 3:QZgeProj. | Qs2   | -0.43  | -0.43 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2     | 3:QZgeProj. | Qs1   | -0.87  | -0.87 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3     | 3:QZgeProj. | Qs2   | -0.43  | -0.43 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 4     | 3:QZgeProj. | Qs1   | -0.87  | -0.87 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7     | 3:QZgeProj. | Qs2   | -0.43  | -0.43 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 8     | 3:QZgeProj. | Qs1   | -0.87  | -0.87 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |

**BELASTINGEN**

B.G:22

Sneeuw C

**STAAFBELASTINGEN**

B.G:22

Sneeuw C

| Staat | Type        | Index | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|-------|-------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 1     | 3:QZgeProj. | Qs1   | -0.87  | -0.87 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 2     | 3:QZgeProj. | Qs2   | -0.43  | -0.43 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 3     | 3:QZgeProj. | Qs1   | -0.87  | -0.87 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 4     | 3:QZgeProj. | Qs2   | -0.43  | -0.43 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 7     | 3:QZgeProj. | Qs1   | -0.87  | -0.87 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |
| 8     | 3:QZgeProj. | Qs2   | -0.43  | -0.43 | 0.000 | 0.000 | 0.00     | 0.20     | 0.00     |

**BEREKENINGSTATUS**

| B.C. | Iteratie | Status                 |
|------|----------|------------------------|
| 1    | 3        | Nauwkeurigheid bereikt |
| 2    | 3        | Nauwkeurigheid bereikt |
| 3    | 3        | Nauwkeurigheid bereikt |
| 4    | 3        | Nauwkeurigheid bereikt |
| 5    | 3        | Nauwkeurigheid bereikt |
| 6    | 3        | Nauwkeurigheid bereikt |
| 7    | 3        | Nauwkeurigheid bereikt |
| 8    | 3        | Nauwkeurigheid bereikt |
| 9    | 3        | Nauwkeurigheid bereikt |
| 10   | 3        | Nauwkeurigheid bereikt |
| 11   | 3        | Nauwkeurigheid bereikt |
| 12   | 3        | Nauwkeurigheid bereikt |
| 13   | 3        | Nauwkeurigheid bereikt |
| 14   | 3        | Nauwkeurigheid bereikt |
| 15   | 3        | Nauwkeurigheid bereikt |
| 16   | 3        | Nauwkeurigheid bereikt |

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



Project.....: 240772

Onderdeel....: spant

**BEREKENINGSTATUS**

| B.C. | Iteratie | Status                 |
|------|----------|------------------------|
| 17   | 3        | Nauwkeurigheid bereikt |
| 18   | 3        | Nauwkeurigheid bereikt |
| 19   | 3        | Nauwkeurigheid bereikt |
| 20   | 3        | Nauwkeurigheid bereikt |
| 21   | 3        | Nauwkeurigheid bereikt |
| 22   | 3        | Nauwkeurigheid bereikt |
| 23   | 3        | Nauwkeurigheid bereikt |
| 24   | 3        | Nauwkeurigheid bereikt |
| 25   | 3        | Nauwkeurigheid bereikt |
| 26   | 3        | Nauwkeurigheid bereikt |
| 27   | 3        | Nauwkeurigheid bereikt |
| 28   | 3        | Nauwkeurigheid bereikt |
| 29   | 3        | Nauwkeurigheid bereikt |
| 30   | 3        | Nauwkeurigheid bereikt |
| 31   | 3        | Nauwkeurigheid bereikt |
| 32   | 3        | Nauwkeurigheid bereikt |
| 33   | 3        | Nauwkeurigheid bereikt |
| 34   | 3        | Nauwkeurigheid bereikt |
| 35   | 3        | Nauwkeurigheid bereikt |
| 36   | 3        | Nauwkeurigheid bereikt |
| 37   | 3        | Nauwkeurigheid bereikt |
| 38   | 3        | Nauwkeurigheid bereikt |
| 39   | 3        | Nauwkeurigheid bereikt |
| 40   | 3        | Nauwkeurigheid bereikt |
| 41   | 3        | Nauwkeurigheid bereikt |
| 42   | 3        | Nauwkeurigheid bereikt |
| 43   | 3        | Nauwkeurigheid bereikt |
| 44   | 3        | Nauwkeurigheid bereikt |
| 45   | 3        | Nauwkeurigheid bereikt |
| 46   | 3        | Nauwkeurigheid bereikt |
| 47   | 3        | Nauwkeurigheid bereikt |
| 48   | 3        | Nauwkeurigheid bereikt |
| 49   | 3        | Nauwkeurigheid bereikt |
| 50   | 3        | Nauwkeurigheid bereikt |
| 51   | 3        | Nauwkeurigheid bereikt |
| 52   | 3        | Nauwkeurigheid bereikt |
| 53   | 3        | Nauwkeurigheid bereikt |
| 54   | 3        | Nauwkeurigheid bereikt |
| 55   | 3        | Nauwkeurigheid bereikt |
| 56   | 3        | Nauwkeurigheid bereikt |
| 57   | 3        | Nauwkeurigheid bereikt |
| 58   | 3        | Nauwkeurigheid bereikt |
| 59   | 3        | Nauwkeurigheid bereikt |
| 60   | 3        | Nauwkeurigheid bereikt |
| 61   | 3        | Nauwkeurigheid bereikt |
| 62   | 3        | Nauwkeurigheid bereikt |
| 63   | 3        | Nauwkeurigheid bereikt |
| 64   | 3        | Nauwkeurigheid bereikt |
| 65   | 3        | Nauwkeurigheid bereikt |
| 66   | 3        | Nauwkeurigheid bereikt |
| 67   | 3        | Nauwkeurigheid bereikt |
| 68   | 3        | Nauwkeurigheid bereikt |
| 69   | 3        | Nauwkeurigheid bereikt |
| 70   | 3        | Nauwkeurigheid bereikt |
| 71   | 3        | Nauwkeurigheid bereikt |
| 72   | 3        | Nauwkeurigheid bereikt |
| 73   | 3        | Nauwkeurigheid bereikt |
| 74   | 3        | Nauwkeurigheid bereikt |
| 75   | 3        | Nauwkeurigheid bereikt |
| 76   | 3        | Nauwkeurigheid bereikt |

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



Project.....: 240772

Onderdeel.....: spant

#### BEREKENINGSTATUS

| B.C. | Iteratie | Status                 |
|------|----------|------------------------|
| 77   | 3        | Nauwkeurigheid bereikt |
| 78   | 3        | Nauwkeurigheid bereikt |
| 79   | 3        | Nauwkeurigheid bereikt |
| 80   | 3        | Nauwkeurigheid bereikt |
| 81   | 3        | Nauwkeurigheid bereikt |
| 82   | 3        | Nauwkeurigheid bereikt |
| 83   | 3        | Nauwkeurigheid bereikt |
| 84   | 3        | Nauwkeurigheid bereikt |
| 85   | 3        | Nauwkeurigheid bereikt |
| 86   | 3        | Nauwkeurigheid bereikt |
| 87   | 3        | Nauwkeurigheid bereikt |
| 88   | 3        | Nauwkeurigheid bereikt |
| 89   | 3        | Nauwkeurigheid bereikt |
| 90   | 3        | Nauwkeurigheid bereikt |
| 91   | 3        | Nauwkeurigheid bereikt |
| 92   | 3        | Nauwkeurigheid bereikt |
| 93   | 3        | Nauwkeurigheid bereikt |
| 94   | 3        | Nauwkeurigheid bereikt |
| 95   | 3        | Nauwkeurigheid bereikt |
| 96   | 3        | Nauwkeurigheid bereikt |
| 97   | 3        | Nauwkeurigheid bereikt |
| 98   | 3        | Nauwkeurigheid bereikt |
| 99   | 3        | Nauwkeurigheid bereikt |
| 100  | 3        | Nauwkeurigheid bereikt |
| 101  | 3        | Nauwkeurigheid bereikt |
| 102  | 3        | Nauwkeurigheid bereikt |
| 103  | 3        | Nauwkeurigheid bereikt |
| 104  | 3        | Nauwkeurigheid bereikt |
| 105  | 3        | Nauwkeurigheid bereikt |
| 106  | 3        | Nauwkeurigheid bereikt |
| 107  | 3        | Nauwkeurigheid bereikt |
| 108  | 3        | Nauwkeurigheid bereikt |
| 109  | 3        | Nauwkeurigheid bereikt |
| 110  | 3        | Nauwkeurigheid bereikt |
| 111  | 3        | Nauwkeurigheid bereikt |
| 112  | 3        | Nauwkeurigheid bereikt |
| 113  | 3        | Nauwkeurigheid bereikt |
| 114  | 3        | Nauwkeurigheid bereikt |
| 115  | 3        | Nauwkeurigheid bereikt |
| 116  | 3        | Nauwkeurigheid bereikt |
| 117  | 3        | Nauwkeurigheid bereikt |
| 118  | 3        | Nauwkeurigheid bereikt |
| 119  | 3        | Nauwkeurigheid bereikt |
| 120  | 3        | Nauwkeurigheid bereikt |
| 121  | 3        | Nauwkeurigheid bereikt |
| 122  | 3        | Nauwkeurigheid bereikt |
| 123  | 3        | Nauwkeurigheid bereikt |
| 124  | 3        | Nauwkeurigheid bereikt |
| 125  | 1        | Lineaire berekening    |
| 126  | 1        | Lineaire berekening    |
| 127  | 1        | Lineaire berekening    |
| 128  | 1        | Lineaire berekening    |
| 129  | 1        | Lineaire berekening    |
| 130  | 1        | Lineaire berekening    |
| 131  | 1        | Lineaire berekening    |
| 132  | 1        | Lineaire berekening    |
| 133  | 1        | Lineaire berekening    |
| 134  | 1        | Lineaire berekening    |
| 135  | 1        | Lineaire berekening    |
| 136  | 1        | Lineaire berekening    |

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



Project.....: 240772

Onderdeel.....: spant

**BEREKENINGSTATUS**

| B.C. | Iteratie | Status              |
|------|----------|---------------------|
| 137  | 1        | Lineaire berekening |
| 138  | 1        | Lineaire berekening |
| 139  | 1        | Lineaire berekening |
| 140  | 1        | Lineaire berekening |
| 141  | 1        | Lineaire berekening |
| 142  | 1        | Lineaire berekening |
| 143  | 1        | Lineaire berekening |
| 144  | 1        | Lineaire berekening |
| 145  | 1        | Lineaire berekening |
| 146  | 1        | Lineaire berekening |
| 147  | 1        | Lineaire berekening |
| 148  | 1        | Lineaire berekening |
| 149  | 1        | Lineaire berekening |
| 150  | 1        | Lineaire berekening |
| 151  | 1        | Lineaire berekening |
| 152  | 1        | Lineaire berekening |
| 153  | 1        | Lineaire berekening |
| 154  | 1        | Lineaire berekening |
| 155  | 1        | Lineaire berekening |
| 156  | 1        | Lineaire berekening |
| 157  | 1        | Lineaire berekening |
| 158  | 1        | Lineaire berekening |
| 159  | 1        | Lineaire berekening |
| 160  | 1        | Lineaire berekening |
| 161  | 1        | Lineaire berekening |
| 162  | 1        | Lineaire berekening |
| 163  | 1        | Lineaire berekening |
| 164  | 1        | Lineaire berekening |
| 165  | 1        | Lineaire berekening |
| 166  | 1        | Lineaire berekening |
| 167  | 1        | Lineaire berekening |
| 168  | 1        | Lineaire berekening |
| 169  | 1        | Lineaire berekening |
| 170  | 1        | Lineaire berekening |
| 171  | 1        | Lineaire berekening |
| 172  | 1        | Lineaire berekening |
| 173  | 1        | Lineaire berekening |
| 174  | 1        | Lineaire berekening |
| 175  | 1        | Lineaire berekening |
| 176  | 1        | Lineaire berekening |
| 177  | 1        | Lineaire berekening |
| 178  | 1        | Lineaire berekening |
| 179  | 1        | Lineaire berekening |
| 180  | 1        | Lineaire berekening |
| 181  | 1        | Lineaire berekening |
| 182  | 1        | Lineaire berekening |
| 183  | 1        | Lineaire berekening |
| 184  | 1        | Lineaire berekening |
| 185  | 1        | Lineaire berekening |
| 186  | 1        | Lineaire berekening |
| 187  | 1        | Lineaire berekening |
| 188  | 1        | Lineaire berekening |
| 189  | 1        | Lineaire berekening |
| 190  | 1        | Lineaire berekening |
| 191  | 1        | Lineaire berekening |
| 192  | 1        | Lineaire berekening |
| 193  | 1        | Lineaire berekening |
| 194  | 1        | Lineaire berekening |
| 195  | 1        | Lineaire berekening |
| 196  | 1        | Lineaire berekening |

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



Project.....: 240772

Onderdeel....: spant

#### BEREKENINGSTATUS

| B.C. | Iteratie | Status              |
|------|----------|---------------------|
| 197  | 1        | Lineaire berekening |
| 198  | 1        | Lineaire berekening |
| 199  | 1        | Lineaire berekening |
| 200  | 1        | Lineaire berekening |
| 201  | 1        | Lineaire berekening |
| 202  | 1        | Lineaire berekening |
| 203  | 1        | Lineaire berekening |
| 204  | 1        | Lineaire berekening |
| 205  | 1        | Lineaire berekening |
| 206  | 1        | Lineaire berekening |
| 207  | 1        | Lineaire berekening |
| 208  | 1        | Lineaire berekening |
| 209  | 1        | Lineaire berekening |
| 210  | 1        | Lineaire berekening |
| 211  | 1        | Lineaire berekening |
| 212  | 1        | Lineaire berekening |
| 213  | 1        | Lineaire berekening |
| 214  | 1        | Lineaire berekening |
| 215  | 1        | Lineaire berekening |
| 216  | 1        | Lineaire berekening |
| 217  | 1        | Lineaire berekening |
| 218  | 1        | Lineaire berekening |
| 219  | 1        | Lineaire berekening |
| 220  | 1        | Lineaire berekening |
| 221  | 1        | Lineaire berekening |
| 222  | 1        | Lineaire berekening |
| 223  | 1        | Lineaire berekening |
| 224  | 1        | Lineaire berekening |
| 225  | 1        | Lineaire berekening |
| 226  | 1        | Lineaire berekening |
| 227  | 1        | Lineaire berekening |
| 228  | 1        | Lineaire berekening |
| 229  | 1        | Lineaire berekening |
| 230  | 1        | Lineaire berekening |
| 231  | 1        | Lineaire berekening |
| 232  | 1        | Lineaire berekening |
| 233  | 1        | Lineaire berekening |
| 234  | 1        | Lineaire berekening |
| 235  | 1        | Lineaire berekening |
| 236  | 1        | Lineaire berekening |
| 237  | 1        | Lineaire berekening |
| 238  | 1        | Lineaire berekening |
| 239  | 1        | Lineaire berekening |
| 240  | 1        | Lineaire berekening |
| 241  | 1        | Lineaire berekening |
| 242  | 1        | Lineaire berekening |
| 243  | 1        | Lineaire berekening |
| 244  | 1        | Lineaire berekening |
| 245  | 1        | Lineaire berekening |
| 246  | 1        | Lineaire berekening |
| 247  | 1        | Lineaire berekening |

#### BELASTINGCOMBINATIES

| BC      | Type                                   |
|---------|----------------------------------------|
| 1 Fund. | 1.35 $G_{k,1}$                         |
| 2 Fund. | 0.90 $G_{k,1}$                         |
| 3 Fund. | 1.35 $G_{k,1}$ + 1.50 $\psi_0 Q_{k,2}$ |
| 4 Fund. | 1.35 $G_{k,1}$ + 1.50 $\psi_0 Q_{k,3}$ |
| 5 Fund. | 1.20 $G_{k,1}$ + 1.50 $Q_{k,2}$        |
| 6 Fund. | 1.20 $G_{k,1}$ + 1.50 $Q_{k,3}$        |
| 7 Fund. | 1.20 $G_{k,1}$ + 1.50 $Q_{k,4}$        |
| 8 Fund. | 1.20 $G_{k,1}$ + 1.50 $Q_{k,5}$        |

Project.....: 240772

Onderdeel.....: spant

**BELASTINGCOMBINATIES**

| BC | Type  |      |           |   |      |                  |   |      |                  |
|----|-------|------|-----------|---|------|------------------|---|------|------------------|
| 9  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,6}$        |   |      |                  |
| 10 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,7}$        |   |      |                  |
| 11 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,8}$        |   |      |                  |
| 12 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,9}$        |   |      |                  |
| 13 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,10}$       |   |      |                  |
| 14 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,11}$       |   |      |                  |
| 15 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,12}$       |   |      |                  |
| 16 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,13}$       |   |      |                  |
| 17 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,14}$       |   |      |                  |
| 18 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,15}$       |   |      |                  |
| 19 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,16}$       |   |      |                  |
| 20 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,17}$       |   |      |                  |
| 21 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,18}$       |   |      |                  |
| 22 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,19}$       |   |      |                  |
| 23 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,20}$       |   |      |                  |
| 24 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,21}$       |   |      |                  |
| 25 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,22}$       |   |      |                  |
| 26 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,2}$        |   |      |                  |
| 27 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $\psi_0 Q_{k,2}$ |   |      |                  |
| 28 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $\psi_0 Q_{k,3}$ |   |      |                  |
| 29 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,3}$        |   |      |                  |
| 30 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,4}$        |   |      |                  |
| 31 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,5}$        |   |      |                  |
| 32 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,6}$        |   |      |                  |
| 33 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,7}$        |   |      |                  |
| 34 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,8}$        |   |      |                  |
| 35 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,9}$        |   |      |                  |
| 36 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,10}$       |   |      |                  |
| 37 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,11}$       |   |      |                  |
| 38 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,12}$       |   |      |                  |
| 39 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,13}$       |   |      |                  |
| 40 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,14}$       |   |      |                  |
| 41 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,15}$       |   |      |                  |
| 42 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,16}$       |   |      |                  |
| 43 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,17}$       |   |      |                  |
| 44 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,18}$       |   |      |                  |
| 45 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,19}$       |   |      |                  |
| 46 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,20}$       |   |      |                  |
| 47 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,21}$       |   |      |                  |
| 48 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,22}$       |   |      |                  |
| 49 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,4}$        | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 50 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,4}$        | + | 1.50 | $\psi_0 Q_{k,3}$ |
| 51 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,5}$        | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 52 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,5}$        | + | 1.50 | $\psi_0 Q_{k,3}$ |
| 53 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,6}$        | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 54 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,6}$        | + | 1.50 | $\psi_0 Q_{k,3}$ |
| 55 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,7}$        | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 56 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,7}$        | + | 1.50 | $\psi_0 Q_{k,3}$ |
| 57 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,8}$        | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 58 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,8}$        | + | 1.50 | $\psi_0 Q_{k,3}$ |
| 59 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,9}$        | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 60 | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,9}$        | + | 1.50 | $\psi_0 Q_{k,3}$ |

Project.....: 240772

Onderdeel....: spant

**BELASTINGCOMBINATIES**

| BC  | Type  |      |           |   |      |            |   |      |                  |
|-----|-------|------|-----------|---|------|------------|---|------|------------------|
| 61  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,10}$ | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 62  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,10}$ | + | 1.50 | $\psi_0 Q_{k,3}$ |
| 63  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,11}$ | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 64  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,11}$ | + | 1.50 | $\psi_0 Q_{k,3}$ |
| 65  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,12}$ | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 66  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,12}$ | + | 1.50 | $\psi_0 Q_{k,3}$ |
| 67  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,13}$ | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 68  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,13}$ | + | 1.50 | $\psi_0 Q_{k,3}$ |
| 69  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,14}$ | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 70  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,14}$ | + | 1.50 | $\psi_0 Q_{k,3}$ |
| 71  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,15}$ | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 72  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,15}$ | + | 1.50 | $\psi_0 Q_{k,3}$ |
| 73  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,16}$ | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 74  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,16}$ | + | 1.50 | $\psi_0 Q_{k,3}$ |
| 75  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,17}$ | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 76  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,17}$ | + | 1.50 | $\psi_0 Q_{k,3}$ |
| 77  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,18}$ | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 78  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,18}$ | + | 1.50 | $\psi_0 Q_{k,3}$ |
| 79  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,19}$ | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 80  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,19}$ | + | 1.50 | $\psi_0 Q_{k,3}$ |
| 81  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,20}$ | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 82  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,20}$ | + | 1.50 | $\psi_0 Q_{k,3}$ |
| 83  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,21}$ | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 84  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,21}$ | + | 1.50 | $\psi_0 Q_{k,3}$ |
| 85  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,22}$ | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 86  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 | $Q_{k,22}$ | + | 1.50 | $\psi_0 Q_{k,3}$ |
| 87  | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,4}$  | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 88  | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,4}$  | + | 1.50 | $\psi_0 Q_{k,3}$ |
| 89  | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,5}$  | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 90  | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,5}$  | + | 1.50 | $\psi_0 Q_{k,3}$ |
| 91  | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,6}$  | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 92  | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,6}$  | + | 1.50 | $\psi_0 Q_{k,3}$ |
| 93  | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,7}$  | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 94  | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,7}$  | + | 1.50 | $\psi_0 Q_{k,3}$ |
| 95  | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,8}$  | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 96  | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,8}$  | + | 1.50 | $\psi_0 Q_{k,3}$ |
| 97  | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,9}$  | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 98  | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,9}$  | + | 1.50 | $\psi_0 Q_{k,3}$ |
| 99  | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,10}$ | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 100 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,10}$ | + | 1.50 | $\psi_0 Q_{k,3}$ |
| 101 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,11}$ | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 102 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,11}$ | + | 1.50 | $\psi_0 Q_{k,3}$ |
| 103 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,12}$ | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 104 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,12}$ | + | 1.50 | $\psi_0 Q_{k,3}$ |
| 105 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,13}$ | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 106 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,13}$ | + | 1.50 | $\psi_0 Q_{k,3}$ |
| 107 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,14}$ | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 108 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,14}$ | + | 1.50 | $\psi_0 Q_{k,3}$ |
| 109 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,15}$ | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 110 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,15}$ | + | 1.50 | $\psi_0 Q_{k,3}$ |

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



|     |       |      |           |   |      |            |   |      |          |           |
|-----|-------|------|-----------|---|------|------------|---|------|----------|-----------|
| 111 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,16}$ | + | 1.50 | $\psi_0$ | $Q_{k,2}$ |
| 112 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,16}$ | + | 1.50 | $\psi_0$ | $Q_{k,3}$ |
| 113 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,17}$ | + | 1.50 | $\psi_0$ | $Q_{k,2}$ |

Project.....: 240772

Onderdeel....: spant

**BELASTINGCOMBINATIES**

| BC  | Type  |      |           |   |      |            |   |      |                  |
|-----|-------|------|-----------|---|------|------------|---|------|------------------|
| 114 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,17}$ | + | 1.50 | $\psi_0 Q_{k,3}$ |
| 115 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,18}$ | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 116 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,18}$ | + | 1.50 | $\psi_0 Q_{k,3}$ |
| 117 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,19}$ | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 118 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,19}$ | + | 1.50 | $\psi_0 Q_{k,3}$ |
| 119 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,20}$ | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 120 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,20}$ | + | 1.50 | $\psi_0 Q_{k,3}$ |
| 121 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,21}$ | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 122 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,21}$ | + | 1.50 | $\psi_0 Q_{k,3}$ |
| 123 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,22}$ | + | 1.50 | $\psi_0 Q_{k,2}$ |
| 124 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 | $Q_{k,22}$ | + | 1.50 | $\psi_0 Q_{k,3}$ |
| 125 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,2}$  |   |      |                  |
| 126 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,3}$  |   |      |                  |
| 127 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,4}$  |   |      |                  |
| 128 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,5}$  |   |      |                  |
| 129 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,6}$  |   |      |                  |
| 130 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,7}$  |   |      |                  |
| 131 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,8}$  |   |      |                  |
| 132 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,9}$  |   |      |                  |
| 133 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,10}$ |   |      |                  |
| 134 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,11}$ |   |      |                  |
| 135 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,12}$ |   |      |                  |
| 136 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,13}$ |   |      |                  |
| 137 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,14}$ |   |      |                  |
| 138 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,15}$ |   |      |                  |
| 139 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,16}$ |   |      |                  |
| 140 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,17}$ |   |      |                  |
| 141 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,18}$ |   |      |                  |
| 142 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,19}$ |   |      |                  |
| 143 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,20}$ |   |      |                  |
| 144 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,21}$ |   |      |                  |
| 145 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,22}$ |   |      |                  |
| 146 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,4}$  | + | 1.00 | $\psi_0 Q_{k,2}$ |
| 147 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,4}$  | + | 1.00 | $\psi_0 Q_{k,3}$ |
| 148 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,5}$  | + | 1.00 | $\psi_0 Q_{k,2}$ |
| 149 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,5}$  | + | 1.00 | $\psi_0 Q_{k,3}$ |
| 150 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,6}$  | + | 1.00 | $\psi_0 Q_{k,2}$ |
| 151 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,6}$  | + | 1.00 | $\psi_0 Q_{k,3}$ |
| 152 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,7}$  | + | 1.00 | $\psi_0 Q_{k,2}$ |
| 153 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,7}$  | + | 1.00 | $\psi_0 Q_{k,3}$ |
| 154 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,8}$  | + | 1.00 | $\psi_0 Q_{k,2}$ |
| 155 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,8}$  | + | 1.00 | $\psi_0 Q_{k,3}$ |
| 156 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,9}$  | + | 1.00 | $\psi_0 Q_{k,2}$ |
| 157 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,9}$  | + | 1.00 | $\psi_0 Q_{k,3}$ |
| 158 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,10}$ | + | 1.00 | $\psi_0 Q_{k,2}$ |
| 159 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,10}$ | + | 1.00 | $\psi_0 Q_{k,3}$ |
| 160 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,11}$ | + | 1.00 | $\psi_0 Q_{k,2}$ |
| 161 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,11}$ | + | 1.00 | $\psi_0 Q_{k,3}$ |
| 162 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,12}$ | + | 1.00 | $\psi_0 Q_{k,2}$ |
| 163 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,12}$ | + | 1.00 | $\psi_0 Q_{k,3}$ |
| 164 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,13}$ | + | 1.00 | $\psi_0 Q_{k,2}$ |
| 165 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,13}$ | + | 1.00 | $\psi_0 Q_{k,3}$ |

Project.....: 240772

Onderdeel....: spant

**BELASTINGCOMBINATIES**

| BC  | Type  |      |           |   |      |                   |   |      |                  |
|-----|-------|------|-----------|---|------|-------------------|---|------|------------------|
| 166 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,14}$        | + | 1.00 | $\psi_0 Q_{k,2}$ |
| 167 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,14}$        | + | 1.00 | $\psi_0 Q_{k,3}$ |
| 168 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,15}$        | + | 1.00 | $\psi_0 Q_{k,2}$ |
| 169 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,15}$        | + | 1.00 | $\psi_0 Q_{k,3}$ |
| 170 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,16}$        | + | 1.00 | $\psi_0 Q_{k,2}$ |
| 171 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,16}$        | + | 1.00 | $\psi_0 Q_{k,3}$ |
| 172 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,17}$        | + | 1.00 | $\psi_0 Q_{k,2}$ |
| 173 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,17}$        | + | 1.00 | $\psi_0 Q_{k,3}$ |
| 174 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,18}$        | + | 1.00 | $\psi_0 Q_{k,2}$ |
| 175 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,18}$        | + | 1.00 | $\psi_0 Q_{k,3}$ |
| 176 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,19}$        | + | 1.00 | $\psi_0 Q_{k,2}$ |
| 177 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,19}$        | + | 1.00 | $\psi_0 Q_{k,3}$ |
| 178 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,20}$        | + | 1.00 | $\psi_0 Q_{k,2}$ |
| 179 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,20}$        | + | 1.00 | $\psi_0 Q_{k,3}$ |
| 180 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,21}$        | + | 1.00 | $\psi_0 Q_{k,2}$ |
| 181 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,21}$        | + | 1.00 | $\psi_0 Q_{k,3}$ |
| 182 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,22}$        | + | 1.00 | $\psi_0 Q_{k,2}$ |
| 183 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 | $Q_{k,22}$        | + | 1.00 | $\psi_0 Q_{k,3}$ |
| 184 | Quas. | 1.00 | $G_{k,1}$ |   |      |                   |   |      |                  |
| 185 | Quas. | 1.00 | $G_{k,1}$ | + | 1.00 | $\psi_2 Q_{k,2}$  |   |      |                  |
| 186 | Quas. | 1.00 | $G_{k,1}$ | + | 1.00 | $\psi_2 Q_{k,3}$  |   |      |                  |
| 187 | Freq. | 1.00 | $G_{k,1}$ |   |      |                   |   |      |                  |
| 188 | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 | $\psi_1 Q_{k,2}$  |   |      |                  |
| 189 | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 | $\psi_1 Q_{k,3}$  |   |      |                  |
| 190 | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 | $\psi_1 Q_{k,4}$  |   |      |                  |
| 191 | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 | $\psi_1 Q_{k,5}$  |   |      |                  |
| 192 | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 | $\psi_1 Q_{k,6}$  |   |      |                  |
| 193 | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 | $\psi_1 Q_{k,7}$  |   |      |                  |
| 194 | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 | $\psi_1 Q_{k,8}$  |   |      |                  |
| 195 | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 | $\psi_1 Q_{k,9}$  |   |      |                  |
| 196 | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 | $\psi_1 Q_{k,10}$ |   |      |                  |
| 197 | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 | $\psi_1 Q_{k,11}$ |   |      |                  |
| 198 | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 | $\psi_1 Q_{k,12}$ |   |      |                  |
| 199 | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 | $\psi_1 Q_{k,13}$ |   |      |                  |
| 200 | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 | $\psi_1 Q_{k,14}$ |   |      |                  |
| 201 | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 | $\psi_1 Q_{k,15}$ |   |      |                  |
| 202 | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 | $\psi_1 Q_{k,16}$ |   |      |                  |
| 203 | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 | $\psi_1 Q_{k,17}$ |   |      |                  |
| 204 | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 | $\psi_1 Q_{k,18}$ |   |      |                  |
| 205 | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 | $\psi_1 Q_{k,19}$ |   |      |                  |
| 206 | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 | $\psi_1 Q_{k,20}$ |   |      |                  |
| 207 | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 | $\psi_1 Q_{k,21}$ |   |      |                  |
| 208 | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 | $\psi_1 Q_{k,22}$ |   |      |                  |
| 209 | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 | $\psi_1 Q_{k,4}$  | + | 1.00 | $\psi_2 Q_{k,2}$ |
| 210 | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 | $\psi_1 Q_{k,4}$  | + | 1.00 | $\psi_2 Q_{k,3}$ |
| 211 | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 | $\psi_1 Q_{k,5}$  | + | 1.00 | $\psi_2 Q_{k,2}$ |
| 212 | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 | $\psi_1 Q_{k,5}$  | + | 1.00 | $\psi_2 Q_{k,3}$ |
| 213 | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 | $\psi_1 Q_{k,6}$  | + | 1.00 | $\psi_2 Q_{k,2}$ |
| 214 | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 | $\psi_1 Q_{k,6}$  | + | 1.00 | $\psi_2 Q_{k,3}$ |
| 215 | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 | $\psi_1 Q_{k,7}$  | + | 1.00 | $\psi_2 Q_{k,2}$ |

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



|           |      |           |   |      |          |           |   |      |          |           |
|-----------|------|-----------|---|------|----------|-----------|---|------|----------|-----------|
| 216 Freq. | 1.00 | $G_{k,1}$ | + | 1.00 | $\psi_1$ | $Q_{k,7}$ | + | 1.00 | $\psi_2$ | $Q_{k,3}$ |
| 217 Freq. | 1.00 | $G_{k,1}$ | + | 1.00 | $\psi_1$ | $Q_{k,8}$ | + | 1.00 | $\psi_2$ | $Q_{k,2}$ |
| 218 Freq. | 1.00 | $G_{k,1}$ | + | 1.00 | $\psi_1$ | $Q_{k,8}$ | + | 1.00 | $\psi_2$ | $Q_{k,3}$ |



Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



Project.....: 240772  
Onderdeel.....: spant

#### **GUNSTIGE WERKING PERMANENTE BELASTINGEN**

BC Staven met gunstige werking

24 Geen  
25 Geen  
26 Alle staven de factor:0.90  
27 Alle staven de factor:0.90  
28 Alle staven de factor:0.90  
29 Alle staven de factor:0.90  
30 Alle staven de factor:0.90  
31 Alle staven de factor:0.90  
32 Alle staven de factor:0.90  
33 Alle staven de factor:0.90  
34 Alle staven de factor:0.90  
35 Alle staven de factor:0.90  
36 Alle staven de factor:0.90  
37 Alle staven de factor:0.90  
38 Alle staven de factor:0.90  
39 Alle staven de factor:0.90  
40 Alle staven de factor:0.90  
41 Alle staven de factor:0.90  
42 Alle staven de factor:0.90  
43 Alle staven de factor:0.90  
44 Alle staven de factor:0.90  
45 Alle staven de factor:0.90  
46 Alle staven de factor:0.90  
47 Alle staven de factor:0.90  
48 Alle staven de factor:0.90  
49 Geen  
50 Geen  
51 Geen  
52 Geen  
53 Geen  
54 Geen  
55 Geen  
56 Geen  
57 Geen  
58 Geen  
59 Geen  
60 Geen  
61 Geen  
62 Geen  
63 Geen  
64 Geen  
65 Geen  
66 Geen  
67 Geen  
68 Geen  
69 Geen  
70 Geen  
71 Geen  
72 Geen  
73 Geen  
74 Geen  
75 Geen  
76 Geen  
77 Geen  
78 Geen  
79 Geen  
80 Geen  
81 Geen  
82 Geen  
83 Geen  
84 Geen  
85 Geen

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



Project.....: 240772  
Onderdeel.....: spant

#### **GUNSTIGE WERKING PERMANENTE BELASTINGEN**

BC Staven met gunstige werking

86 Geen  
87 Alle staven de factor:0.90  
88 Alle staven de factor:0.90  
89 Alle staven de factor:0.90  
90 Alle staven de factor:0.90  
91 Alle staven de factor:0.90  
92 Alle staven de factor:0.90  
93 Alle staven de factor:0.90  
94 Alle staven de factor:0.90  
95 Alle staven de factor:0.90  
96 Alle staven de factor:0.90  
97 Alle staven de factor:0.90  
98 Alle staven de factor:0.90  
99 Alle staven de factor:0.90  
100 Alle staven de factor:0.90  
101 Alle staven de factor:0.90  
102 Alle staven de factor:0.90  
103 Alle staven de factor:0.90  
104 Alle staven de factor:0.90  
105 Alle staven de factor:0.90  
106 Alle staven de factor:0.90  
107 Alle staven de factor:0.90  
108 Alle staven de factor:0.90  
109 Alle staven de factor:0.90  
110 Alle staven de factor:0.90  
111 Alle staven de factor:0.90  
112 Alle staven de factor:0.90  
113 Alle staven de factor:0.90  
114 Alle staven de factor:0.90  
115 Alle staven de factor:0.90  
116 Alle staven de factor:0.90  
117 Alle staven de factor:0.90  
118 Alle staven de factor:0.90  
119 Alle staven de factor:0.90  
120 Alle staven de factor:0.90  
121 Alle staven de factor:0.90  
122 Alle staven de factor:0.90  
123 Alle staven de factor:0.90  
124 Alle staven de factor:0.90

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



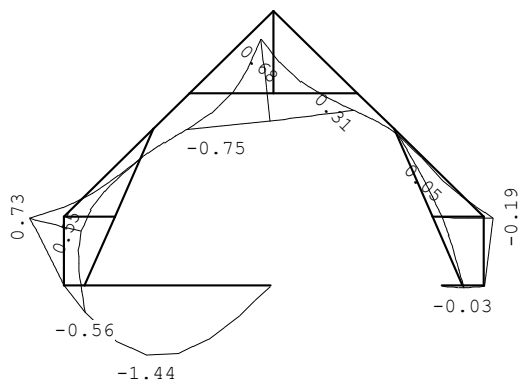
Project.....: 240772  
Onderdeel.....: spant

### BELASTINGCOMBINATIE Blijvend

B.C:247

VERPLAATSINGEN 1e orde [mm]  
Blijvend

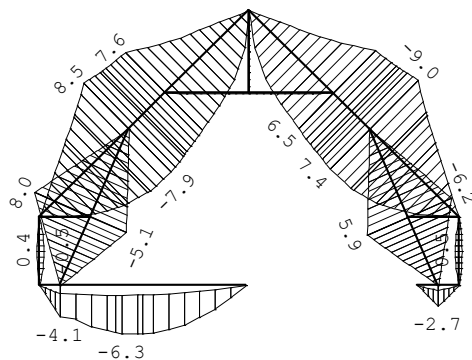
B.C:247



### OMHULLENDE VAN DE FUNDAMENTELE COMBINATIES

MOMENTEN 2e orde  
combinatie

Fundamentele



Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie

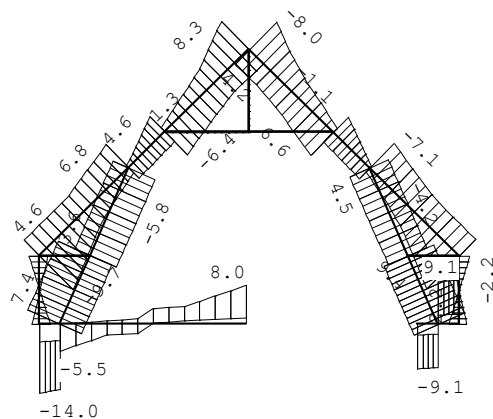


Project.....: 240772  
Onderdeel.....: spant

**DWARSKRACHTEN**  
combinatie

2e orde

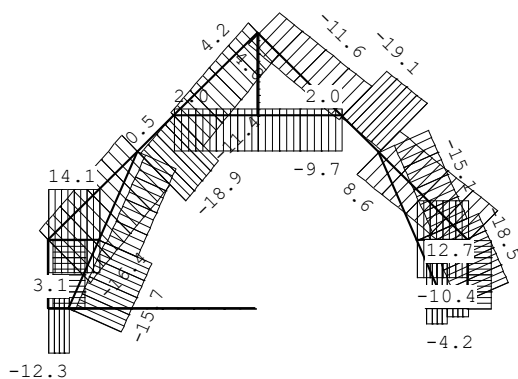
Fundamentele



**NORMAALKRACHTEN**  
combinatie

2e orde

Fundamentele



**REACTIES**  
combinatie

2e orde

Fundamentele

| Kn. | X-min  | X-max | Z-min | Z-max | M-min | M-max |
|-----|--------|-------|-------|-------|-------|-------|
| 11  | -4.19  | 12.70 | 5.01  | 24.00 |       |       |
| 12  |        |       | 2.63  | 15.15 |       |       |
| 13  |        |       | 1.35  | 8.03  |       |       |
| 14  | -12.68 | 4.17  | 2.14  | 9.05  |       |       |

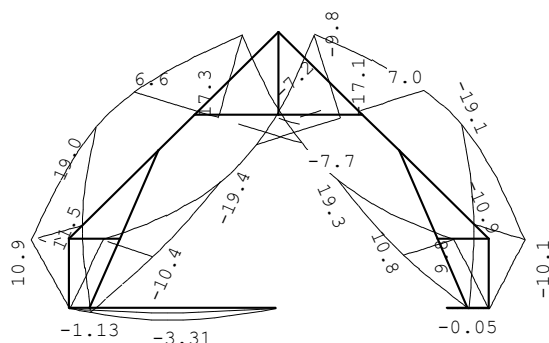
Project.....: 240772

Onderdeel.....: spant

**OMHULLENDE VAN DE KARAKTERISTIEKE COMBINATIES****VERPLAATSINGEN**  
combinatie

1e orde [mm]

Karakteristieke

**REACTIES**

1e orde

Karakteristieke

## combinatie

| Kn. | X-min | X-max | Z-min | Z-max | M-min | M-max |
|-----|-------|-------|-------|-------|-------|-------|
| 11  | -1.17 | 9.31  | 7.64  | 18.05 |       |       |
| 12  |       |       | 4.32  | 11.34 |       |       |
| 13  |       |       | 1.64  | 5.72  |       |       |
| 14  | -9.30 | 1.16  | 3.19  | 6.91  |       |       |

**OMHULLENDE VAN DE BLIJVENDE COMBINATIES****REACTIES**

1e orde

Blijvende

## combinatie

| Kn. | X     | Z     | M |
|-----|-------|-------|---|
| 11  | 3.91  | 10.73 |   |
| 12  |       | 6.43  |   |
| 13  |       | 1.85  |   |
| 14  | -3.91 | 4.41  |   |

**MATERIAALGEGEVENS**

| Mt | Kwaliteit | $f_{m,y,k}$<br>[N/mm <sup>2</sup> ] | $\rho_k$<br>[kg/m <sup>3</sup> ] | $\rho_{mean}$<br>[kg/m <sup>3</sup> ] | $f_{t,0,k}$<br>[N/mm <sup>2</sup> ] | $f_{t,90,k}$<br>[N/mm <sup>2</sup> ] | $f_{c,0,k}$<br>[N/mm <sup>2</sup> ] | $f_{c,90,k}$<br>[N/mm <sup>2</sup> ] | $f_{v,k}$<br>[N/mm <sup>2</sup> ] |
|----|-----------|-------------------------------------|----------------------------------|---------------------------------------|-------------------------------------|--------------------------------------|-------------------------------------|--------------------------------------|-----------------------------------|
| 1  | C18       | 18                                  | 320                              | 380                                   | 10.0                                | 0.4                                  | 18.0                                | 2.2                                  | 3.4                               |

**MATERIAALGEGEVENS (vervolg)**

| Mt | Kwaliteit | $G_{mean}$<br>[N/mm <sup>2</sup> ] | $E_{0,05}$<br>[N/mm <sup>2</sup> ] | $E_{90,mean}$<br>[N/mm <sup>2</sup> ] | $E_{0,mean}$<br>[N/mm <sup>2</sup> ] | Klimaatklasse | $k_{def}$ | $E_{0,mean,fin}$<br>[N/mm <sup>2</sup> ] |
|----|-----------|------------------------------------|------------------------------------|---------------------------------------|--------------------------------------|---------------|-----------|------------------------------------------|
| 1  | C18       | 560                                | 6000                               | 300                                   | 9000                                 | I             | 0.60      | 5625                                     |

**KIPSTABILITEIT**

| Staafl | Plts.<br>aangr. | l sys.<br>[m] | Kipsteunafstanden<br>[m] |
|--------|-----------------|---------------|--------------------------|
| 1      | 1.0*h           | boven:        | 1.82 0;1.823             |
|        |                 | onder:        | 1.82 0;1.823             |
| 2      | 0.0*h           | boven:        | 1.82 0;1.823             |
|        |                 | onder:        | 1.82 0;1.823             |
| 3      | 1.0*h           | boven:        | 0.74 0.743               |
|        |                 | onder:        | 0.74 0.743               |
| 4      | 0.0*h           | boven:        | 0.74 0.743               |
|        |                 | onder:        | 0.74 0.743               |
| 5      | 1.0*h           | boven:        | 1.09 0;1.092             |
|        |                 | onder:        | 1.09 0;1.092             |

Project.....: 240772

Onderdeel.....: spant

**KIPSTABILITEIT**

| Staaft | Plts.<br>aanr. |        | l sys.<br>[m] | Kipsteunafstanden<br>[m] |
|--------|----------------|--------|---------------|--------------------------|
| 6      | 1.0*h          | boven: | 1.09          | 0;1.092                  |
|        |                | onder: | 1.09          | 0;1.092                  |
| 7      | 1.0*h          | boven: | 1.71          | 1.711                    |
|        |                | onder: | 1.71          | 1.711                    |
| 8      | 0.0*h          | boven: | 1.71          | 1.711                    |
|        |                | onder: | 1.71          | 1.711                    |
| 9      | 1.0*h          | boven: | 1.22          | 0;1.220                  |
|        |                | onder: | 1.22          | 0;1.220                  |
| 10     | 1.0*h          | boven: | 1.22          | 1.220                    |
|        |                | onder: | 1.22          | 1.220                    |
| 11     | 1.0*h          | boven: | 1.20          | 0;1.200                  |
|        |                | onder: | 1.20          | 0;1.200                  |
| 12     | 1.0*h          | boven: | 0.30          | 0;0.300                  |
|        |                | onder: | 0.30          | 0;0.300                  |
| 13     | 1.0*h          | boven: | 2.70          | 2.700                    |
|        |                | onder: | 2.70          | 2.700                    |
| 14     | 1.0*h          | boven: | 1.00          | 0;1.000                  |
|        |                | onder: | 1.00          | 0;1.000                  |
| 15     | 1.0*h          | boven: | 0.30          | 0;0.300                  |
|        |                | onder: | 0.30          | 0;0.300                  |
| 16     | 1.0*h          | boven: | 0.30          | 0.300                    |
|        |                | onder: | 0.30          | 0.300                    |
| 17     | 0.0*h          | boven: | 1.00          | 0;1.000                  |
|        |                | onder: | 1.00          | 0;1.000                  |
| 18     | 1.0*h          | boven: | 1.40          | 1.396                    |
|        |                | onder: | 1.40          | 1.396                    |
| 19     | 1.0*h          | boven: | 1.40          | 1.396                    |
|        |                | onder: | 1.40          | 1.396                    |
| 20     | 1.0*h          | boven: | 0.74          | 0;0.739                  |
|        |                | onder: | 0.74          | 0;0.739                  |
| 21     | 1.0*h          | boven: | 0.74          | 0;0.739                  |
|        |                | onder: | 0.74          | 0;0.739                  |

**STABILITEIT**

| Stf | b <sub>gem</sub><br>[mm] | h <sub>gem</sub><br>[mm] | l <sub>sys</sub><br>[mm] | l <sub>buc, y/z</sub><br>[mm] |      | λ <sub>y</sub> | λ <sub>z</sub> | λ <sub>rel, y/z</sub> | β <sub>c</sub> | k <sub>y</sub> | k <sub>z</sub> | k <sub>c, y</sub> | k <sub>c, z</sub> |       |
|-----|--------------------------|--------------------------|--------------------------|-------------------------------|------|----------------|----------------|-----------------------|----------------|----------------|----------------|-------------------|-------------------|-------|
| 1   | 100                      | 220                      | 1823                     | nvt                           | 1823 | 28.7           | 63.2           | 0.501                 | 1.101          | 0.2            | 0.645          | 1.187             | 0.950             | 0.614 |
| 2   | 100                      | 220                      | 1823                     | nvt                           | 1823 | 28.7           | 63.2           | 0.501                 | 1.101          | 0.2            | 0.645          | 1.187             | 0.950             | 0.614 |
| 3   | 100                      | 220                      | 743                      | nvt                           | 743  | 11.7           | 25.8           | 0.204                 | 0.449          | 0.2            | 0.511          | 0.616             | 1.020             | 0.964 |
| 4   | 100                      | 220                      | 743                      | nvt                           | 743  | 11.7           | 25.8           | 0.204                 | 0.449          | 0.2            | 0.511          | 0.616             | 1.020             | 0.964 |
| 5   | 100                      | 220                      | 1092                     | nvt                           | 1092 | 17.2           | 37.8           | 0.300                 | 0.660          | 0.2            | 0.545          | 0.753             | 1.000             | 0.895 |
| 6   | 100                      | 220                      | 1092                     | nvt                           | 1092 | 17.2           | 37.8           | 0.300                 | 0.660          | 0.2            | 0.545          | 0.753             | 1.000             | 0.895 |
| 7   | 100                      | 220                      | 1711                     | nvt                           | 1711 | 26.9           | 59.3           | 0.470                 | 1.034          | 0.2            | 0.627          | 1.107             | 0.959             | 0.664 |
| 8   | 100                      | 220                      | 1711                     | nvt                           | 1711 | 26.9           | 59.3           | 0.470                 | 1.034          | 0.2            | 0.627          | 1.107             | 0.959             | 0.664 |
| 9   | 100                      | 220                      | 1220                     | nvt                           | 1220 | 19.2           | 42.3           | 0.335                 | 0.737          | 0.2            | 0.560          | 0.815             | 0.992             | 0.859 |
| 10  | 100                      | 220                      | 1220                     | nvt                           | 1220 | 19.2           | 42.3           | 0.335                 | 0.737          | 0.2            | 0.560          | 0.815             | 0.992             | 0.859 |
| 11  | 100                      | 220                      | 1200                     | nvt                           | 1200 | 18.9           | 41.6           | 0.329                 | 0.725          | 0.2            | 0.557          | 0.805             | 0.993             | 0.865 |
| 12  | 95                       | 265                      | 300                      | nvt                           | 300  | 3.9            | 10.9           | 0.068                 | 0.191          | 0.2            | 0.479          | 0.507             | 1.049             | 1.023 |
| 13  | 95                       | 265                      | 2700                     | nvt                           | 2700 | 35.3           | 98.5           | 0.615                 | 1.716          | 0.2            | 0.721          | 2.115             | 0.912             | 0.298 |
| 14  | 100                      | 220                      | 1000                     | nvt                           | 1000 | 15.7           | 34.6           | 0.275                 | 0.604          | 0.2            | 0.535          | 0.713             | 1.006             | 0.916 |
| 15  | 95                       | 265                      | 300                      | nvt                           | 300  | 3.9            | 10.9           | 0.068                 | 0.191          | 0.2            | 0.479          | 0.507             | 1.049             | 1.023 |

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



Project.....: 240772

Onderdeel.....: spant

#### STABILITEIT

| Stf | b <sub>gem</sub><br>[mm] | h <sub>gem</sub><br>[mm] | l <sub>sys</sub><br>[mm] | l <sub>buc, y/z</sub><br>[mm] |      | $\lambda_y$ | $\lambda_z$ | $\lambda_{rel, y/z}$ | $\beta_c$ | k <sub>y</sub> | k <sub>z</sub> | k <sub>c, y</sub> | k <sub>c, z</sub> |       |
|-----|--------------------------|--------------------------|--------------------------|-------------------------------|------|-------------|-------------|----------------------|-----------|----------------|----------------|-------------------|-------------------|-------|
| 16  | 95                       | 265                      | 300                      | nvt                           | 300  | 3.9         | 10.9        | 0.068                | 0.191     | 0.2            | 0.479          | 0.507             | 1.049             | 1.023 |
| 17  | 100                      | 220                      | 1000                     | nvt                           | 1000 | 15.7        | 34.6        | 0.275                | 0.604     | 0.2            | 0.535          | 0.713             | 1.006             | 0.916 |
| 18  | 100                      | 220                      | 1396                     | nvt                           | 1396 | 22.0        | 48.4        | 0.383                | 0.843     | 0.2            | 0.582          | 0.910             | 0.981             | 0.799 |
| 19  | 100                      | 220                      | 1396                     | nvt                           | 1396 | 22.0        | 48.4        | 0.383                | 0.843     | 0.2            | 0.582          | 0.910             | 0.981             | 0.799 |
| 20  | 100                      | 220                      | 739                      | nvt                           | 739  | 11.6        | 25.6        | 0.203                | 0.446     | 0.2            | 0.511          | 0.614             | 1.021             | 0.965 |
| 21  | 100                      | 220                      | 739                      | nvt                           | 739  | 11.6        | 25.6        | 0.203                | 0.446     | 0.2            | 0.511          | 0.614             | 1.021             | 0.965 |

#### STABILITEIT (vervolg)

| Staafl | positie<br>[mm] | l <sub>ef,y</sub><br>[mm] | $\sigma_{my,crit}$<br>[N/mm <sup>2</sup> ] | $\lambda_{rel,my}$ | k <sub>crit,y</sub> |
|--------|-----------------|---------------------------|--------------------------------------------|--------------------|---------------------|
| 1      | 1823            | 1531                      | 138.97                                     | 0.36               | 1.00                |
| 2      | 1823            | 1531                      | 138.97                                     | 0.36               | 1.00                |
| 3      | 0               | 633                       | 336.06                                     | 0.23               | 1.00                |
| 4      | 0               | 633                       | 336.06                                     | 0.23               | 1.00                |
| 5      | 1092            | 873                       | 243.73                                     | 0.27               | 1.00                |
| 6      | 1092            | 1423                      | 149.51                                     | 0.35               | 1.00                |
| 7      | 0               | 1430                      | 148.77                                     | 0.35               | 1.00                |
| 8      | 0               | 1430                      | 148.77                                     | 0.35               | 1.00                |
| 9      | 1219            | 1660                      | 128.15                                     | 0.37               | 1.00                |
| 10     | 0               | 1660                      | 128.15                                     | 0.37               | 1.00                |
| 11     | 0               | 1640                      | 129.71                                     | 0.37               | 1.00                |
| 12     | 0               | 138                       | 1159.16                                    | 0.12               | 1.00                |
| 13     | 900             | 2960                      | 53.85                                      | 0.58               | 1.00                |
| 14     | 500             | 1340                      | 158.75                                     | 0.34               | 1.00                |
| 15     | 0               | 138                       | 1159.16                                    | 0.12               | 1.00                |
| 16     | 299             | 138                       | 1159.16                                    | 0.12               | 1.00                |
| 17     | 0               | 1340                      | 158.75                                     | 0.34               | 1.00                |
| 18     | 0               | 1146                      | 185.56                                     | 0.31               | 1.00                |
| 19     | 0               | 1696                      | 125.40                                     | 0.38               | 1.00                |
| 20     | 0               | 1179                      | 180.43                                     | 0.32               | 1.00                |
| 21     | 0               | 1179                      | 180.43                                     | 0.32               | 1.00                |

#### TOETSING SPANNINGEN

| Staafl |    |           |        |              |      |
|--------|----|-----------|--------|--------------|------|
| Staafl | 1  | BC / Sit. | 66 / 4 | UC frm(6.23) | 0.89 |
| Staafl | 2  | BC / Sit. | 49 / 1 | UC frm(6.23) | 0.93 |
| Staafl | 3  | BC / Sit. | 66 / 4 | UC frm(6.19) | 0.85 |
| Staafl | 4  | BC / Sit. | 49 / 1 | UC frm(6.19) | 0.90 |
| Staafl | 5  | BC / Sit. | 65 / 1 | UC frm(6.19) | 0.80 |
| Staafl | 6  | BC / Sit. | 50 / 4 | UC frm(6.19) | 0.62 |
| Staafl | 7  | BC / Sit. | 66 / 4 | UC frm(6.23) | 0.80 |
| Staafl | 8  | BC / Sit. | 49 / 1 | UC frm(6.23) | 0.83 |
| Staafl | 9  | BC / Sit. | 57 / 1 | UC frm(6.24) | 0.04 |
| Staafl | 10 | BC / Sit. | 57 / 1 | UC frm(6.24) | 0.04 |
| Staafl | 12 | BC / Sit. | 1 / 1  | UC frm(6.13) | 0.36 |
| Staafl | 13 | BC / Sit. | 5 / 1  | UC frm(6.17) | 0.51 |
| Staafl | 14 | BC / Sit. | 57 / 1 | UC frm(6.24) | 0.08 |

Project.....: 240772

Onderdeel.....: spant

**TOETSING SPANNINGEN**

|        |    |           |        |              |      |
|--------|----|-----------|--------|--------------|------|
| Staaaf | 15 | BC / Sit. | 6 / 1  | UC frm(6.13) | 0.26 |
| Staaaf | 16 | BC / Sit. | 6 / 1  | UC frm(6.13) | 0.26 |
| Staaaf | 17 | BC / Sit. | 19 / 1 | UC frm(6.13) | 0.06 |
| Staaaf | 18 | BC / Sit. | 65 / 1 | UC frm(6.23) | 0.83 |
| Staaaf | 19 | BC / Sit. | 50 / 1 | UC frm(6.23) | 0.67 |
| Staaaf | 20 | BC / Sit. | 65 / 1 | UC frm(6.17) | 0.09 |
| Staaaf | 21 | BC / Sit. | 50 / 4 | UC frm(6.17) | 0.07 |

**TOETSING DOORBUIGING**

| Stf | Soort | Mtg | $l_{sys}$<br>[mm] | Overstek<br>i j | BC  | Sit | $u_{bij}$<br>[mm] | Toelaatbaar<br>[mm] | $u_{fin,net}$<br>[mm] | Toelaatbaar<br>[mm] |
|-----|-------|-----|-------------------|-----------------|-----|-----|-------------------|---------------------|-----------------------|---------------------|
| 1   | Dak   | ss  | 1823              | Nee Nee         | 185 | 1   | -11.8             | -14.6 2*0.004       | -12.5                 | -14.6 2*0.004       |
| 2   | Dak   | ss  | 1823              | Nee Nee         | 185 | 1   | -11.0             | -14.6 2*0.004       | -11.2                 | -14.6 2*0.004       |
| 3   | Dak   | ss  | 743               | Nee Nee         | 185 | 1   | -0.6              | -5.9 2*0.004        | -0.8                  | -5.9 2*0.004        |
| 4   | Dak   | ss  | 743               | Nee Nee         | 185 | 1   | 0.6               | 5.9 2*0.004         | 0.9                   | 5.9 2*0.004         |
| 7   | Dak   | ss  | 1711              | Nee Nee         | 185 | 1   | 10.6              | 13.7 2*0.004        | 10.9                  | 13.7 2*0.004        |
| 8   | Dak   | ss  | 1711              | Nee Nee         | 185 | 1   | -10.6             | -13.7 2*0.004       | -10.9                 | -13.7 2*0.004       |
| 9   | Vloer | ss  | 1220              | Nee Nee         | 185 | 1   | -7.6              | -7.3 2*0.003        | -7.8                  | -9.8 2*0.004        |
| 10  | Vloer | ss  | 1220              | Nee Nee         | 185 | 1   | -7.6              | -7.3 2*0.003        | -7.8                  | -9.8 2*0.004        |
| 12  | Vloer | ss  | 300               | Nee Nee         | 185 | 1   | -1.0              | -1.8 2*0.003        | -1.6                  | -2.4 2*0.004        |
| 13  | Vloer | db  | 2700              | Nee Nee         | 185 | 1   | -2.6              | -8.1 0.003          | -3.7                  | -10.8 0.004         |
| 15  | Vloer | ss  | 300               | Nee Nee         | 186 | 1   | -0.0              | -1.8 2*0.003        | -0.1                  | -2.4 2*0.004        |
| 16  | Vloer | ss  | 300               | Nee Nee         | 186 | 1   | -0.0              | -1.8 2*0.003        | -0.1                  | -2.4 2*0.004        |
| 20  | Vloer | ss  | 739               | Nee Nee         | 185 | 1   | -4.7              | -4.4 2*0.003        | -5.0                  | -5.9 2*0.004        |
| 21  | Vloer | ss  | 739               | Nee Nee         | 184 | 1   | -4.4              | -4.4 2*0.003        | -4.4                  | -5.9 2*0.004        |

**TOETSING DOORBUIGING (vervolg)**

| Stf | Soort | Mtg | $l_{sys}$<br>[mm] | Overstek<br>i j | Zeeg<br>[mm] | BC  | Sit | $u_{inst}$<br>[mm] | Toelaatbaar<br>[mm] |
|-----|-------|-----|-------------------|-----------------|--------------|-----|-----|--------------------|---------------------|
| 1   | Dak   | ss  | 1823              | Nee Nee         | 0.0          | 146 | 1   | -11.9              | -14.6 2*0.004       |
| 2   | Dak   | ss  | 1823              | Nee Nee         | 0.0          | 162 | 1   | -11.1              | -14.6 2*0.004       |
| 3   | Dak   | db  | 743               | Nee Nee         | 0.0          | 163 | 4   | 0.4                | 3.0 0.004           |
| 4   | Dak   | db  | 743               | Nee Nee         | 0.0          | 146 | 1   | -0.5               | -3.0 0.004          |
| 7   | Dak   | ss  | 1711              | Nee Nee         | 0.0          | 146 | 1   | -10.7              | -13.7 2*0.004       |
| 8   | Dak   | ss  | 1711              | Nee Nee         | 0.0          | 146 | 1   | -10.7              | -13.7 2*0.004       |
| 9   | Vloer | ss  | 1220              | Nee Nee         | 0.0          | 146 | 1   | -7.6               | -9.8 2*0.004        |
| 10  | Vloer | ss  | 1220              | Nee Nee         | 0.0          | 146 | 1   | -7.6               | -9.8 2*0.004        |
| 12  | Vloer | ss  | 300               | Nee Nee         | 0.0          | 125 | 1   | -1.1               | -2.4 2*0.004        |
| 13  | Vloer | db  | 2700              | Nee Nee         | 0.0          | 125 | 1   | -2.7               | -10.8 0.004         |
| 15  | Vloer | ss  | 300               | Nee Nee         | 0.0          | 126 | 1   | -0.0               | -2.4 2*0.004        |
| 16  | Vloer | ss  | 300               | Nee Nee         | 0.0          | 126 | 1   | -0.0               | -2.4 2*0.004        |
| 20  | Vloer | ss  | 739               | Nee Nee         | 0.0          | 146 | 1   | -4.8               | -5.9 2*0.004        |
| 21  | Vloer | ss  | 739               | Nee Nee         | 0.0          | 162 | 1   | -4.4               | -5.9 2*0.004        |

**TOETSING HORIZONTALE VERPLAATSING**

| Staaaf | Mtg | $l_{sys}$<br>[mm] | BC  | Sit | $w_{tot}$<br>[mm] | Toelaatbaar<br>[mm] |
|--------|-----|-------------------|-----|-----|-------------------|---------------------|
| 11     | ss  | 1200              | 146 | 1   | -7.5              | -4.0 300            |
| 14     | ss  | 1000              | 164 | 1   | -10.9             | -3.3 300            |
| 17     | ss  | 1000              | 149 | 4   | -10.1             | -3.3 300            |

Project.....: 240772

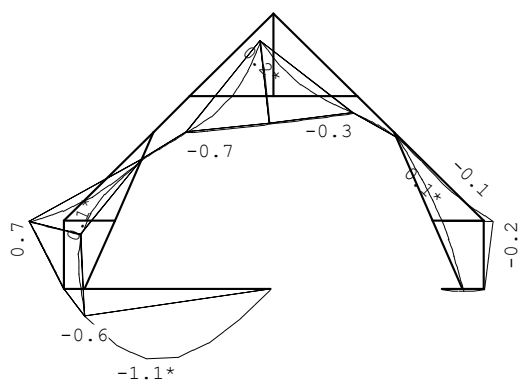
Onderdeel.....: spant

**VERVORMINGEN w1**

Blijvende

combinatie

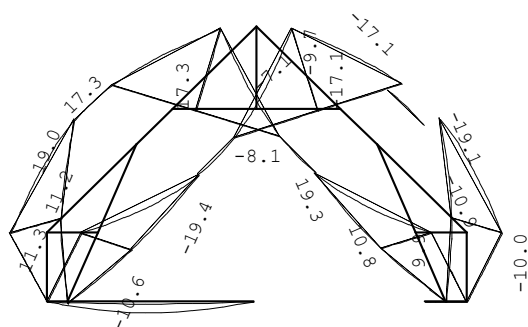
\* - relatief aan de rechte lijn die de uiteinden verbindt

**VERVORMINGEN w<sub>bij</sub>**

Karakteristieke

combinatie

\* - relatief aan de rechte lijn die de uiteinden verbindt



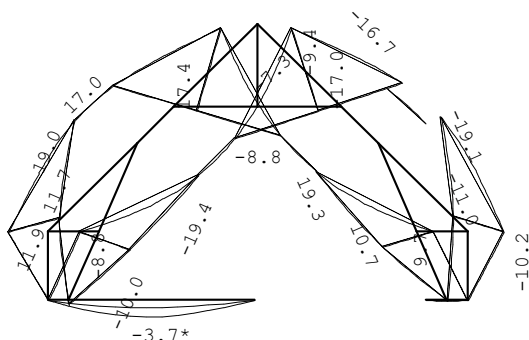
Project.....: 240772  
Onderdeel.....: spant

**VERVORMINGEN W<sub>max</sub>**

Karakteristieke

combinatie

\* - relatief aan de rechte lijn die de uiteinden verbindt

**DOORBUIGINGEN**

Karakteristieke

combinatie

| Nr. | staven | Zijde | positie | $l_{rep}$ | $W_1$ | $W_2$ | $W_{bij}$ | $W_{tot}$ | $W_c$ | $W_{max}$ |
|-----|--------|-------|---------|-----------|-------|-------|-----------|-----------|-------|-----------|
|     |        |       | [m]     | [mm]      | [mm]  | [mm]  | [lrep/]   | [mm]      | [mm]  | [lrep/]   |
| 1   | 1      | Neg.  | /       | 3647      | -0.7  | -0.6  | -11.6     | 313       | -12.4 | -12.4     |
| 1   | 1      | Pos.  | /       | 3647      | -0.7  | -0.4  | 10.1      | 360       | 9.4   | 9.4       |
| 2   | 3      | Neg.  | 0.372   | 743       | 0.0   | 0.0   | -0.4      | 1806      | -0.4  | -0.4      |
| 2   | 3      | Pos.  | 0.372   | 743       | 0.0   | 0.0   | 0.4       | 1736      | 0.4   | 0.4       |
| 3   | 7      | Neg.  | /       | 3423      | 0.3   | 0.2   | -10.0     | 341       | -9.8  | -9.8      |
| 3   | 7      | Pos.  | /       | 3423      | 0.3   | 0.2   | 10.6      | 323       | 10.9  | 10.9      |
| 4   | 2      | Neg.  | /       | 3647      | 0.2   | 0.1   | -10.7     | 342       | -10.5 | -10.5     |
| 4   | 2      | Pos.  | /       | 3647      | 0.2   | 0.1   | 11.0      | 331       | 11.2  | 11.2      |
| 5   | 4      | Neg.  | 0.372   | 743       | -0.0  | -0.0  | -0.4      | 2088      | -0.4  | -0.4      |
| 5   | 4      | Pos.  | 0.372   | 743       | -0.0  | -0.0  | 0.4       | 1921      | 0.4   | 0.4       |
| 6   | 8      | Neg.  | /       | 3423      | 0.3   | 0.2   | -10.0     | 342       | -9.7  | -9.7      |
| 6   | 8      | Pos.  | /       | 3423      | 0.3   | 0.2   | 10.5      | 325       | 10.8  | 10.8      |
| 7   | 5      | Neg.  | /       | 2184      | 0.8   | 0.5   | -10.4     | 209       | -9.7  | -9.7      |
| 7   | 5      | Pos.  | /       | 2184      | 0.8   | 0.6   | 11.6      | 188       | 12.4  | 12.4      |
| 8   | 18     | Neg.  | /       | 2793      | -0.6  | -0.4  | -8.9      | 312       | -9.5  | -9.5      |
| 8   | 18     | Pos.  | /       | 2793      | -0.6  | -0.3  | 7.8       | 356       | 7.3   | 7.3       |
| 9   | 6      | Neg.  | /       | 2184      | -0.2  | -0.1  | -10.9     | 201       | -11.0 | -11.0     |
| 9   | 6      | Pos.  | /       | 2184      | -0.2  | -0.1  | 10.8      | 202       | 10.6  | 10.6      |
| 10  | 19     | Neg.  | /       | 2793      | 0.1   | 0.1   | -8.2      | 340       | -8.1  | -8.1      |
| 10  | 19     | Pos.  | /       | 2793      | 0.1   | 0.1   | 8.5       | 328       | 8.6   | 8.6       |
| 11  | 9      | Neg.  | /       | 2440      | 0.2   | 0.1   | -7.2      | 338       | -7.0  | -7.0      |
| 11  | 9      | Pos.  | /       | 2440      | 0.2   | 0.1   | 7.6       | 321       | 7.8   | 7.8       |
| 12  | 10     | Neg.  | /       | 2440      | 0.2   | 0.1   | -7.1      | 341       | -6.9  | -6.9      |
| 12  | 10     | Pos.  | /       | 2440      | 0.2   | 0.2   | 7.5       | 323       | 7.8   | 7.8       |
| 14  | 12     | Neg.  | /       | 600       | -0.6  | -0.4  | -1.0      | 593       | -1.6  | -1.6      |
| 15  | 13     | Neg.  | 1.350   | 2700      | -1.1  | -1.0  | -2.6      | 1044      | -3.7  | -3.7      |
| 15  | 13     | Pos.  | /       | 5400      | 0.6   | 0.4   | 1.0       | 5340      | 1.6   | 1.6       |
| 17  | 15     | Neg.  | /       | 600       | -0.0  | -0.0  | -0.0      | 16456     | -0.1  | -0.1      |
| 18  | 16     | Pos.  | /       | 600       | 0.0   | 0.0   | 0.0       | 16456     | 0.1   | 0.1       |
| 20  | 20     | Neg.  | /       | 1478      | -0.3  | -0.2  | -4.7      | 313       | -5.0  | -5.0      |
| 20  | 20     | Pos.  | /       | 1478      | -0.3  | -0.2  | 4.1       | 359       | 3.9   | 3.9       |
| 21  | 21     | Neg.  | /       | 1478      |       |       | -4.3      | 343       | -4.3  | -4.3      |

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



Project.....: 240772  
Onderdeel.....: spant

#### DOORBUIGINGEN

Karakteristieke

combinatie

| Nr. | staven | Zijde | positie | $l_{rep}$ | $w_1$ | $w_2$ | -- $w_{bij}$ -- | $w_{tot}$ | $w_c$ | -- $w_{max}$ -- |
|-----|--------|-------|---------|-----------|-------|-------|-----------------|-----------|-------|-----------------|
|     |        |       | [m]     | [mm]      | [mm]  | [mm]  | [mm] [lrep/]    | [mm]      | [mm]  | [mm] [lrep/]    |
| 21  | 21     | Pos.  | /       | 1478      |       |       | 4.4 338         | 4.4       |       | 4.4 338         |

**3.9 Traptraveling**

Uitgangspunt traptraveling wordt opgezet uit nieuwe houten balken

**q1**

|               | $\Psi_0$ | breedte | lengte | kN/m <sup>2</sup> | kN/m <sup>1</sup> |       | kN/m <sup>2</sup> | kN/m <sup>1</sup> |
|---------------|----------|---------|--------|-------------------|-------------------|-------|-------------------|-------------------|
| 3e verdieping | 1        | 0,50    | 3,00   | 0,90              | 1,35              | extr. | 3,00              | 4,50              |
|               |          |         |        | $g_k =$           | 1,4               |       | $q_k =$           | 4,5               |

**q2**

|               | $\Psi_0$ | breedte | lengte | kN/m <sup>2</sup> | kN/m <sup>1</sup> |       | kN/m <sup>2</sup> | kN/m <sup>1</sup> |
|---------------|----------|---------|--------|-------------------|-------------------|-------|-------------------|-------------------|
| 3e verdieping | 1        | 0,50    | 0,60   | 0,90              | 0,27              | extr. | 3,00              | 0,90              |
|               |          |         |        | $G_k =$           | 0,3               |       | $q_k =$           | 0,9               |

**q3**

|               | $\Psi_0$ | breedte | lengte | kN/m <sup>2</sup> | kN/m <sup>1</sup> |       | kN/m <sup>2</sup> | kN/m <sup>1</sup> |
|---------------|----------|---------|--------|-------------------|-------------------|-------|-------------------|-------------------|
| 3e verdieping | 1        | 0,50    | 0,88   | 0,90              | 0,39              | extr. | 3,00              | 1,31              |
|               |          |         |        | $G_k =$           | 0,4               |       | $q_k =$           | 1,3               |

**q4**

|          | $\Psi_0$ | breedte | lengte | kN/m <sup>2</sup> | kN/m <sup>1</sup> |  | kN/m <sup>2</sup> | kN/m <sup>1</sup> |
|----------|----------|---------|--------|-------------------|-------------------|--|-------------------|-------------------|
| hsb wand |          | 1,00    | 2,80   | 0,80              | 2,24              |  |                   |                   |
|          |          |         |        | $G_k =$           | 2,2               |  | $q_k =$           | 0,0               |

$$P1 = \text{reactie spantbeen links} = (7,5 + 4,4) * 1/6 = 1,3 + 0,7$$

$$P1 = \text{reactie spantbeen rechts} = (7,5 + 4,4) * 2/3 = 5 + 2,9$$

Technosoft Raamwerken release 6.82  
2024

11 dec

Project.....: 240772  
 Onderdeel.....: trapaveling  
 Dimensies.....: kN;m;rad (tenzij anders aangegeven)  
 Datum.....: 11/12/2024  
 Bestand.....: G:\.shortcut-targets-by-id\0ByYUb81WrbDqYlpOSXRzaHdIV0E\  
 Projecten\2024\240772\Houtconstructie\trapaveling.rww

Belastingbreedte.: 1.000  
 Rekenmodel.....: 2e-orde-elastisch.  
 Theorieën voor de bepaling van de krachtsverdeling:  
 1) Uiterste grenstoestand:  
 Geometrisch niet lineair alle staven.  
 Fysisch lineair alle staven.  
 2) Gebruiksgrenstoestand:  
 Lineaire-elasticiteitstheorie

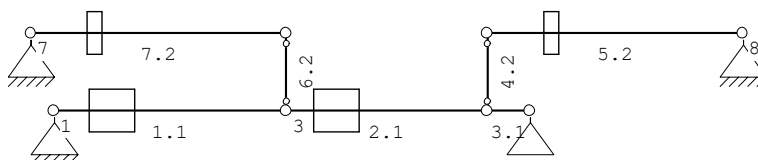
Maximum aantal iteraties.....: 50  
 Max.deellengte kolommen/wanden: 0.500 Max.deellengte balken/vloeren: 0.500  
 Max. X-verplaatsing in UGT.....: 0.500 Max. Z-verplaatsing in UGT....: 0.250

Gunstige werking van de permanente belasting wordt automatisch verwerkt.

#### Toegepaste normen volgens Eurocode met Nederlandse NB

|             |                      |                  |              |
|-------------|----------------------|------------------|--------------|
| Belastingen | NEN-EN 1990:2002     | C2:2010, A1:2019 | NB:2019 (nl) |
|             | NEN-EN 1991-1-1:2002 | C1/C11:2019      | NB:2019 (nl) |
| Hout        | NEN-EN 1995-1-1:2005 | A1:2011, C1:2006 | NB:2013 (nl) |

#### GEOMETRIE



#### MATERIALEN

| Mt | Kwaliteit | E-modulus [N/mm <sup>2</sup> ] | S.G. | S.G.verhoogd | Pois. | Uitz. coëff |
|----|-----------|--------------------------------|------|--------------|-------|-------------|
| 1  | C24       | 11000                          | 3.5  | 4.2          | 1.00  | 5.0000e-06  |

Bij de bepaling v.h. e.g. van houten staven is de S.G.verhoogd toegepast.

#### PROFIELEN [mm]

| Prof. | Omschrijving | Materiaal | Oppervlak  | Traagheid  | Vormf. |
|-------|--------------|-----------|------------|------------|--------|
| 1     | B*H 288*271  | 1:C24     | 7.8048e+04 | 4.7766e+08 | 0.00   |
| 2     | B*H 96*271   | 1:C24     | 2.6016e+04 | 1.5922e+08 | 0.00   |
| 3     | B*H 71*271   | 1:C24     | 1.9241e+04 | 1.1776e+08 | 0.00   |

#### PROFIELEN vervolg [mm]

| Prof. | Staaftype | Breedte | Hoogte | e     | Type | b1 | h1 | b2 | h2 |
|-------|-----------|---------|--------|-------|------|----|----|----|----|
| 1     | 0:Normaal | 288     | 271    | 135.5 | 0:RH |    |    |    |    |
| 2     | 0:Normaal | 96      | 271    | 135.5 | 0:RH |    |    |    |    |
| 3     | 0:Normaal | 71      | 271    | 135.5 | 0:RH |    |    |    |    |

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



Project.....: 240772  
Onderdeel.....: trapaveling

#### PROFIELVORMEN [mm]

1 B\*H 288\*271



2 B\*H 96\*271



3 B\*H 71\*271



#### KNOPEN

| Knoop | X     | Z     | Knoop | X      | Z     |
|-------|-------|-------|-------|--------|-------|
| 1     | 0.000 | 0.000 | 6     | 5.600  | 0.000 |
| 2     | 6.150 | 0.000 | 7     | -0.300 | 1.000 |
| 3     | 3.000 | 0.000 | 8     | 8.900  | 1.000 |
| 4     | 3.000 | 1.000 |       |        |       |
| 5     | 5.600 | 1.000 |       |        |       |

#### STAVEN

| St. | ki | kj | Profiel       | Aansl.i | Aansl.j | Lengte Opm. |
|-----|----|----|---------------|---------|---------|-------------|
| 1   | 1  | 3  | 1:B*H 288*271 | NDM     | NDM     | 3.000       |
| 2   | 3  | 6  | 1:B*H 288*271 | NDM     | NDM     | 2.600       |
| 3   | 6  | 2  | 1:B*H 288*271 | NDM     | NDM     | 0.550       |
| 4   | 6  | 5  | 2:B*H 96*271  | ND-     | ND-     | 1.000       |
| 5   | 5  | 8  | 2:B*H 96*271  | NDM     | NDM     | 3.300       |
| 6   | 3  | 4  | 2:B*H 96*271  | ND-     | ND-     | 1.000       |
| 7   | 7  | 4  | 2:B*H 96*271  | NDM     | NDM     | 3.300       |

#### VASTE STEUNPUNTEN

| Nr. | knoop | Kode | XZR 1=vast 0=vrij | Hoek |
|-----|-------|------|-------------------|------|
| 1   | 1     | 110  |                   | 0.00 |
| 2   | 2     | 010  |                   | 0.00 |
| 3   | 7     | 110  |                   | 0.00 |
| 4   | 8     | 110  |                   | 0.00 |

#### BELASTINGGENERATIE ALGEMEEN.

Betrouwbaarheidsklasse.....: 2 Referentieperiode.....: 50  
Gebouwdiepte.....: 0.00 Gebouwhoogte.....: 1.00  
Niveau aansl.terrein.....: 0.00 E.g. scheid.w. [kN/m2]: 0.00

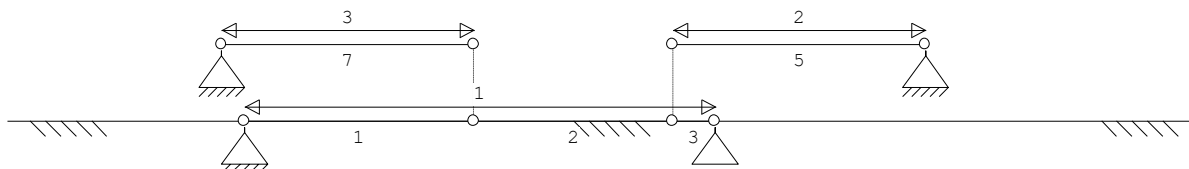
#### STAFTYPEN

| Type            | staven    |
|-----------------|-----------|
| 1:Vloer.        | : 1-3,5,7 |
| 5:Linker gevel. | : 4,6     |

Project.....: 240772  
Onderdeel....: trapaveling

**LASTVELDEN**

Veranderlijke belastingen door personen

**LASTVELDEN**

| Nr | Staaf | Tabel | Klasse-Gebruiksfunctie | Verd. | $q_k$ | $Q_k$ | $F_t/F_{t0}$ |
|----|-------|-------|------------------------|-------|-------|-------|--------------|
| 1  | 1-3   | 6.2   | B-Kantoorruimtes       | 0     | -2.50 | -3.00 | 1.00         |
| 2  | 5-5   | 6.2   | B-Kantoorruimtes       | 0     | -2.50 | -3.00 | 1.00         |
| 3  | 7-7   | 6.2   | B-Kantoorruimtes       | 0     | -2.50 | -3.00 | 1.00         |

**BELASTINGGEVALLEN**

| B.G. | Omschrijving                    | Type |
|------|---------------------------------|------|
| 1    | Permanente belasting EGZ=0.00   | 1    |
| g*   | 2 Ver. bel. pers. ed. ( $q_k$ ) | 2    |
| g    | 3 Ver. bel. pers. ed. ( $Q_k$ ) | 3    |

g = gegenereerd belastinggeval

\* = belastinggeval bevat 1 of meer handmatig toegevoegde en/of gewijzigde lasten

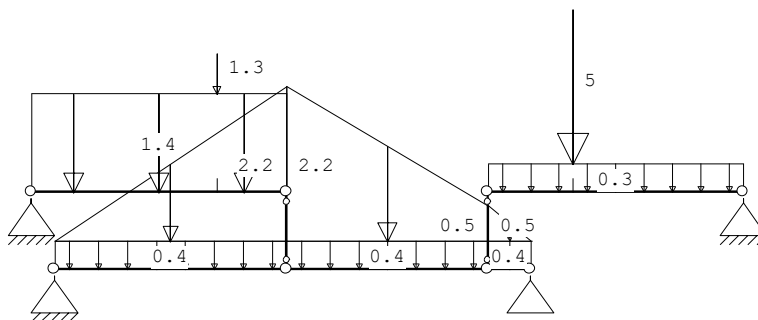
**BELASTINGGEVALLEN vervolg**

| B.G. | Omschrijving                  | Belastingduurklasse |
|------|-------------------------------|---------------------|
| 1    | Permanente belasting          | Blijvend            |
| 2    | Ver. bel. pers. ed. ( $q_k$ ) | Middellang          |
| 3    | Ver. bel. pers. ed. ( $Q_k$ ) | Middellang          |

**BELASTINGEN**

B.G:1 Permanente

belasting

**STAAFBELASTINGEN**

B.G:1 Permanente

belasting

| Staaf | Type       | $q_1/p/m$ | $q_2$ | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|-------|------------|-----------|-------|-------|-------|----------|----------|----------|
| 7     | 1:QZLokaal | -1.40     | -1.40 | 0.000 | 0.000 |          |          |          |
| 1     | 1:QZLokaal | -0.40     | -0.40 | 0.000 | 0.000 |          |          |          |
| 5     | 1:QZLokaal | -0.30     | -0.30 | 0.000 | 0.000 |          |          |          |
| 2     | 1:QZLokaal | -0.40     | -0.40 | 0.000 | 0.000 |          |          |          |
| 3     | 1:QZLokaal | -0.40     | -0.40 | 0.000 | 0.000 |          |          |          |
| 1     | 1:QZLokaal | 0.00      | -2.20 | 0.000 | 0.000 |          |          |          |
| 2     | 1:QZLokaal | -2.20     | -0.50 | 0.000 | 0.000 |          |          |          |
| 3     | 1:QZLokaal | -0.50     | 0.00  | 0.000 | 0.000 |          |          |          |
| 7     | 8:PZLokaal | -1.30     |       | 2.400 |       |          |          |          |

Project.....: 240772  
Onderdeel.....: trapaveling

**STAAFBELASTINGEN**

B.G:1 Permanente

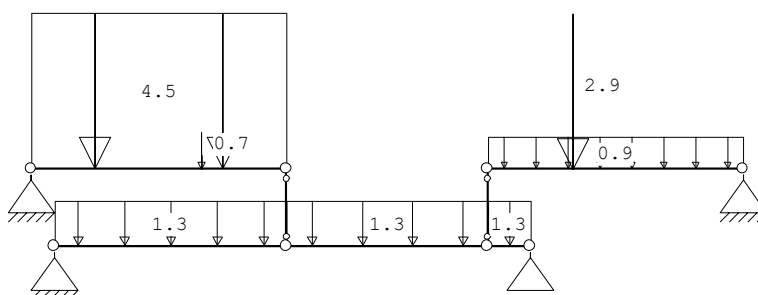
belasting

| Staaf | Type       | q1/p/m | q2 | A     | B | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|-------|------------|--------|----|-------|---|----------|----------|----------|
| 5     | 8:PZLokaal | -5.00  |    | 1.100 |   |          |          |          |

**BELASTINGEN**

B.G:2 Ver. bel. pers. ed.

(q\_k)

**STAAFBELASTINGEN**

B.G:2 Ver. bel. pers. ed.

(q\_k)

| Staaf | Type        | Index | q1/p/m | q2    | A     | B     | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|-------|-------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 1     | 3:QZgeProj. | *     | -1.30  | -1.30 | 0.000 | 0.000 | 0.50     | 0.50     | 0.30     |
| 2     | 3:QZgeProj. | *     | -1.30  | -1.30 | 0.000 | 0.000 | 0.50     | 0.50     | 0.30     |
| 3     | 3:QZgeProj. | *     | -1.30  | -1.30 | 0.000 | 0.000 | 0.50     | 0.50     | 0.30     |
| 5     | 3:QZgeProj. | *     | -0.90  | -0.90 | 0.000 | 0.000 | 0.50     | 0.50     | 0.30     |
| 7     | 3:QZgeProj. | *     | -4.50  | -4.50 | 0.000 | 0.000 | 0.50     | 0.50     | 0.30     |
| 7     | 8:PZLokaal  | *     | -0.70  |       | 2.200 |       | 0.50     | 0.50     | 0.30     |
| 5     | 8:PZLokaal  | *     | -2.90  |       | 1.100 |       | 0.50     | 0.50     | 0.30     |

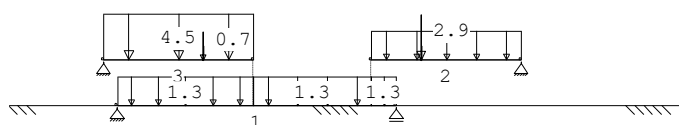
Opmerkingen

[\*] Deze belasting is handmatig toegevoegd of gewijzigd.

**SITUATIES BELAST/ONBELAST**

B.G:2 Ver. bel. pers. ed.

(q\_k)

**SITUATIES BELAST/ONBELAST**

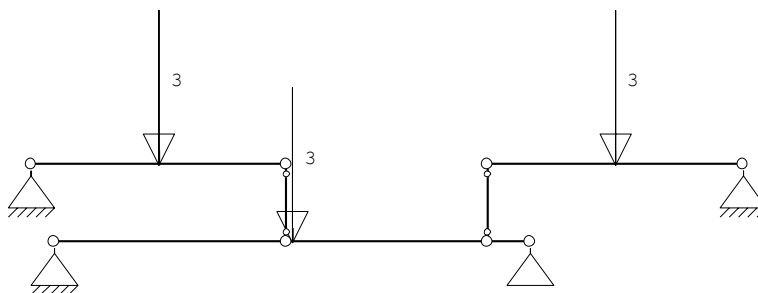
Belastingtype: q\_k

| Nr | Lastvelden belast | Lastvelden onbelast |
|----|-------------------|---------------------|
| 1  | 1-3               |                     |

Project.....: 240772  
Onderdeel....: trapaveling

**BELASTINGEN**

B.G:3 Ver. bel. pers. ed.

(Q<sub>k</sub>)**STAAFBELASTINGEN**

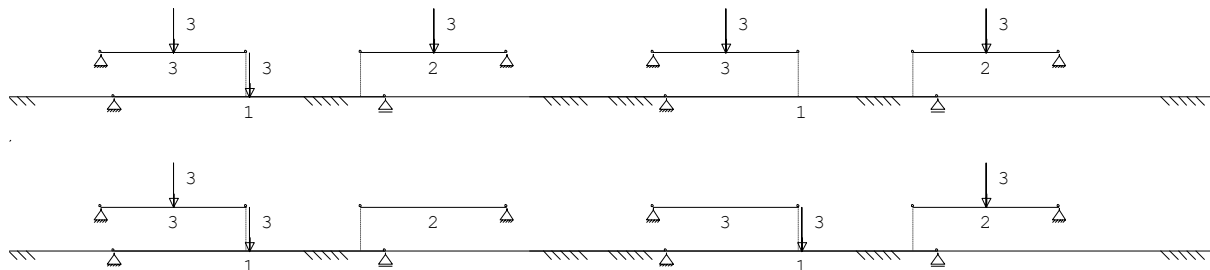
B.G:3 Ver. bel. pers. ed.

(Q<sub>k</sub>)

| Staat | Type        | q1/p/m | q2 | A     | B | ψ <sub>0</sub> | ψ <sub>1</sub> | ψ <sub>2</sub> |
|-------|-------------|--------|----|-------|---|----------------|----------------|----------------|
| 2     | 10:PZGepro. | -3.00  |    | 0.075 |   | 0.50           | 0.50           | 0.30           |
| 5     | 10:PZGepro. | -3.00  |    | 1.650 |   | 0.50           | 0.50           | 0.30           |
| 7     | 10:PZGepro. | -3.00  |    | 1.650 |   | 0.50           | 0.50           | 0.30           |

**SITUATIES BELAST/ONBELAST**

B.G:3 Ver. bel. pers. ed.

(Q<sub>k</sub>)**SITUATIES BELAST/ONBELAST**Belastingtype: Q<sub>k</sub>

| Nr | Lastvelden belast | Lastvelden onbelast |
|----|-------------------|---------------------|
| 1  | 1-3               |                     |
| 2  | 2,3               | 1                   |
| 3  | 1,3               | 2                   |
| 4  | 1,2               | 3                   |

**BEREKENINGSTATUS**

| B.C. | Iteratie | Status                 |
|------|----------|------------------------|
| 1    | 3        | Nauwkeurigheid bereikt |
| 2    | 3        | Nauwkeurigheid bereikt |
| 3    | 3        | Nauwkeurigheid bereikt |
| 4    | 3        | Nauwkeurigheid bereikt |
| 5    | 3        | Nauwkeurigheid bereikt |
| 6    | 3        | Nauwkeurigheid bereikt |
| 7    | 3        | Nauwkeurigheid bereikt |
| 8    | 3        | Nauwkeurigheid bereikt |
| 9    | 3        | Nauwkeurigheid bereikt |
| 10   | 3        | Nauwkeurigheid bereikt |
| 11   | 1        | Lineaire berekening    |
| 12   | 1        | Lineaire berekening    |

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



Project.....: 240772  
Onderdeel....: trapaveling

#### BEREKENINGSTATUS

| B.C. | Iteratie | Status              |
|------|----------|---------------------|
| 13   | 1        | Lineaire berekening |
| 14   | 1        | Lineaire berekening |
| 15   | 1        | Lineaire berekening |
| 16   | 1        | Lineaire berekening |
| 17   | 1        | Lineaire berekening |
| 18   | 1        | Lineaire berekening |
| 19   | 1        | Lineaire berekening |

#### BELASTINGCOMBINATIES

| BC | Type  |      |           |   |                       |
|----|-------|------|-----------|---|-----------------------|
| 1  | Fund. | 1.35 | $G_{k,1}$ |   |                       |
| 2  | Fund. | 0.90 | $G_{k,1}$ |   |                       |
| 3  | Fund. | 1.35 | $G_{k,1}$ | + | 1.50 $\psi_0 Q_{k,2}$ |
| 4  | Fund. | 1.35 | $G_{k,1}$ | + | 1.50 $\psi_0 Q_{k,3}$ |
| 5  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 $Q_{k,2}$        |
| 6  | Fund. | 1.20 | $G_{k,1}$ | + | 1.50 $Q_{k,3}$        |
| 7  | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 $Q_{k,2}$        |
| 8  | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 $\psi_0 Q_{k,2}$ |
| 9  | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 $\psi_0 Q_{k,3}$ |
| 10 | Fund. | 0.90 | $G_{k,1}$ | + | 1.50 $Q_{k,3}$        |
| 11 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 $Q_{k,2}$        |
| 12 | Kar.  | 1.00 | $G_{k,1}$ | + | 1.00 $Q_{k,3}$        |
| 13 | Quas. | 1.00 | $G_{k,1}$ |   |                       |
| 14 | Quas. | 1.00 | $G_{k,1}$ | + | 1.00 $\psi_2 Q_{k,2}$ |
| 15 | Quas. | 1.00 | $G_{k,1}$ | + | 1.00 $\psi_2 Q_{k,3}$ |
| 16 | Freq. | 1.00 | $G_{k,1}$ |   |                       |
| 17 | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 $\psi_1 Q_{k,2}$ |
| 18 | Freq. | 1.00 | $G_{k,1}$ | + | 1.00 $\psi_1 Q_{k,3}$ |
| 19 | Blij. | 1.00 | $G_{k,1}$ |   |                       |

#### GUNSTIGE WERKING PERMANENTE BELASTINGEN

| BC | Staven met gunstige werking |
|----|-----------------------------|
| 1  | Geen                        |
| 2  | Alle staven de factor:0.90  |
| 3  | Geen                        |
| 4  | Geen                        |
| 5  | Geen                        |
| 6  | Geen                        |
| 7  | Alle staven de factor:0.90  |
| 8  | Alle staven de factor:0.90  |
| 9  | Alle staven de factor:0.90  |
| 10 | Alle staven de factor:0.90  |

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



Project.....: 240772  
Onderdeel.....: trapaveling

### BELASTINGCOMBINATIE

B.C:19

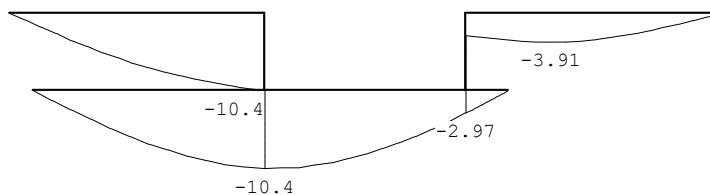
Blijvend

### VERPLAATSINGEN

1e orde [mm]

B.C:19

Blijvend



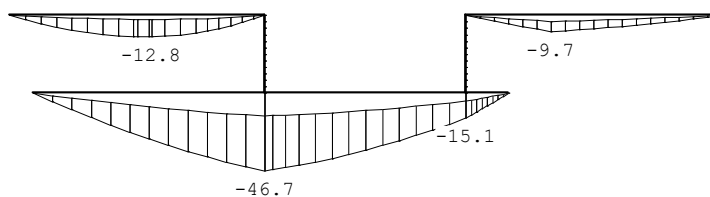
### OMHULLENDE VAN DE FUNDAMENTELE COMBINATIES

### MOMENTEN

2e orde

Fundamentele

combinatie

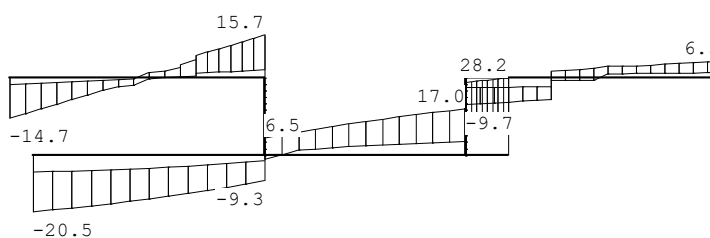


### DWARSKRACHTEN

2e orde

Fundamentele

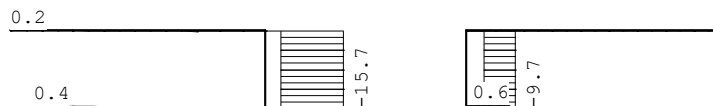
combinatie



Project.....: 240772  
 Onderdeel.....: trapaveling

**NORMAALKRACHTEN** 2e orde  
 combinatie

Fundamentele

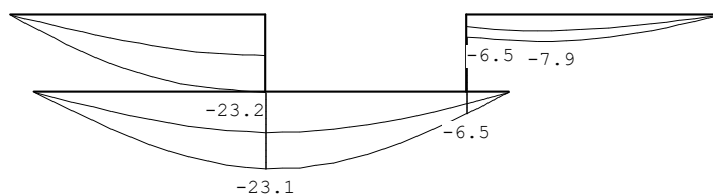

**REACTIES** 2e orde  
 combinatie

Fundamentele

| Kn. | X-min | X-max | Z-min | Z-max | M-min | M-max |
|-----|-------|-------|-------|-------|-------|-------|
| 1   | 0.00  | 0.01  | 6.02  | 20.54 |       |       |
| 2   |       |       | 8.82  | 28.20 |       |       |
| 7   | 0.02  | 0.08  | 2.40  | 14.68 |       |       |
| 8   | -0.03 | -0.00 | 1.95  | 6.27  |       |       |

**OMHULLENDE VAN DE KARAKTERISTIEKE COMBINATIES**
**VERPLAATSINGEN** 1e orde [mm]  
 combinatie

Karakteristieke


**REACTIES** 1e orde  
 combinatie

Karakteristieke

| Kn. | X-min | X-max | Z-min | Z-max | M-min | M-max |
|-----|-------|-------|-------|-------|-------|-------|
| 1   | 0.00  | 0.00  | 7.59  | 15.03 |       |       |
| 2   |       |       | 11.90 | 20.76 |       |       |
| 7   | 0.00  | 0.00  | 2.66  | 10.32 |       |       |
| 8   | 0.00  | 0.00  | 2.16  | 4.61  |       |       |

**OMHULLENDE VAN DE BLIJVENDE COMBINATIES**
**REACTIES** 1e orde  
 combinatie

Blijvende

| Kn. | X    | Z    | M |
|-----|------|------|---|
| 1   | 0.00 | 6.69 |   |
| 2   |      | 9.80 |   |
| 7   | 0.00 | 2.66 |   |
| 8   | 0.00 | 2.16 |   |

**MATERIAALGEGEVENS**

| Mt | Kwaliteit | $f_{m,y,k}$<br>[N/mm <sup>2</sup> ] | $\rho_k$<br>[kg/m <sup>3</sup> ] | $\rho_{mean}$<br>[kg/m <sup>3</sup> ] | $f_{t,0,k}$<br>[N/mm <sup>2</sup> ] | $f_{t,90,k}$<br>[N/mm <sup>2</sup> ] | $f_{c,0,k}$<br>[N/mm <sup>2</sup> ] | $f_{c,90,k}$<br>[N/mm <sup>2</sup> ] | $f_{v,k}$<br>[N/mm <sup>2</sup> ] |
|----|-----------|-------------------------------------|----------------------------------|---------------------------------------|-------------------------------------|--------------------------------------|-------------------------------------|--------------------------------------|-----------------------------------|
| 1  | C24       | 24                                  | 350                              | 420                                   | 14.5                                | 0.4                                  | 21.0                                | 2.5                                  | 4.0                               |

**MATERIAALGEGEVENS (vervolg)**

| Mt | Kwaliteit | $G_{mean}$<br>[N/mm <sup>2</sup> ] | $E_{0,05}$<br>[N/mm <sup>2</sup> ] | $E_{90,mean}$<br>[N/mm <sup>2</sup> ] | $E_{0,mean}$<br>[N/mm <sup>2</sup> ] | Klimaatklasse | $k_{def}$ | $E_{0,mean,fin}$<br>[N/mm <sup>2</sup> ] |
|----|-----------|------------------------------------|------------------------------------|---------------------------------------|--------------------------------------|---------------|-----------|------------------------------------------|
| 1  | C24       | 690                                | 7400                               | 370                                   | 11000                                | I             | 0.60      | 6875                                     |

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



Project.....: 240772  
Onderdeel....: trapaveling

#### KIPSTABILITEIT

| Staaft | Plts.<br>aangr. | l sys.<br>[m]    | Kipsteunafstanden<br>[m]     |
|--------|-----------------|------------------|------------------------------|
| 1      | 1.0*h           | boven:<br>onder: | 3.00 0;3.000<br>3.00 0;3.000 |
| 2      | 1.0*h           | boven:<br>onder: | 2.60 2.600<br>2.60 2.600     |
| 3      | 1.0*h           | boven:<br>onder: | 0.55 0.550<br>0.55 0.550     |
| 4      | 1.0*h           | boven:<br>onder: | 1.00 0;1.000<br>1.00 0;1.000 |
| 5      | 1.0*h           | boven:<br>onder: | 3.30 0;3.300<br>3.30 0;3.300 |
| 6      | 1.0*h           | boven:<br>onder: | 1.00 0;1.000<br>1.00 0;1.000 |
| 7      | 1.0*h           | boven:<br>onder: | 3.30 0;3.300<br>3.30 0;3.300 |

#### STABILITEIT

| Stf | b <sub>gem</sub><br>[mm] | h <sub>gem</sub><br>[mm] | l <sub>sys</sub><br>[mm] | l <sub>buc, y/z</sub><br>[mm] |      | $\lambda_y$ | $\lambda_z$ | $\lambda_{rel, y/z}$ | $\beta_c$ | k <sub>y</sub> | k <sub>z</sub> | k <sub>c, y</sub> | k <sub>c, z</sub> |       |
|-----|--------------------------|--------------------------|--------------------------|-------------------------------|------|-------------|-------------|----------------------|-----------|----------------|----------------|-------------------|-------------------|-------|
| 1   | 288                      | 271                      | 3000                     | 3000                          | nvt  | 38.3        | 36.1        | 0.650                | 0.612     | 0.2            | 0.746          | 0.718             | 0.898             | 0.913 |
| 2   | 288                      | 271                      | 2600                     | 2600                          | nvt  | 33.2        | 31.3        | 0.564                | 0.530     | 0.2            | 0.685          | 0.664             | 0.930             | 0.941 |
| 3   | 288                      | 271                      | 550                      | 550                           | nvt  | 7.0         | 6.6         | 0.119                | 0.112     | 0.2            | 0.489          | 0.488             | 1.038             | 1.040 |
| 4   | 96                       | 271                      | 1000                     | nvt                           | 1000 | 12.8        | 36.1        | 0.217                | 0.612     | 0.2            | 0.515          | 0.718             | 1.018             | 0.913 |
| 5   | 96                       | 271                      | 3300                     | nvt                           | 3300 | 42.2        | 119.1       | 0.715                | 2.019     | 0.2            | 0.797          | 2.710             | 0.870             | 0.221 |
| 6   | 96                       | 271                      | 1000                     | nvt                           | 1000 | 12.8        | 36.1        | 0.217                | 0.612     | 0.2            | 0.515          | 0.718             | 1.018             | 0.913 |
| 7   | 96                       | 271                      | 3300                     | nvt                           | 3300 | 42.2        | 119.1       | 0.715                | 2.019     | 0.2            | 0.797          | 2.710             | 0.870             | 0.221 |

#### STABILITEIT (vervolg)

| Staaft | positie<br>[mm] | l <sub>ef,y</sub><br>[mm] | $\sigma_{my,crit}$<br>[N/mm <sup>2</sup> ] | $\lambda_{rel,my}$ | k <sub>crit,y</sub> |
|--------|-----------------|---------------------------|--------------------------------------------|--------------------|---------------------|
| 1      | 3000            | 3242                      | 544.92                                     | 0.21               | 1.00                |
| 2      | 0               | 3142                      | 562.26                                     | 0.21               | 1.00                |
| 3      | 0               | 1037                      | 1703.58                                    | 0.12               | 1.00                |
| 4      | 0               | 864                       | 227.06                                     | 0.33               | 1.00                |
| 5      | 1100            | 3842                      | 51.09                                      | 0.69               | 1.00                |
| 6      | 0               | 864                       | 227.06                                     | 0.33               | 1.00                |
| 7      | 1833            | 3512                      | 55.89                                      | 0.66               | 1.00                |

#### TOETSING SPANNINGEN

| Staaft |   |           |       |              |      |
|--------|---|-----------|-------|--------------|------|
| Staaft | 1 | BC / Sit. | 5 / 1 | UC frm(6.17) | 0.90 |
| Staaft | 2 | BC / Sit. | 5 / 1 | UC frm(6.17) | 0.90 |
| Staaft | 3 | BC / Sit. | 5 / 1 | UC frm(6.17) | 0.29 |
| Staaft | 4 | BC / Sit. | 5 / 1 | UC frm(6.24) | 0.03 |
| Staaft | 5 | BC / Sit. | 5 / 1 | UC frm(6.23) | 0.56 |
| Staaft | 6 | BC / Sit. | 5 / 1 | UC frm(6.24) | 0.05 |

Project.....: 240772  
Onderdeel.....: trapaveling

**TOETSING SPANNINGEN**

Staaf 7 BC / Sit. 5 / 1 UC frm(6.23) 0.74

**TOETSING DOORBUIGING**

| Stf | Soort | Mtg | $l_{sys}$<br>[mm] | Overstek<br>i j | BC | Sit | $u_{bij}$<br>[mm] | Toelaatbaar<br>[mm] *1 | $u_{fin,net}$<br>[mm] | Toelaatbaar<br>[mm] *1 |
|-----|-------|-----|-------------------|-----------------|----|-----|-------------------|------------------------|-----------------------|------------------------|
| 1   | Vloer | ss  | 3000              | Nee Nee         | 14 | 1   | -21.2             | -18.0 2*0.003          | -31.7                 | -24.0 2*0.004          |
| 2   | Dak   | ss  | 2600              | Nee Nee         | 14 | 1   | -15.3             | -20.8 2*0.004          | -22.7                 | -20.8 2*0.004          |
| 3   | Vloer | ss  | 550               | Nee Nee         | 14 | 1   | -6.0              | -3.3 2*0.003           | -8.9                  | -4.4 2*0.004           |
| 5   | Dak   | db  | 3300              | Nee Nee         | 14 | 1   | -3.4              | -13.2 0.004            | -5.5                  | -13.2 0.004            |
| 7   | Dak   | ss  | 3300              | Nee Nee         | 14 | 1   | -21.3             | -26.4 2*0.004          | -31.7                 | -26.4 2*0.004          |

**TOETSING DOORBUIGING (vervolg)**

| Stf | Soort | Mtg | $l_{sys}$<br>[mm] | Overstek<br>i j | Zeeg<br>[mm] | BC | Sit | $u_{inst}$<br>[mm] | Toelaatbaar<br>[mm] *1 |
|-----|-------|-----|-------------------|-----------------|--------------|----|-----|--------------------|------------------------|
| 1   | Vloer | ss  | 3000              | Nee Nee         | 0.0          | 11 | 1   | -23.1              | -24.0 2*0.004          |
| 2   | Dak   | ss  | 2600              | Nee Nee         | 0.0          | 11 | 1   | -16.6              | -20.8 2*0.004          |
| 3   | Vloer | ss  | 550               | Nee Nee         | 0.0          | 11 | 1   | -6.5               | -4.4 2*0.004           |
| 5   | Dak   | db  | 3300              | Nee Nee         | 0.0          | 11 | 1   | -3.9               | -13.2 0.004            |
| 7   | Dak   | ss  | 3300              | Nee Nee         | 0.0          | 11 | 1   | -23.2              | -26.4 2*0.004          |

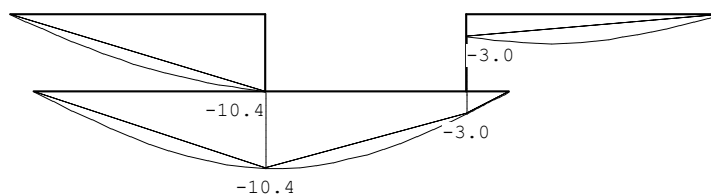
**TOETSING HORIZONTALE VERPLAATSING**

| Staaf | Mtg | $l_{sys}$<br>[mm] | BC | Sit | $w_{tot}$<br>[mm] | Toelaatbaar<br>[mm] [h/ ] |
|-------|-----|-------------------|----|-----|-------------------|---------------------------|
| 4     | db  | 1000              | 11 | 0   | 0.0               | -3.3 300                  |
| 6     | db  | 1000              | 11 | 0   | 0.0               | -3.3 300                  |

**VERVORMINGEN w1**  
combinatie

Blijvende

\* - relatief aan de rechte lijn die de uiteinden verbindt



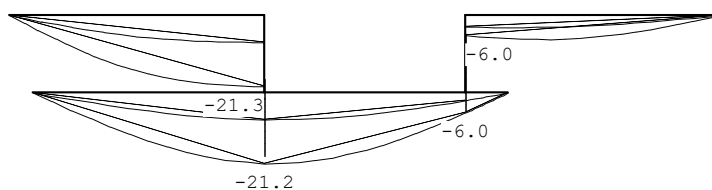
Project.....: 240772  
Onderdeel.....: trapaveling

**VERVORMINGEN  $W_{bij}$** 

Karakteristieke

combinatie

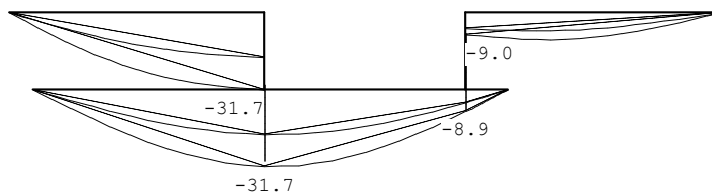
\* - relatief aan de rechte lijn die de uiteinden verbindt

**VERVORMINGEN  $W_{max}$** 

Karakteristieke

combinatie

\* - relatief aan de rechte lijn die de uiteinden verbindt

**DOORBUIGINGEN**

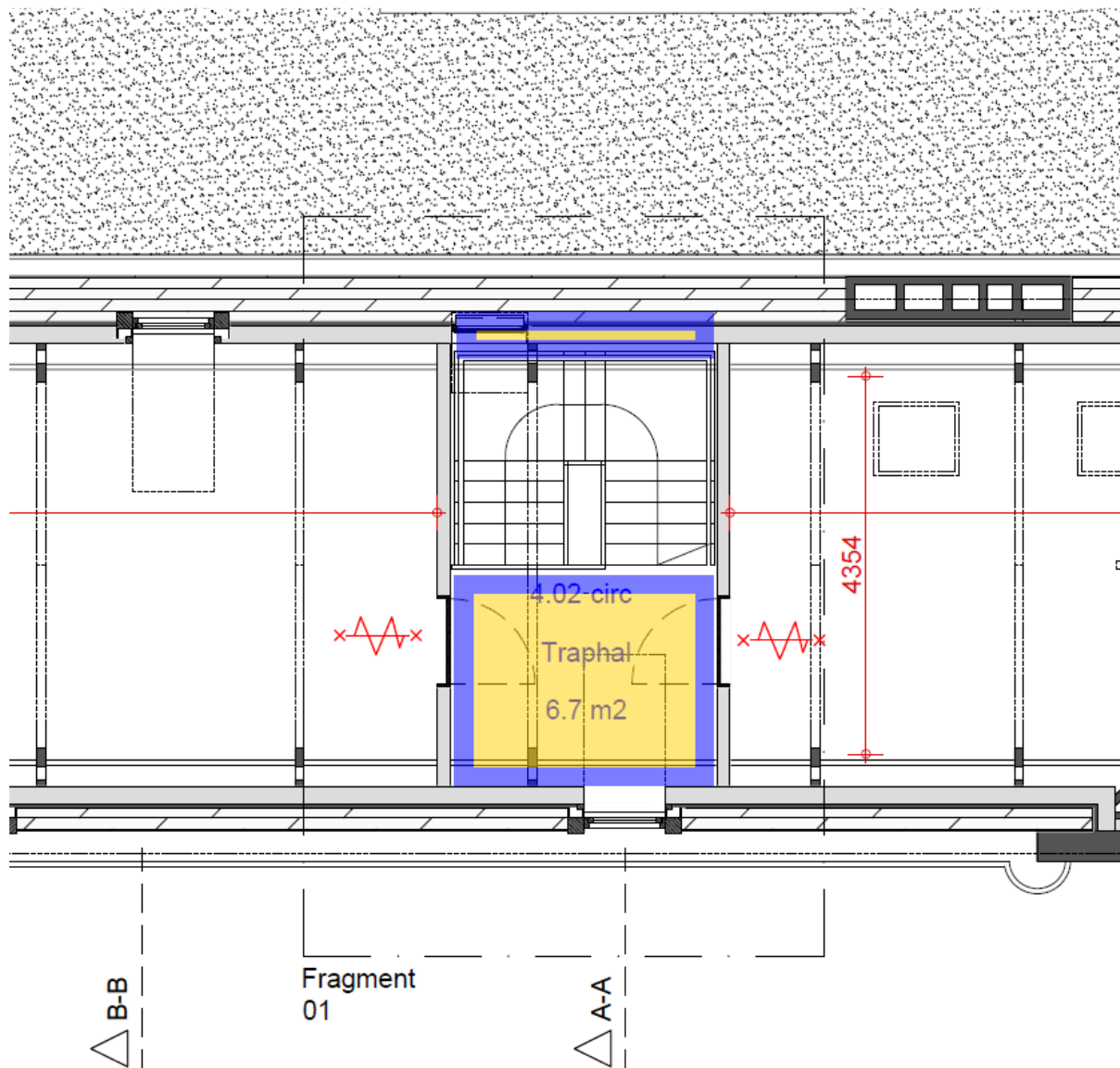
Karakteristieke

combinatie

| Nr. | staven | Zijde | positie | $l_{rep}$ | $W_1$ | $W_2$ | $W_{bij}$    | $W_{tot}$ | $W_c$ | $W_{max}$    |
|-----|--------|-------|---------|-----------|-------|-------|--------------|-----------|-------|--------------|
|     |        |       | [m]     | [mm]      | [mm]  | [mm]  | [mm] [lrep/] | [mm]      | [mm]  | [mm] [lrep/] |
| 1   | 1      | Neg.  | /       | 6000      | -10.4 | -8.5  | -21.2        | 282       | -31.7 | -31.7        |
| 2   | 2      | Neg.  | 1.300   | 2600      | -1.8  | -1.5  | -3.6         | 713       | -5.5  | -5.5         |
| 2   | 2      | Pos.  | /       | 5200      | 7.5   | 6.1   | 15.3         | 340       | 22.7  | 22.7         |
| 3   | 3      | Neg.  | 0.275   | 550       | -0.0  | -0.0  | -0.0         | 15006     | -0.1  | -0.1         |
| 3   | 3      | Pos.  | /       | 1100      | 3.0   | 2.4   | 6.0          | 184       | 8.9   | 8.9          |
| 5   | 5      | Neg.  | 1.650   | 3300      | -2.1  | -1.6  | -3.4         | 975       | -5.4  | -5.4         |
| 5   | 5      | Pos.  | /       | 6600      | 3.0   | 2.4   | 6.0          | 1102      | 9.0   | 9.0          |
| 7   | 7      | Neg.  | /       | 6600      | -10.4 | -8.6  | -21.3        | 310       | -31.7 | -31.7        |

### 3.10 Afdracht horizontale belasting spant naar vloer

De horizontale belasting uit de spanten moet door de vloervelden onder en boven de trapparing naar het stijve vloerveld worden afgedragen.



Aan de onderzijde zit een vloerveld van 3 meter hoog hier is de vloer stijf genoeg.

Aan de bovenzijde is dit vloerveld maar 500 mm breed.

Hier zal dit door de nieuwe raveelbalk opgevangen moeten worden.

$P1 = \text{horizontale belasting spant} = 3,9 + 5,4$

Technosoft Raamwerken release 6.82  
2024

11 dec

Project.....: 240772  
 Onderdeel.....: raveelbalk boven horizontaal  
 Dimensies.....: kN;m;rad (tenzij anders aangegeven)  
 Datum.....: 11/12/2024  
 Bestand.....: G:\.shortcut-targets-by-id\0ByYUb81WrbDqYlpOSXRzaHdIV0E\  
 Projecten\2024\240772\Houtconstructie\raveelbalk  
 horizontaal.rww

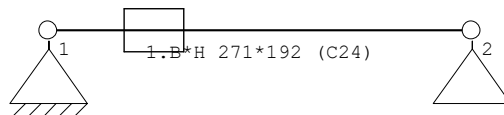
Belastingbreedte.: 1.000  
 Rekenmodel.....: 2e-orde-elastisch.  
 Theorieën voor de bepaling van de krachtsverdeling:  
 1) Uiterste grenstoestand:  
 Geometrisch niet lineair alle staven.  
 Fysisch lineair alle staven.  
 2) Gebruiksgrenstoestand:  
 Lineaire-elasticiteitstheorie

Maximum aantal iteraties.....: 50  
 Max.deellengte kolommen/wanden: 0.500 Max.deellengte balken/vloeren: 0.500  
 Max. X-verplaatsing in UGT.....: 0.500 Max. Z-verplaatsing in UGT....: 0.250

Gunstige werking van de permanente belasting wordt automatisch verwerkt.

**Toegepaste normen volgens Eurocode met Nederlandse NB**

|             |                      |                 |             |
|-------------|----------------------|-----------------|-------------|
| Belastingen | NEN-EN 1990:2002     | C2:2010,A1:2019 | NB:2019(nl) |
|             | NEN-EN 1991-1-1:2002 | C1/C11:2019     | NB:2019(nl) |
| Hout        | NEN-EN 1995-1-1:2005 | A1:2011,C1:2006 | NB:2013(nl) |

**GEOMETRIE****MATERIALEN**

| Mt | Kwaliteit | E-modulus [N/mm <sup>2</sup> ] | S.G. | S.G.verhoogd | Pois. | Uitz. coëff |
|----|-----------|--------------------------------|------|--------------|-------|-------------|
| 1  | C24       | 11000                          | 3.5  | 4.2          | 1.00  | 5.0000e-06  |

Bij de bepaling v.h. e.g. van houten staven is de S.G.verhoogd toegepast.

**PROFIELEN [mm]**

| Prof. | Omschrijving | Materiaal | Oppervlak  | Traagheid  | Vormf. |
|-------|--------------|-----------|------------|------------|--------|
| 1     | B*H 271*192  | 1:C24     | 5.2032e+04 | 1.5984e+08 | 0.00   |

**PROFIELEN vervolg [mm]**

| Prof. | Staaftype | Breedte | Hoogte | e    | Type | b1 | h1 | b2 | h2 |
|-------|-----------|---------|--------|------|------|----|----|----|----|
| 1     | 0:Normaal | 271     | 192    | 96.0 | 0:RH |    |    |    |    |

**PROFIELVORMEN [mm]**

1 B\*H 271\*192



Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



Project.....: 240772  
Onderdeel.....: raveelbalk boven horizontaal

#### KNOPEN

| Knoop | X     | Z     |
|-------|-------|-------|
| 1     | 0.000 | 0.000 |
| 2     | 3.300 | 0.000 |

#### STAVEN

| St. | ki | kj | Profiel       | Aansl.i | Aansl.j | Lengte | Opm. |
|-----|----|----|---------------|---------|---------|--------|------|
| 1   | 1  | 2  | 1:B*H 271*192 | NDM     | NDM     | 3.300  |      |

#### VASTE STEUNPUNTEN

| Nr. | knoop | Kode | XZR 1=vast 0=vrij | Hoek |
|-----|-------|------|-------------------|------|
| 1   | 1     | 110  |                   | 0.00 |
| 2   | 2     | 010  |                   | 0.00 |

#### BELASTINGGENERATIE ALGEMEEN.

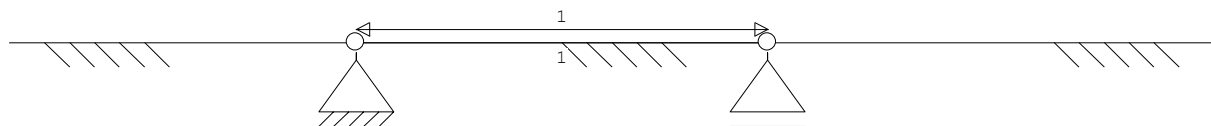
Betrouwbaarheidsklasse.....: 2 Referentieperiode.....: 50  
Gebouwdiepte.....: 0.00 Gebouwhoogte.....: 0.00  
Niveau aansl.terrein.....: 0.00 E.g. scheid.w. [kN/m2]: 0.00

#### STAFTYPEN

| Type     | staven |
|----------|--------|
| 1:Vloer. | : 1    |

#### LASTVELDEN

Veranderlijke belastingen door personen



#### LASTVELDEN

| Nr | Staaf | Tabel | Klasse-Gebruiksfunctie | Verd. | q <sub>k</sub> | Q <sub>k</sub> | F <sub>t</sub> /F <sub>t0</sub> |
|----|-------|-------|------------------------|-------|----------------|----------------|---------------------------------|
| 1  | 1-1   | 6.2   | A-Vloeren              | 0     | -1.75          | -3.00          | 1.00                            |

#### BELASTINGGEVALLEN

| B.G. | Omschrijving                            | Type       |
|------|-----------------------------------------|------------|
| 1    | Permanente belasting                    | EGZ=0.00 1 |
| g*   | 2 Ver. bel. pers. ed. (q <sub>k</sub> ) | 2          |

g = gegenereerd belastinggeval

\* = belastinggeval bevat 1 of meer handmatig toegevoegde en/of gewijzigde lasten

#### BELASTINGGEVALLEN vervolg

| B.G. | Omschrijving                          | Belastingduurklasse |
|------|---------------------------------------|---------------------|
| 1    | Permanente belasting                  | Blijvend            |
| 2    | Ver. bel. pers. ed. (q <sub>k</sub> ) | Middellang          |

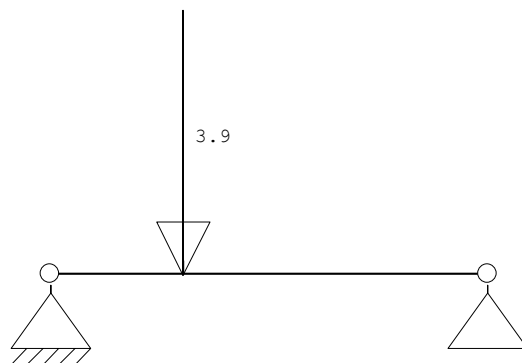
Project.....: 240772

Onderdeel.....: raveelbalk boven horizontaal

**BELASTINGEN**

B.G:1 Permanente

belasting

**STAAFBELASTINGEN**

B.G:1 Permanente

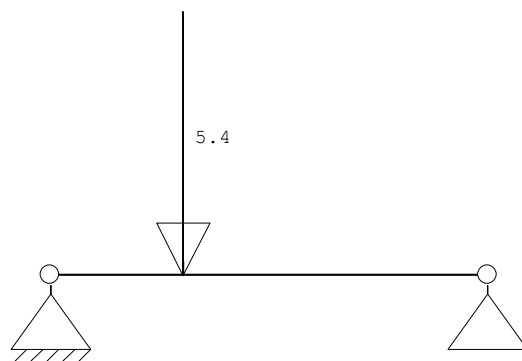
belasting

| Staaf | Type       | q1/p/m | q2 | A     | B | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|-------|------------|--------|----|-------|---|----------|----------|----------|
| 1     | 8:PZLokaal | -3.90  |    | 1.000 |   |          |          |          |

**BELASTINGEN**

B.G:2 Ver. bel. pers. ed.

(q\_k)

**STAAFBELASTINGEN**

B.G:2 Ver. bel. pers. ed.

(q\_k)

| Staaf | Type       | Index | q1/p/m | q2 | A     | B | $\psi_0$ | $\psi_1$ | $\psi_2$ |
|-------|------------|-------|--------|----|-------|---|----------|----------|----------|
| 1     | 8:PZLokaal | *     | -5.40  |    | 1.000 |   | 0.40     | 0.50     | 0.30     |

Opmerkingen

[\*] Deze belasting is handmatig toegevoegd of gewijzigd.

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



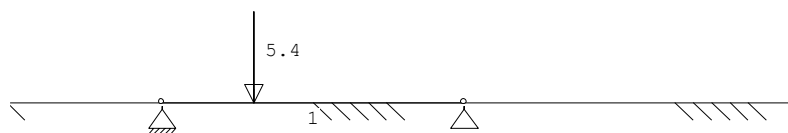
Project.....: 240772

Onderdeel.....: raveelbalk boven horizontaal

## SITUATIES BELAST/ONBELAST

B.G:2 Ver. bel. pers. ed.

(q<sub>k</sub>)



## SITUATIES BELAST/ONBELAST

Belastingtype: q<sub>k</sub>

| Nr Lastvelden belast | Lastvelden onbelast |
|----------------------|---------------------|
| 1 1                  |                     |

## BEREKENINGSTATUS

| B.C. | Iteratie | Status                 |
|------|----------|------------------------|
| 1    | 3        | Nauwkeurigheid bereikt |
| 2    | 3        | Nauwkeurigheid bereikt |
| 3    | 3        | Nauwkeurigheid bereikt |
| 4    | 3        | Nauwkeurigheid bereikt |
| 5    | 3        | Nauwkeurigheid bereikt |
| 6    | 3        | Nauwkeurigheid bereikt |
| 7    | 1        | Lineaire berekening    |
| 8    | 1        | Lineaire berekening    |
| 9    | 1        | Lineaire berekening    |
| 10   | 1        | Lineaire berekening    |
| 11   | 1        | Lineaire berekening    |
| 12   | 1        | Lineaire berekening    |

## BELASTINGCOMBINATIES

| BC | Type  |                                                              |
|----|-------|--------------------------------------------------------------|
| 1  | Fund. | 1.35 G <sub>k,1</sub>                                        |
| 2  | Fund. | 0.90 G <sub>k,1</sub>                                        |
| 3  | Fund. | 1.35 G <sub>k,1</sub> + 1.50 ψ <sub>0</sub> Q <sub>k,2</sub> |
| 4  | Fund. | 1.20 G <sub>k,1</sub> + 1.50 Q <sub>k,2</sub>                |
| 5  | Fund. | 0.90 G <sub>k,1</sub> + 1.50 Q <sub>k,2</sub>                |
| 6  | Fund. | 0.90 G <sub>k,1</sub> + 1.50 ψ <sub>0</sub> Q <sub>k,2</sub> |
| 7  | Kar.  | 1.00 G <sub>k,1</sub> + 1.00 Q <sub>k,2</sub>                |
| 8  | Quas. | 1.00 G <sub>k,1</sub>                                        |
| 9  | Quas. | 1.00 G <sub>k,1</sub> + 1.00 ψ <sub>2</sub> Q <sub>k,2</sub> |
| 10 | Freq. | 1.00 G <sub>k,1</sub>                                        |
| 11 | Freq. | 1.00 G <sub>k,1</sub> + 1.00 ψ <sub>1</sub> Q <sub>k,2</sub> |
| 12 | Blij. | 1.00 G <sub>k,1</sub>                                        |

## GUNSTIGE WERKING PERMANENTE BELASTINGEN

| BC | Staven met gunstige werking |
|----|-----------------------------|
| 1  | Geen                        |
| 2  | Alle staven de factor:0.90  |
| 3  | Geen                        |
| 4  | Geen                        |
| 5  | Alle staven de factor:0.90  |
| 6  | Alle staven de factor:0.90  |

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



Project.....: 240772  
Onderdeel.....: raveelbalk boven horizontaal

### BELASTINGCOMBINATIE

B.C:12

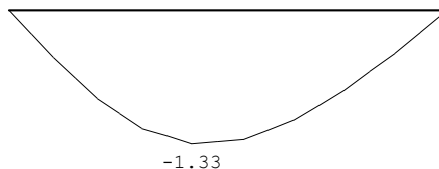
Blijvend

### VERPLAATSINGEN

1e orde [mm]

B.C:12

Blijvend



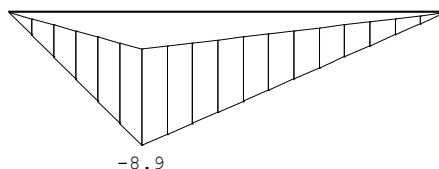
### OMHULLENDE VAN DE FUNDAMENTELE COMBINATIES

### MOMENTEN

2e orde

Fundamentele

combinatie

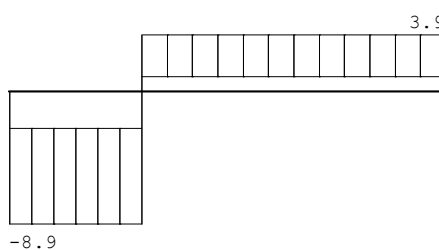


### DWARSKRACHTEN

2e orde

Fundamentele

combinatie



Project Rustenburgerstraat 246 Franse School

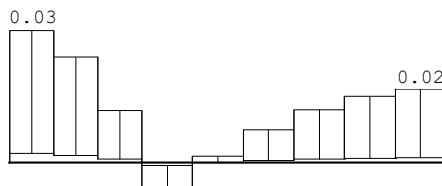
Projectnummer 240772

Revisie



Project.....: 240772  
Onderdeel.....: raveelbalk boven horizontaal

**NORMAALKRACHTEN** 2e orde Fundamentele combinatie

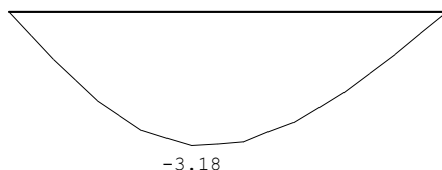


**REACTIES** 2e orde Fundamentele combinatie

| Kn. | X-min | X-max | Z-min | Z-max | M-min | M-max |
|-----|-------|-------|-------|-------|-------|-------|
| 1   | 0.00  | 0.02  | 2.45  | 8.91  |       |       |
| 2   |       |       | 1.06  | 3.87  |       |       |

#### OMHULLENDE VAN DE KARAKTERISTIEKE COMBINATIES

**VERPLAATSINGEN** 1e orde [mm] Karakteristieke combinatie



**REACTIES** 1e orde Karakteristieke combinatie

| Kn. | X    | Z    | M |
|-----|------|------|---|
| 1   | 0.00 | 6.48 |   |
| 2   |      | 2.82 |   |

#### OMHULLENDE VAN DE BLIJVENDE COMBINATIES

**REACTIES** 1e orde Blijvende combinatie

| Kn. | X    | Z    | M |
|-----|------|------|---|
| 1   | 0.00 | 2.72 |   |
| 2   |      | 1.18 |   |

#### MATERIAALGEGEVENS

| Mt | Kwaliteit | $f_{m,y,k}$<br>[N/mm <sup>2</sup> ] | $\rho_k$<br>[kg/m <sup>3</sup> ] | $\rho_{mean}$<br>[kg/m <sup>3</sup> ] | $f_{t,0,k}$<br>[N/mm <sup>2</sup> ] | $f_{t,90,k}$<br>[N/mm <sup>2</sup> ] | $f_{c,0,k}$<br>[N/mm <sup>2</sup> ] | $f_{c,90,k}$<br>[N/mm <sup>2</sup> ] | $f_{v,k}$<br>[N/mm <sup>2</sup> ] |
|----|-----------|-------------------------------------|----------------------------------|---------------------------------------|-------------------------------------|--------------------------------------|-------------------------------------|--------------------------------------|-----------------------------------|
| 1  | C24       | 24                                  | 350                              | 420                                   | 14.5                                | 0.4                                  | 21.0                                | 2.5                                  | 4.0                               |

#### MATERIAALGEGEVENS (vervolg)

| Mt | Kwaliteit | $G_{mean}$<br>[N/mm <sup>2</sup> ] | $E_{0,05}$<br>[N/mm <sup>2</sup> ] | $E_{90,mean}$<br>[N/mm <sup>2</sup> ] | $E_{0,mean}$<br>[N/mm <sup>2</sup> ] | Klimaatklasse | $k_{def}$ | $E_{0,mean,fin}$<br>[N/mm <sup>2</sup> ] |
|----|-----------|------------------------------------|------------------------------------|---------------------------------------|--------------------------------------|---------------|-----------|------------------------------------------|
| 1  | C24       | 690                                | 7400                               | 370                                   | 11000                                | I             | 0.60      | 6875                                     |

#### KIPSTABILITEIT

| Staaf | Plts.<br>aanr. | 1 sys.<br>[m]    | Kipsteunafstanden<br>[m]     |
|-------|----------------|------------------|------------------------------|
| 1     | 1.0*h          | boven:<br>onder: | 3.30 0;3.300<br>3.30 0;3.300 |

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



Project.....: 240772

Onderdeel....: raveelbalk boven horizontaal

### STABILITEIT

| Stf | b <sub>gem</sub><br>[mm] | h <sub>gem</sub><br>[mm] | l <sub>sys</sub><br>[mm] | l <sub>buc, y/z</sub><br>[mm] |     | $\lambda_y$ | $\lambda_z$ | $\lambda_{rel, y/z}$ | $\beta_c$ | k <sub>y</sub> | k <sub>z</sub> | k <sub>c, y</sub> | k <sub>c, z</sub> |       |
|-----|--------------------------|--------------------------|--------------------------|-------------------------------|-----|-------------|-------------|----------------------|-----------|----------------|----------------|-------------------|-------------------|-------|
| 1   | 271                      | 192                      | 3300                     | 3300                          | nvt | 59.5        | 42.2        | 1.010                | 0.715     | 0.2            | 1.081          | 0.797             | 0.682             | 0.870 |

### STABILITEIT (vervolg)

| Staafl | positie<br>[mm] | l <sub>ef,y</sub><br>[mm] | $\sigma_{my,crit}$<br>[N/mm <sup>2</sup> ] | $\lambda_{rel,my}$ | k <sub>crit,y</sub> |
|--------|-----------------|---------------------------|--------------------------------------------|--------------------|---------------------|
| 1      | 1000            | 3684                      | 599.30                                     | 0.20               | 1.00                |

### TOETSING SPANNINGEN

|        |   |           |       |              |      |
|--------|---|-----------|-------|--------------|------|
| Staafl | 1 | BC / Sit. | 4 / 1 | UC frm(6.17) | 0.36 |
|--------|---|-----------|-------|--------------|------|

### TOETSING DOORBUIGING

| Stf | Soort | Mtg | l <sub>sys</sub><br>[mm] | Overstek<br>i j | BC | Sit | u <sub>bi,j</sub><br>[mm] | Toelaatbaar<br>[mm] | *1    | u <sub>fin,net</sub><br>[mm] | Toelaatbaar<br>[mm] | *1    |
|-----|-------|-----|--------------------------|-----------------|----|-----|---------------------------|---------------------|-------|------------------------------|---------------------|-------|
| 1   | Vloer | db  | 3300                     | Nee Nee         | 9  | 1   | -3.0                      | -9.9                | 0.003 | -4.3                         | -13.2               | 0.004 |

### TOETSING DOORBUIGING (vervolg)

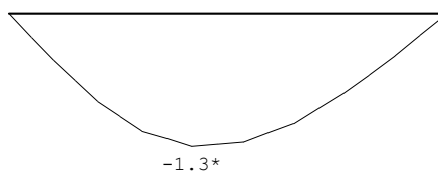
| Stf | Soort | Mtg | l <sub>sys</sub><br>[mm] | Overstek<br>i j | Zeeg<br>[mm] | BC | Sit | u <sub>inst</sub><br>[mm] | Toelaatbaar<br>[mm] | *1    |
|-----|-------|-----|--------------------------|-----------------|--------------|----|-----|---------------------------|---------------------|-------|
| 1   | Vloer | db  | 3300                     | Nee Nee         | 0.0          | 7  | 1   | -3.2                      | -13.2               | 0.004 |

### VERVORMINGEN w1

Blijvende

combinatie

\* - relatief aan de rechte lijn die de uiteinden verbindt



-1.3\*

Project Rustenburgerstraat 246 Franse School

Projectnummer 240772

Revisie



Project.....: 240772

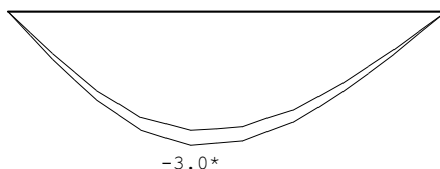
Onderdeel.....: raveelbalk boven horizontaal

#### VERVORMINGEN $W_{bij}$

Karakteristieke

combinatie

\* - relatief aan de rechte lijn die de uiteinden verbindt

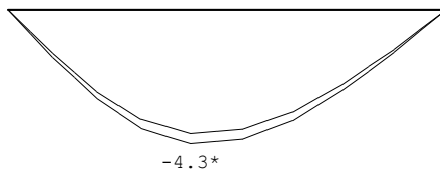


#### VERVORMINGEN $W_{max}$

Karakteristieke

combinatie

\* - relatief aan de rechte lijn die de uiteinden verbindt



#### DOORBUIGINGEN

Karakteristieke

combinatie

| Nr. | staven | Zijde | positie | $l_{rep}$ | $W_1$ | $W_2$ | -- $W_{bij}$ -- | $W_{tot}$ | $W_c$ | -- $W_{max}$ -- |
|-----|--------|-------|---------|-----------|-------|-------|-----------------|-----------|-------|-----------------|
|     |        |       | [m]     | [mm]      | [mm]  | [mm]  | [mm] [lrep/]    | [mm]      | [mm]  | [mm] [lrep/]    |
| 1   | 1      | Neg.  | 1.383   | 3300      | -1.3  | -1.1  | -3.0 1107       | -4.3      |       | -4.3 765        |

Gecombineerde U.C.=0,36+0,56=0,9 akkoord